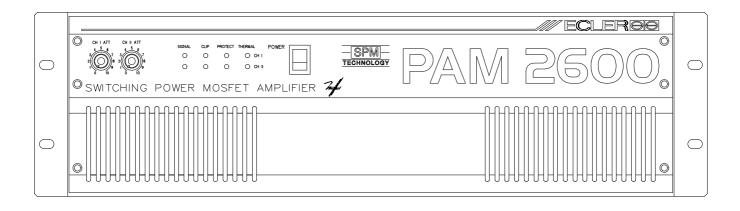
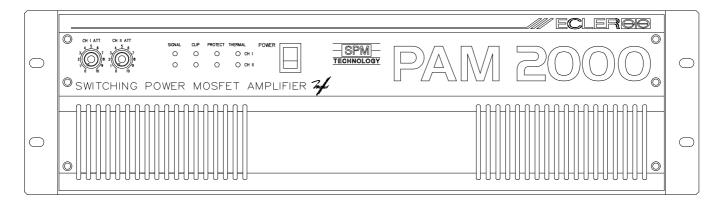
# PAM2600/2000

# **SERVICE MANUAL**



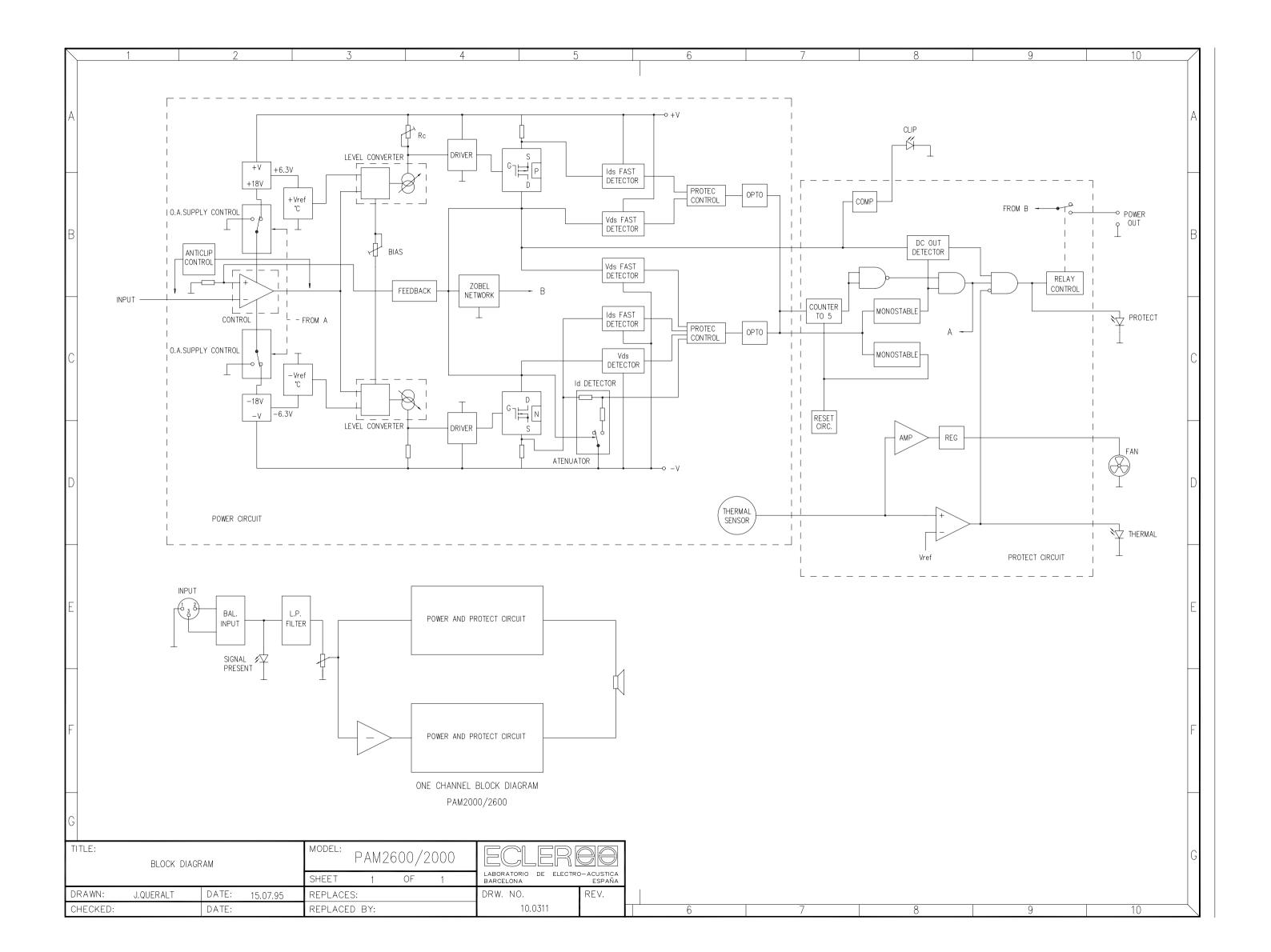




## SERVICE MANUAL PAM2600/2000

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### MODULE CIRCUIT 11.0504B OPERATION - DESCRIPTION

The control element is the operational NE5534. This is a very low noise operational, especially designed for very high quality applications in professional audio equipment, control equipment and telephony channel amplifiers.

The operational is internally compensated for a gain equal to or higher than three. Frequency response can be optimized with an external compensation capacity, for several applications (unity gain amplifier, capacitive load, slew-rate, low overshoot, etc...).

### Characteristics:

Small-signal bandwidth: 10Mhz

Output drive capability:  $600\Omega$  10V(rms) at  $Vs=\pm 18V$ 

Input noise voltage: 4nV/ Hz DC voltage gain: 100000√ AC voltage gain: 6000 at 10KHz Power bandwidth: 200KHz

Slew-rate: 13V/µs

Supply voltage range: ±3 to ±20V

POWER SOURCE STRUCTURE

### **POWER SUPPLY**

The BF871 and BF872 transistors are mounted in a common base configuration, in a current source structure. The current sources have a double function: polarizing the gate-source links in the MOSFETs to the limit of the conduction and moving the voltage variations at the operational output which are refered to ground to voltage variations refered to high voltage power supply. The polarization point is calculated so the voltage dropout in Rc(R112+R111) is the limit voltage of conduction of the MOSFETs ( $\approx 2$  to 3V), enough to carry the bias current. If we modulate in AC the base-emitter voltage, the Ic and VRc will vary proportionally. In our configuration, as the reference voltage Vref is constant (it is a part of the operational power supply), we add the operational output voltage to the transistors emitter through Re (R107-R108).

The Rc value fixes the source output impedance. We do not recommend to raise it higher than  $1K\Omega$  because of frequency response and slew rate reasons. This voltage circuit's gain is, as usual in a common base configuration with Rc/Re emitter resistor, 0.45.

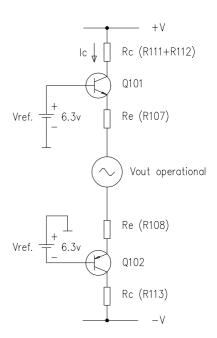


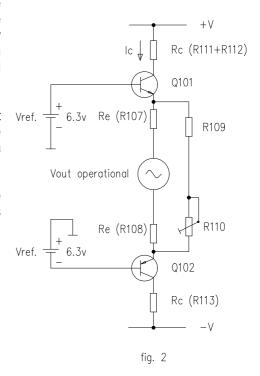
fig. 1

### **BIAS CURRENT ADJUST**

POWER SOURCE STRUCTURE AND BIAS CURRENT ADJUST

The bias current adjust is performed through the variable resistor connected between the emitters of the current sources R110 (5K $\Omega$ ). It delivers a supplementary current (it does not go through the operational) which simultaneously increases the voltage which falls in the Rc load resistors.

This is the easiest way of acting with just one adjust over both branches at the same time. In order to adjust the bias current the adjustable resistor must be varied until a current of about 80mA circulates through each MOSFET. So, for instance, for a PAM2600 in which there are six MOSFETs it will be 80 x 6 = 480mA. The bias current depends on the MOSFETs temperature and the stabilizing circuit transistors temperature.



### TEMPERATURE STABILIZING CIRCUIT

Temperature affects MOSFETs conduction in two different ways: first, the conduction threshold voltage has a negative temperature coefficient; second, the drain-source conduction resistance increases with temperature. Depending on which of the two things is predominating the temperature coefficient of the drain can be positive or negative. In our case, in which the gate-source voltage in the MOSFETs is very low when they conduct, the temperature coefficient of drain current -which is positive- is predominating.

To avoid thermal runaway in the polarizing current we must decrease the gate-source voltage as the MOSFETs get hot. Temperature stabilization is performed by modifying the reference voltage of both sources. If the temperature increases the Vref must decrease so that Ic and VRc decrease and, as a consequence, the gate-source voltage also decreases.

The circuit used is shown in figure 3. The base-emitter Vbe temperature/voltage feature is used to obtain the final result we need. The main idea is adequately choosing R1 and R2 to obtain the right temperature coefficient.

### TEMPERATURE STABILIZING CIRCUIT

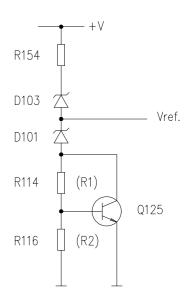


fig. 3

### SYMMETRY ADJUST

The threshold voltage varies much, even between MOSFETs of the same kind. When connecting them in parallel we must be careful that they all have the same conduction current if we want equal currents circulating in all of them. If the conduction voltage of P an N channels MOSFETs is not the same they will conduct different currents, even when we apply identical gate-source voltages. As the bias current of the N MOSFETs must be identical to the one of the P MOSFETs the feedback will correct the continuous voltage at the operational output to polarize the MOSFETs with different voltages until both conduct equal currents.

If the operational output is not 0 V its capacitity to give voltage and current is not the same in both senses. To avoid this we must put a symmetry adjust. It is just an adjust which allows to vary the collector resistance of one of the current sources (R111).

The symmetry adjust does not correct the asymmetrical clipping saturation of the power amplifier with real load. This happens because the conduction resistors (Ron) of the MOSFETs N and P are not equal. Channel P has a higher Ron than channel N. This characteristic depends on the MOSFET's physical construction.

### SYMMETRY ADJUST AND DRIVER

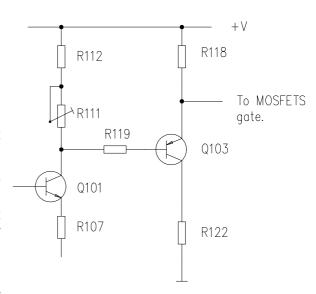


fig. 4

### POWER MOSFETs

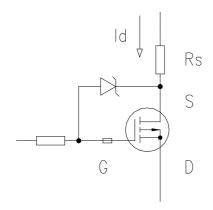
The MOSFETs used are IRFP9240 (P) and IRFP240 (N). They are assembled in a common source configuration so they can be completely saturated.

This kind of configuration has two drawbacks compared to a common drain one: less stability (because of the configuration gain itself) and high output impedance in open loop.

The source resistances  $(0.22\Omega)$  are needed for the MOSFETs to work in parallel. E.g.: Two MOSFETs excited by the same Vgs voltage (gate-source voltage) of 5V. If they have different transconductance curves (Id function Vgs) they will conduct different drain currents; let's say 1A and 3A. The second one will dissipate more power and will get hotter.

The use of source resistances tends to match the current that each of the MOSFETs connected in parallel is conducting.

This resistance performs a negative feedback on the gate, lowering down the Vgs, relating to the drain current; like this:



The higher the Id, the lower the Vgs voltage. The gate is protected by a zener, preventing a possible overload during an unexpected change from overload to real clipping.

Given the high input impedance and the broad frequency response of the MOSFETs there is a high risk of self-oscillations if all gates are excited connected to the same node. Intercalating serial resistances and ferrite beads at the gate this possibility is minimized, because the Q of the LC network made by the inductances and gate-source capacity is reduced.

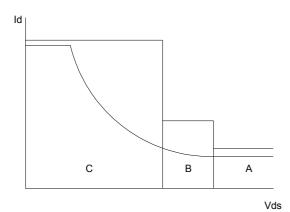
### PROTECTION CIRCUIT

The protection circuit monitors the dissipated power at the MOSFETs stage. It has two basic parts: MOSFET Id current detection.

MOSFET Vds voltage detection.

The goal is limiting the MOSFET so it works inside an area close to the SOA, as indicated in the figure. We chose channel N because, due to construction reasons, its SOA is lower.

ZONE A. This zone is for very low loads, around  $0\Omega$ . As the load voltage is very low, the voltage held by the MOSFET will always be high. The protections should be activated with very low current.



Fast protections and some of the slow ones are working in this zone. The circuit that configures the fast ones is made of: D120, D121, D123, R174, R175, R176, R177, R178, R179, C127, Q122 and Q123 for the N channel. There is also an equivalent circuit in the P channel. These start working when there is a sudden current variation because of a shortcircuit or a transitory. The reaction time -from the exact moment when these things occur to when the current stops circulating through the MOSFETs- is about  $80\mu s$ .

The time constant is given by C127, R174 and R179 and the load circuit made by the LED diode of the IC104 (opto-coupler).

Please note that in order for the protection to be activated Q122 and Q123 must conduct simultaneously, through which R174 is linked to negative power supply, being C127(1 $\mu$ F) loaded very quickly through this resistance, activating the LED of the opto-coupler, sending a pulse to the protection circuit, which will open the corresponding channel's relay, being this way the output from the power amplifier disconnected from the load (0 $\Omega$ ), in this case. Q122, together with the zeners and the base polarization resistances, configure the voltage detector (this group is in parallel with the Vds voltage of the N MOSFET).

Q123, together with the resistances which make the base divider, configure the current detector (this divider takes its voltage from one of the source resistances of a N MOSFET, which is proportional to the current circulating through itself).

The threshold separating zone A from zone B is determinated by the D125 zener. When this zener stops working and there is no current circulating through it because the Vds voltage is lower (let's remember this circuit is also in parallel with this voltage) or, what is the same, the load voltage grows because it is not  $0^\circ$  anymore and has a given value, like  $0.5\Omega$  to  $1\Omega$ , and the help given by D126 stops so more current will be needed for the shot. We have climbed the first stair of the stairway of the SOA graphic.

When the zeners D124 and D118 stop working because the load voltage goes on growing (values higher than  $1\Omega$ ) or -what is the same- the Vds decreases, the Q125 transistor does not receive current anymore in its base and so it is shorted, allowing Q124 to enter conduction. This way R172 stays in parallel with the base-emitter of Q121, making up a voltage divider with R173. This divider will climb another stair of the stairway and enter the ZONE C.

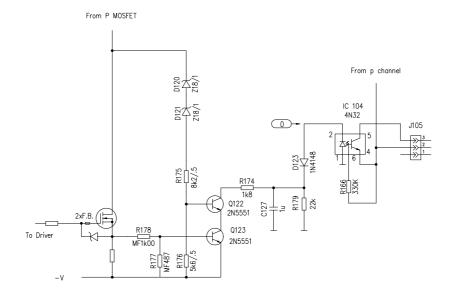
The link between the module's protection circuit and the relays' control circuit is made through IC103 and IC104 which are, as mentioned earlier, opto-couplers, just to insulate the existing high voltages at the power amplifying module,  $\pm 63V$  in the case of the PAM2600, and the power supply voltage of the existing logic circuits in the relays' control card.

Once the pulse generated by the protections is detected, the control circuitry resident in the protection card, appart from opening the corresponding relay, returns the signal A.O. SUPPLY CONTROL to the module, which cuts by means of Q119, Q120 and IC102 the operational's power supply.

This is the way to insure a fast and safe cut of the Id current in the MOSFETs (around 80µs time), because they stop receiving their respective reference voltages and, consequently, their Vgs polarization voltages so they are cut. The circuit is shown in figure 9 and its operation is very simple.

When the A.O. SUPPLY CONTROL (+10V) signal appears, the Q119 transistor starts conducting, shortcircuiting to ground the positive power supply of the operational. On the other hand, the signal is also applied to the IC102's LED (opto TIL112 (4N35)), which puts its internal transistor and Q120 into conduction, connecting the negative power supply of the operational to ground.

N CHANNEL FAST PROTECTIONS CIRCUIT



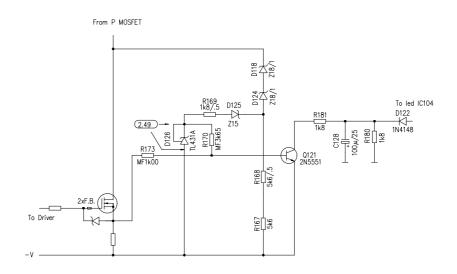


fig. 6

# SLOW PROTECTIONS CIRCUIT (B) STEP SOA DIAGRAM

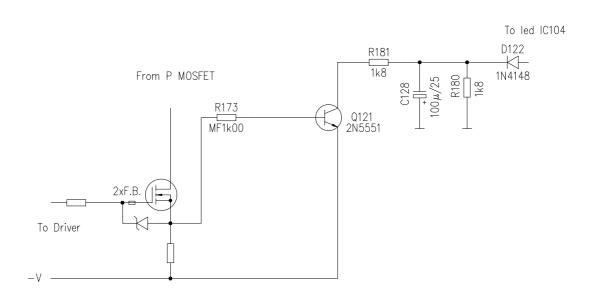
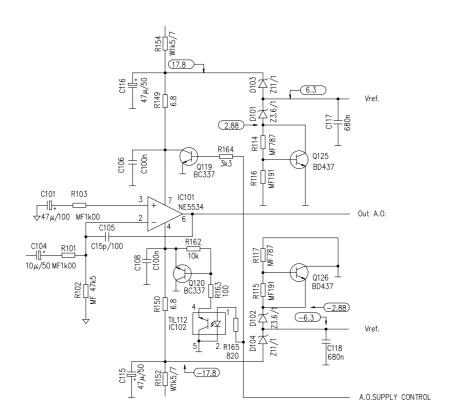


fig. 7

# To led IC104 R173 MF1K00 R173 MF1K00 R173 MF1K00 R174 R175 R181 R181

fig. 8

### OPERATIONAL AMPLIFIER POWER SUPPLY CONTROL

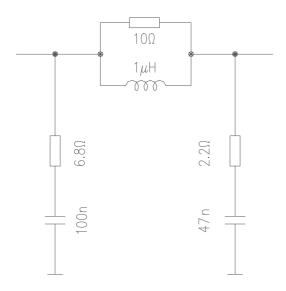


### **ZOBEL NETWORK**

This circuit tries to get a constant load impedance for the power module, in spite of the amplifier's load and frequency, to avoid phase shifting of the feedback signal.

The values have been experimentally calculated through a study with square signal by trying to minimize the power amplifier's ringing with very capacitive loads  $(2,2\mu F//4\Omega)$ .

The Zobel Network eliminates possible oscillations of the MOSFETs between 5MHz and 10MHz, too. This is why it must be physically placed at the module's output, avoiding long wiring. Great care must be taken for the signal not to be too shifted at the output, because the feedback could turn negative.



### **FEEDBACK**

The whole amplifier is compensated with just one capacity, which places the amplifier's general pole at:

1
$$Fp = ---- = 140KHz$$

$$2^*\pi^*Rf^*Cf$$

$$Rf = R106 \qquad Cf = C109-C110$$

### PROTECTION CIRCUIT 11.0411 OPERATION - DESCRIPTION

The circuit is configured by:

- A POWER SUPPLY.
- A THERMAL PROBE DC AMPLIFIER.
- A TEMPERATURE DETECTOR.
- A DC OUT DETECTOR PER CHANNEL.
- A CLIP CIRCUIT PER CHANNEL.
- A RESET (TURN OFF/TURN ON) CIRCUIT.
- A BINARY COUNTER PER CHANNEL.
- TWO MONOSTABLE CIRCUITS PER CHANNEL.

The circuit power supply is performed through various sources: +V, module's power supply. This voltage feeds the relays circuit, manual reset circuit and part of the clip circuit. Alternate voltage from a transformer's secondary (manual reset circuit).

There is also a stabilized 10V power supply which feeds the card's circuitry, made of IC301 (7805) plus the zener D302 (Z4.7)  $4.7+5 \approx 10V$ . We will also need a regulated power supply to get 14Vmax at 0.7A, which can be obtained with IC302 (7805) plus an auxiliary circuitry that will be analysed below.

The cooling fan speed is automatically regulated in relation to the power module's temperature, which is read by a thermal probe (LM35D), jointly linked to the heat sink.

This high sensitivity thermal probe gives variations of 10mV for every  $^{\circ}$ C. This voltage is picked up and amplified by the IC305 (LM358). Of course, there is a probe for each L and R heatsink. The output of both amplifiers is linked through two diodes D304 and D305, making an O gate, whose cathodes go to the regulator, applying the DC of any of them to the regulator. This provides a variable voltage at its output which oscillates from a minimum of approximately 7V for a temperature of 20 $^{\circ}$ C (cold heatsink) to a maximum of 14V for temperatures of 76 $^{\circ}$ C or higher.

The gain of the amplifiers has been calculated for this temperatures window. The maximum voltage allowed by the heatsink in order to work properly is 14V. This maximum is given by the zener D305 (Z9.1/1); as the regulator is a 7805 the voltage will be -as maximum- 9.1+5 = 14.1V. When the zener is not working (not enough voltage) the voltage on the fan will be the output amplifiers', less 0.6V (diodes fall), plus the 5V of the IC302.

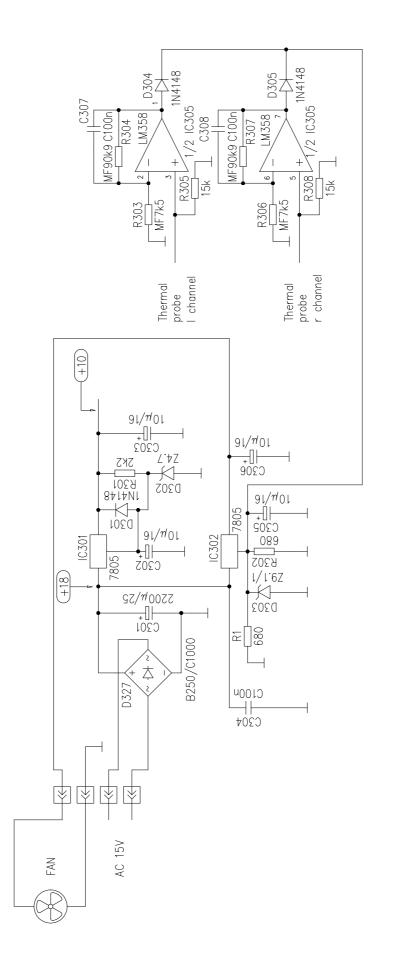


fig. 1

### TEMPERATURE DETECTOR

This circuit is calculated to operate over the output relay opening it if any of both modules' temperature excedes  $90^{\circ}$ C, approximately. It is made with a comparator per channel (L-R), resident in the same IC306. Both share a reference voltage provided by D306 (TL431A), which gives excellent stability at that voltage  $\pm 1\%$ . These comparators reveive, like the DC amplifiers, the signal from their probes, comparing them with the Vref.Once this voltage is surpassed by any of both probes, the output of the corresponding comparator is balanced to the power supply (+10V), acting through D307, R318, D308 and R319 over the respective bases of transistors Q301 y Q307, which makes the corresponding relay open. This output is also connected to the THERMAL LEDs, which light up as the relays are open.

Note that each time the relay is open through any of the variables which act upon it the PROTECT LED must light up. The circuit acting over this LED is made of R327, R328, R329, R4, R5 and Q303. When Q302 stops conducting (open relay), Q303 receives its base current through R327, R326, R6 and the relay's coil, putting this transistor into saturation. This way the LED is linked to the power supply (+V) by means of the group of resistances R328, R329, R4 and R5.

TEMPERATURE DETECTOR CIRCUIT

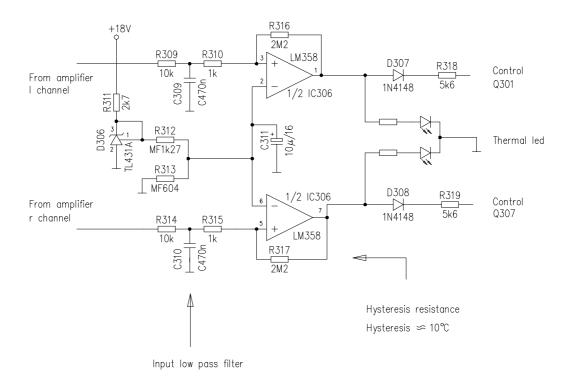


fig. 2

### RELE CIRCUIT AND PROTECT LED

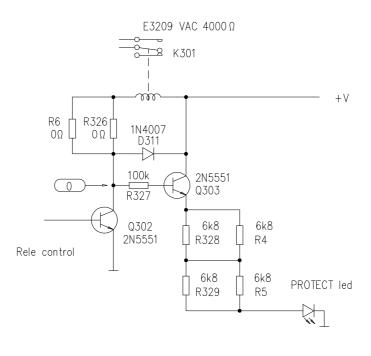


fig. 3

### DC OUT CIRCUIT

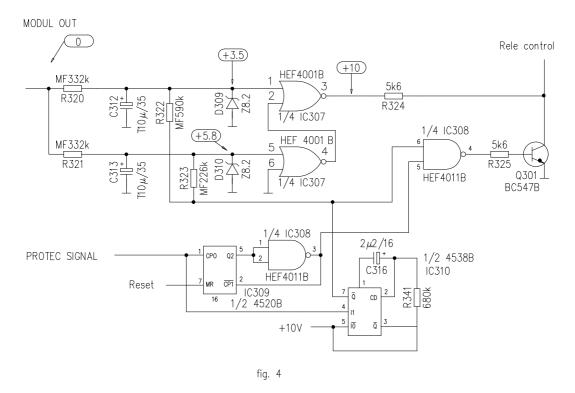
The circuit shown in the figure corresponds to the DC OUT of channel L. The goal of this circuit is protecting the loudspeakers when, because of a module fail, there is some DC appearing at the output. The voltages indicated in the figure correspond to rest state and they are given by the dividers made of R320-R322 and R332-R323.

The resistances R323-R322 are linked by their extreme to the leg 7(Q) of the monostable IC310 (4538), which has +10V at rest state. On the other hand R320-R321 are linked by their extreme to the L output, which, in these conditions, has 0V respect to ground. If we apply Ohm's Law to these dividers we will obtain the above mentioned voltages.

Let's remember briefly the function of a NOR gate like the HEF4001B.

А	В	С
0	0	1
0	1	0
1	0	0
1	1	0

Let's suppose there is a continuous voltage appearing at the module output, because of any malfunction. This makes the voltage dividers lose balance, no matter if the above mentioned voltage is positive or negative, the gate goes to 0V, the base Q302 loses the current stream and, as a consequence, the relay K301 opens. The aim of the zeners D309 and D310 is protecting the gates, avoiding the voltage in them to be higher than 8.2V when the voltage is positive and lower than -0.6V when it is negative; as you can see, the zener plays the role of a diode.

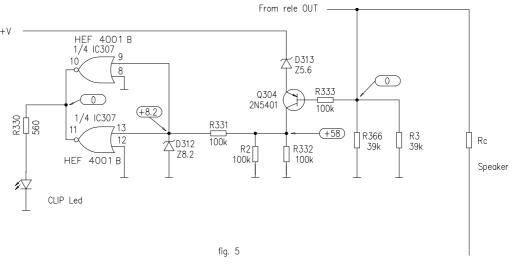


### **CLIP CIRCUIT**

The other half of IC307(4001) is used in the clip circuit. Given that we have two gates more and we just need one for our purposes we will connect them in parallel for a higher output current and a more effective LED lighting up.

The clip threshold or point where we want the LED to light up is determined by the zener D313. In our case it is between 0.5 and 1dB or, what is the same, when the output signal level over the load reaches a value close to that of the power supply (+V), exactly Vout = V - 5.6, moment in which Q304 loses the base-emitter voltage stopping conduction; this makes the zener D312 voltage disappear (0V) and the output from IC307 go to "1" logic (+10V), making the LED light up.

CLIP CIRCUIT



To other channel

### GENERAL RESET CIRCUIT (TURN OFF/TURN ON)

TURN OFF RESET. This circuit starts working when the AC current from the transformer secondary disappears or, what is the same, when we turn the power amplifier off by pushing the power off switch, actually disconnecting it from mains.

Circuit operation: The AC signal present at the anode D321 is rectified by this, attenuated and filtered by R13, R348, R347 and C322, apllying it to the base of Q306, which is conducting into saturation and, as a consequence, Q305 is cut. When this signal disappears Q306 is cut and then Q305 has its base feeded through R345, R346 and R14 from the +V power supply, which has begun to lose voltage -because we have just cut the mains- but, because of the high capacity value of the filter condensers, there is enough time to saturate Q305, which puts the resistances R15 and R344 ( $50\Omega$ ) in parallel with the power supply (+10V) of the logic circuitry, completely discharging the capacities of the circuit, leaving it ready for a new reset pulse -the connection one-, what warranties the new turn-on, even with very short time intervals (.1s) between turn-off and connection pulses.

10V FAST DESCHARGE CIRCUIT

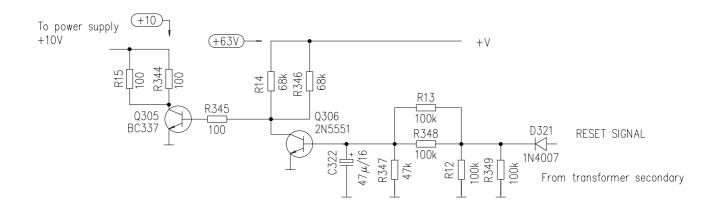


fig. 6

### CONNECTION RESET

This is made of C315, R336 and D314. It is the classical reset circuit, used in lots of applications.

In the exact connection moment the condenser C315 is not charged, with a high amount of current circulating through it, or a high voltage in R336. This current decreases as the condenser is charging until it disappears. At the same time, the voltage -in the extremes- of the resistance goes from maximal, in the beginning, to 0V. This way we get a pulse whose duration depends on the time constant RC. The aim of the diode D314 is a fast discharging of C315 during disconnection.

### **BINARY COUNTER HEF4520**

This is a 4-bit double binary counter. Configured in a way in which when there is the binary code equivalent to decimal number 5 at its output -so this is 1 0 0- it is blocked in this position, until it receives a new MR reset pulse. The blocking action is performed by the NAND gate between legs Q2 and CP1. At this state Q2 becomes "H" one logical, the NAND changes its state putting the leg CP1 to "L" zero logical and -as you can see in the table of functions- the mode can not change in this conditions.

CPO	CP1	MR	MODE
1	Н	L	counter advance
L	1	L	counter advance
ļ	X	L	no change
Х	1	L	no change
1	L	L	no change
Н	1	L	no change
Х	X	Н	Q0 to Q3=low

The general turn-on reset initializes the counter. Every time it receives a pulse from the module opto-couplers because of a protections shot it is counted. If during an interval of approximately 5 minutes it does not receive any other pulse, the counter will go back to the original zero state, because it receives a new MR reset pulse from the monostable IC311, whose time constant is approximately 5 minutes (R342,C319). This monostable begins counting from the very first pulse received by the counter, because both are linked to the PROTECT SIGNAL from the module and, consequently, activated at the same time.

If during this time interval (about 5 minutes) a minimum of 5 successive pulses are received, these will make the counter block at that position. This translates into a logical "1" at the Q2 leg of the counter, a "0" at the NAND (IC308) output; this zero makes a "1" at the output of the next NAND, giving a result of "0" at the collector of Q301, so Q302 is not conducting and the relay K301 remains open. It will stay this way until the reset from the monostable happens or there is a manual mains disconnection by pushing the power off button.

The reset circuit associated with the monostable is made of C320, D320, R339 and D318 (above we have always been refering to channel L). By means of diodes D317 and D318 we build an "O" gate, with which we apply any of the above mentioned reset pulses to the counter.

# BINARY COUNTER CIRCUIT AND RESET MONOSTABLE CIRCUIT

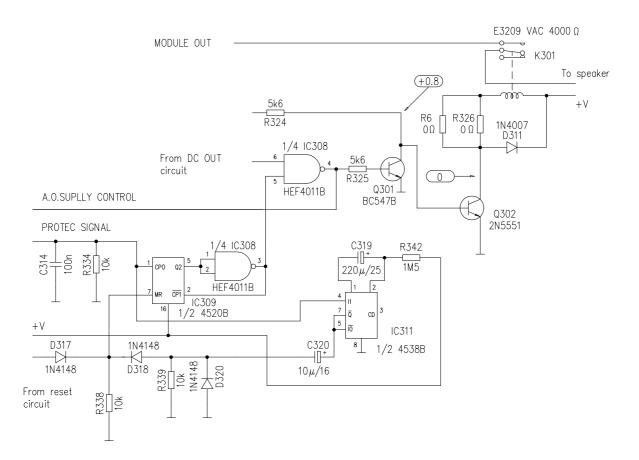


fig. 7

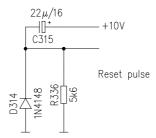


fig. 8

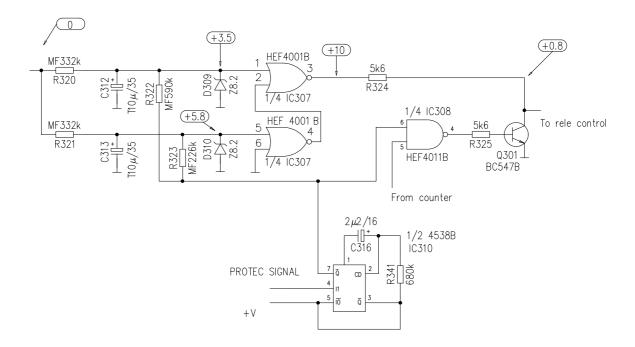
### STANDBY MONOSTABLE

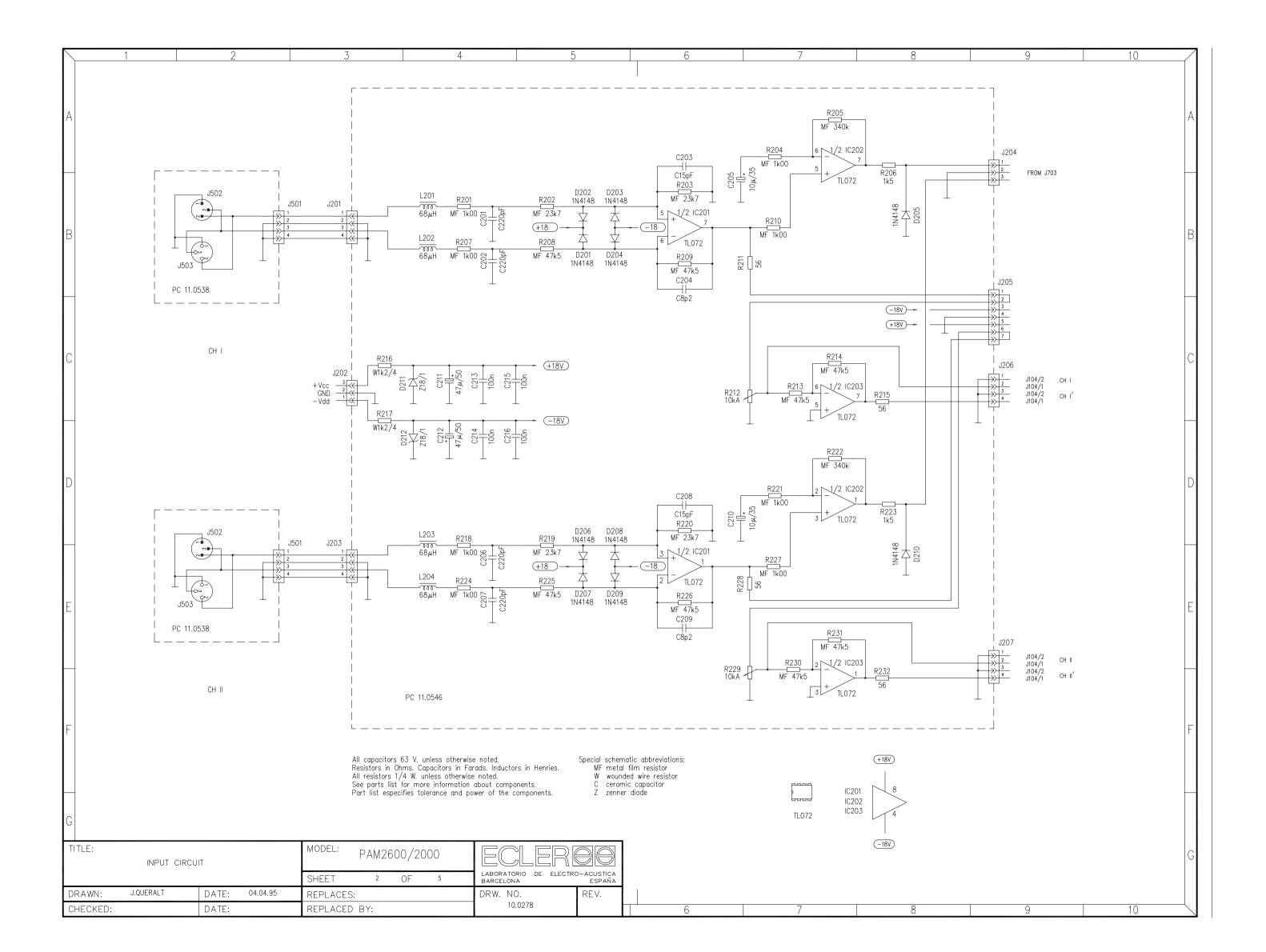
The only thing left is the function of the monostable made of IC310 (4538).

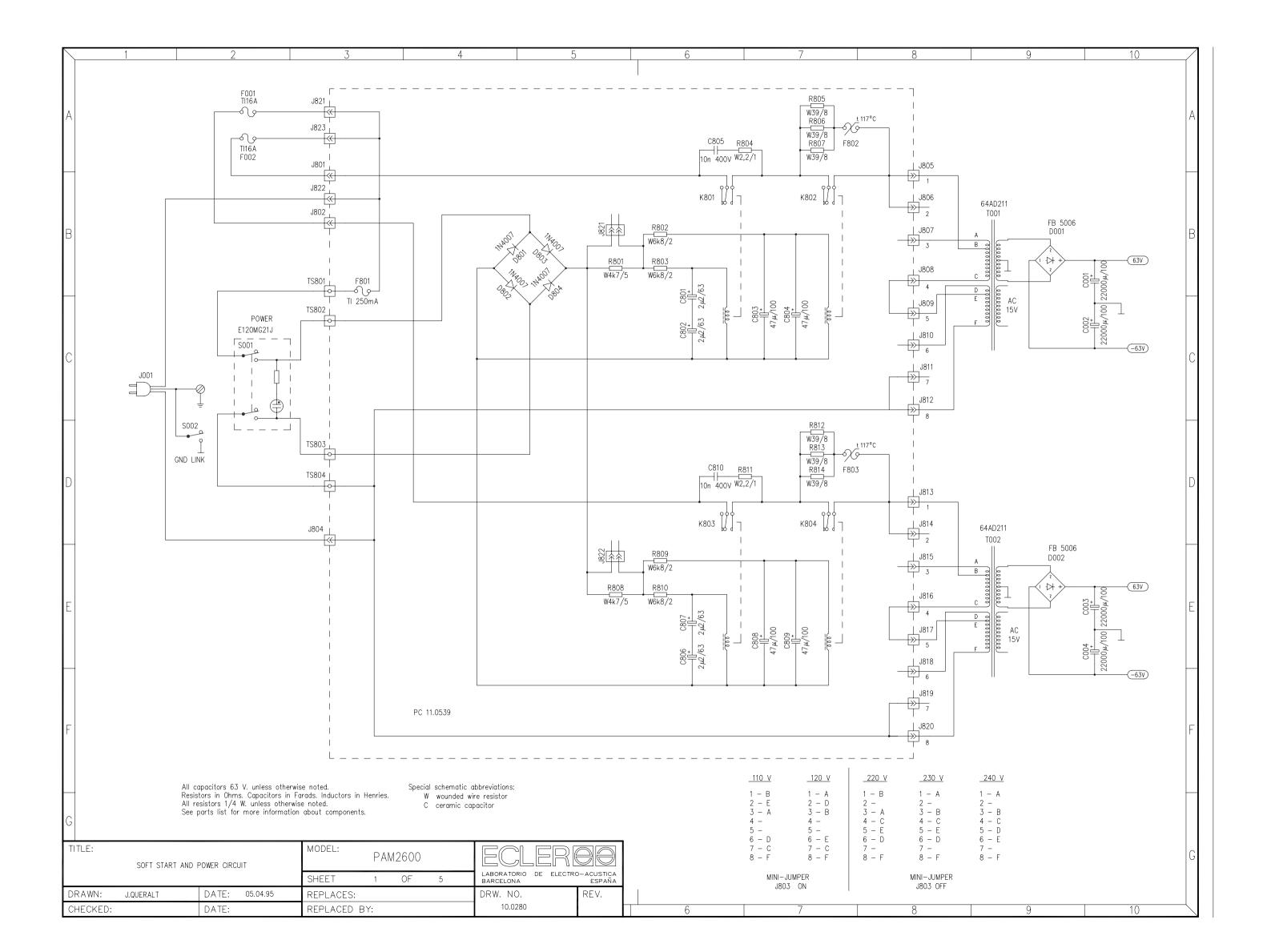
Like the counter and the monostable IC311 (4538), this circuit is connected to the PROTECT SIGNAL, too. Its output is "1" in rest state and becomes "0" during an approximate time of 1.3 seconds, which is given by the constant RC of the circuit R341 C316.

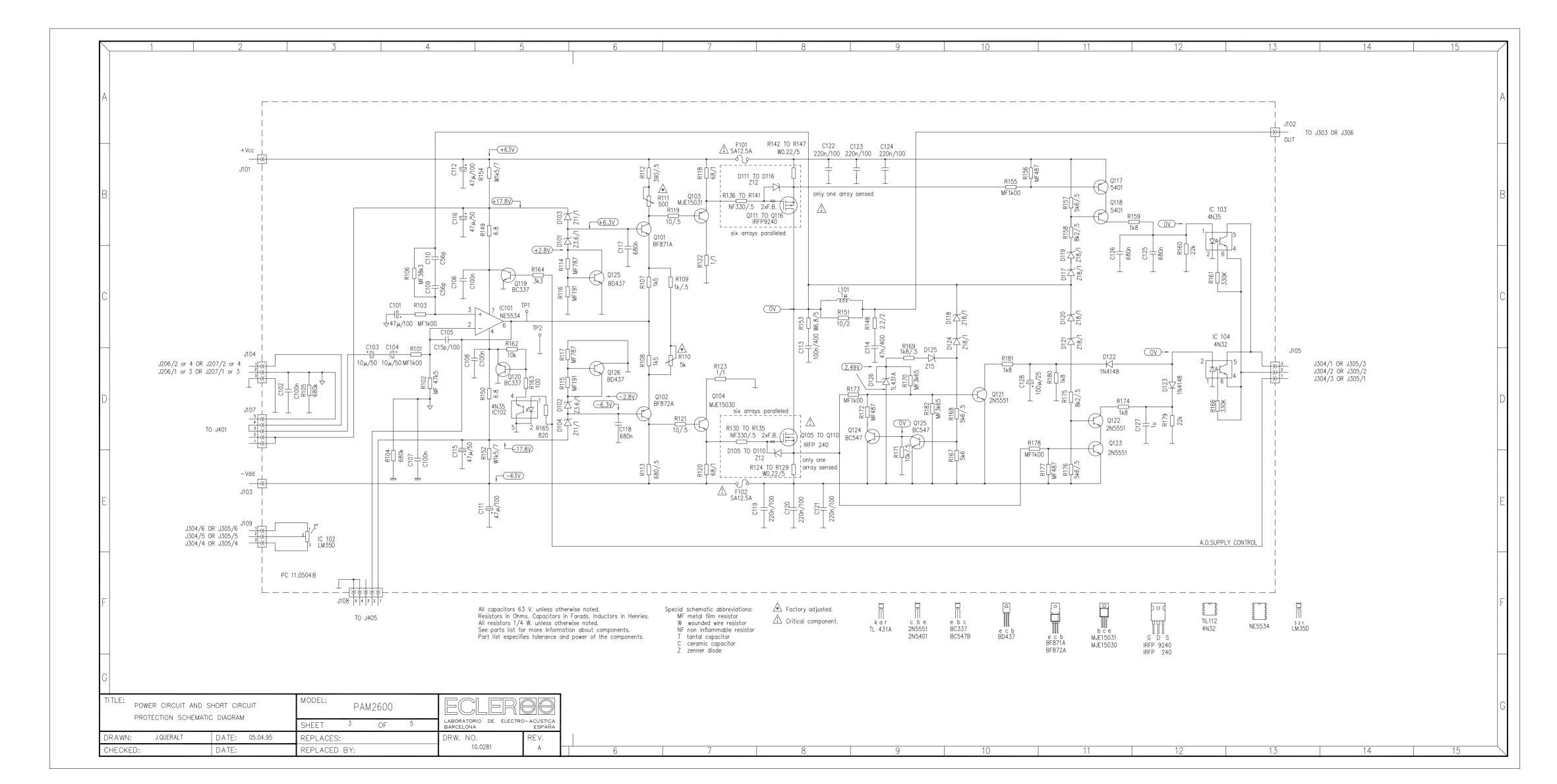
This leads to two situations: First, putting a "0" in one of the legs of the NAND (IC308) generates the immediate opening the relay, as we have seen before. On the other hand the voltage divider of the DC OUT circuit is put off balance. The monostable time is calculated to be long enough to unload the capacities of C312 and C313. This way we get a DC OUT circuit initialization as we had done a manual reset (disconnection from mains), causing the tipical turn-on STANDBY time for each of the disconnections of the relays because of the protections shooting. Let's take into account that the system is locked after the fifth disconnection.

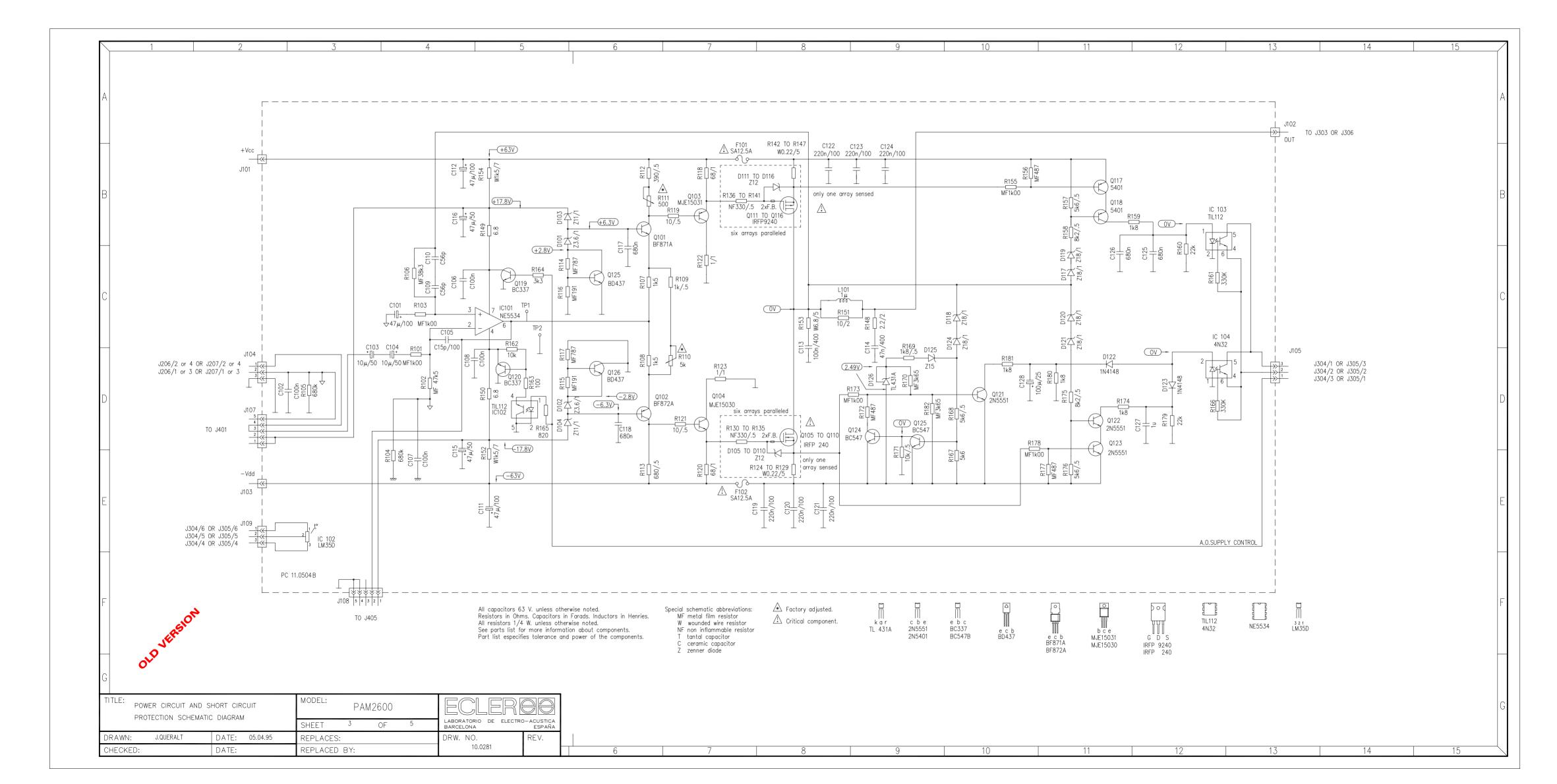
STANDBY MONOSTABLE

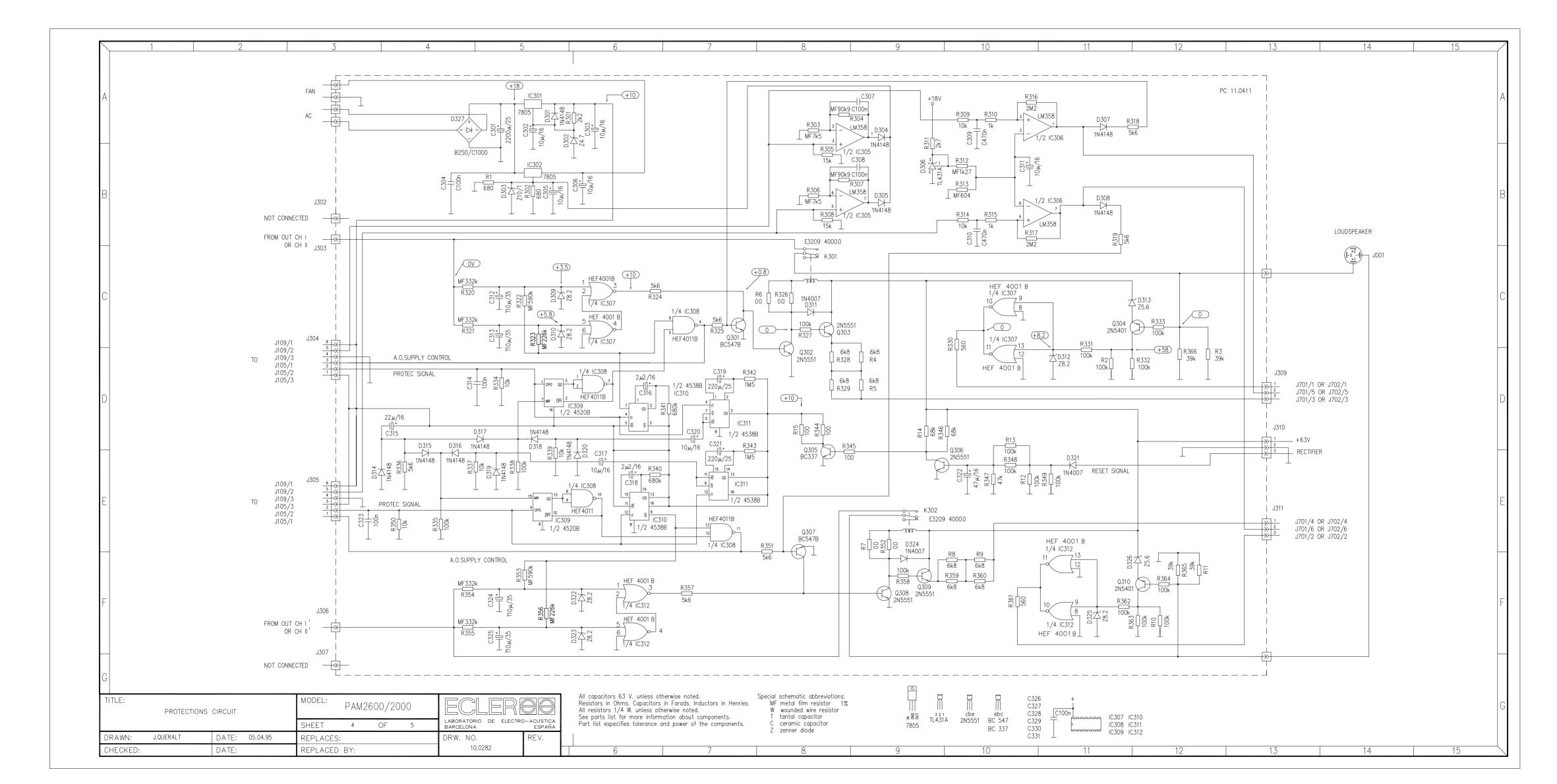


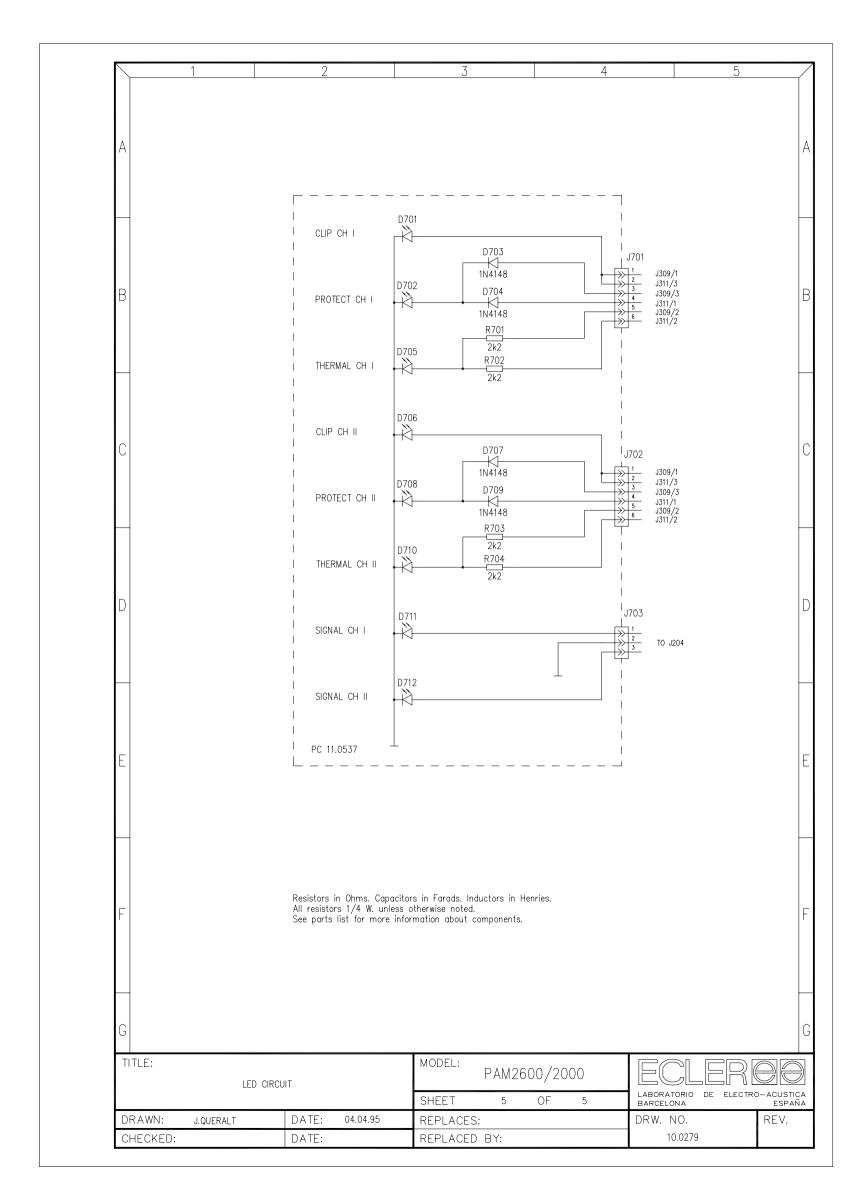


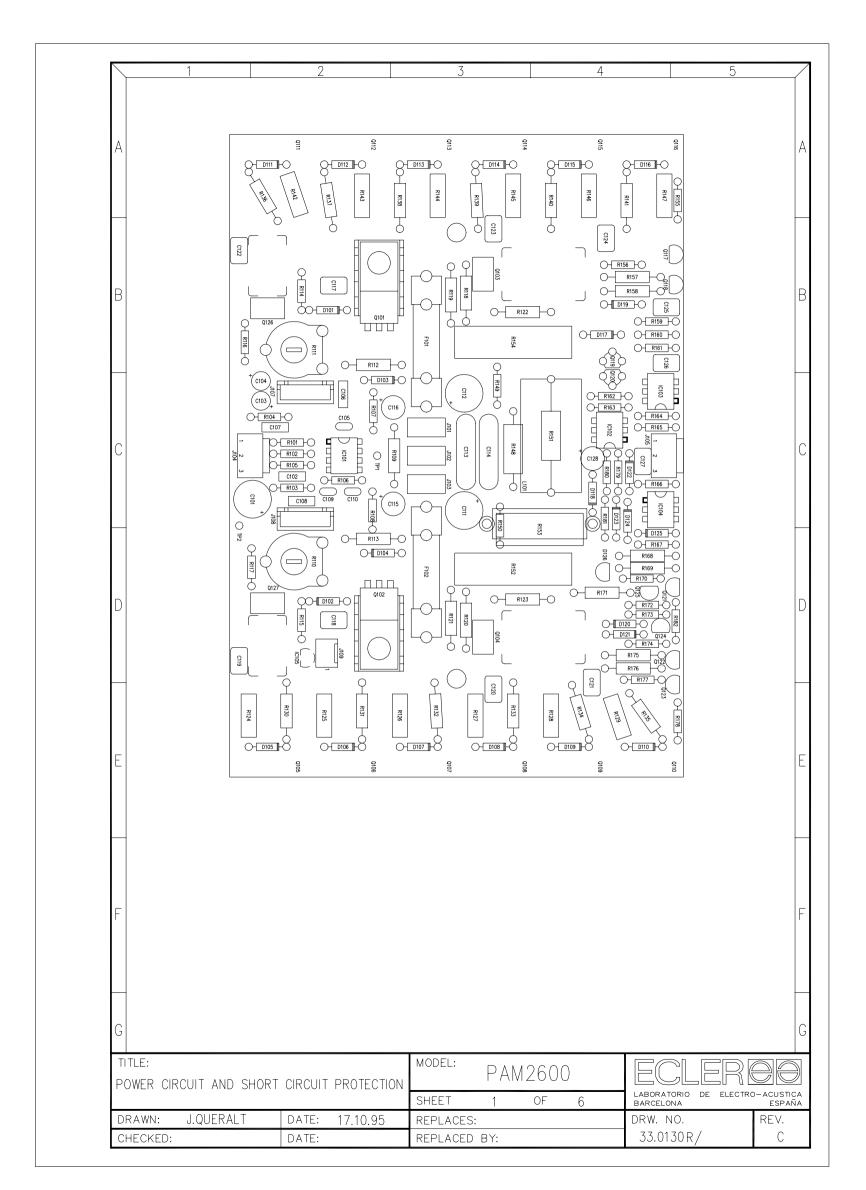


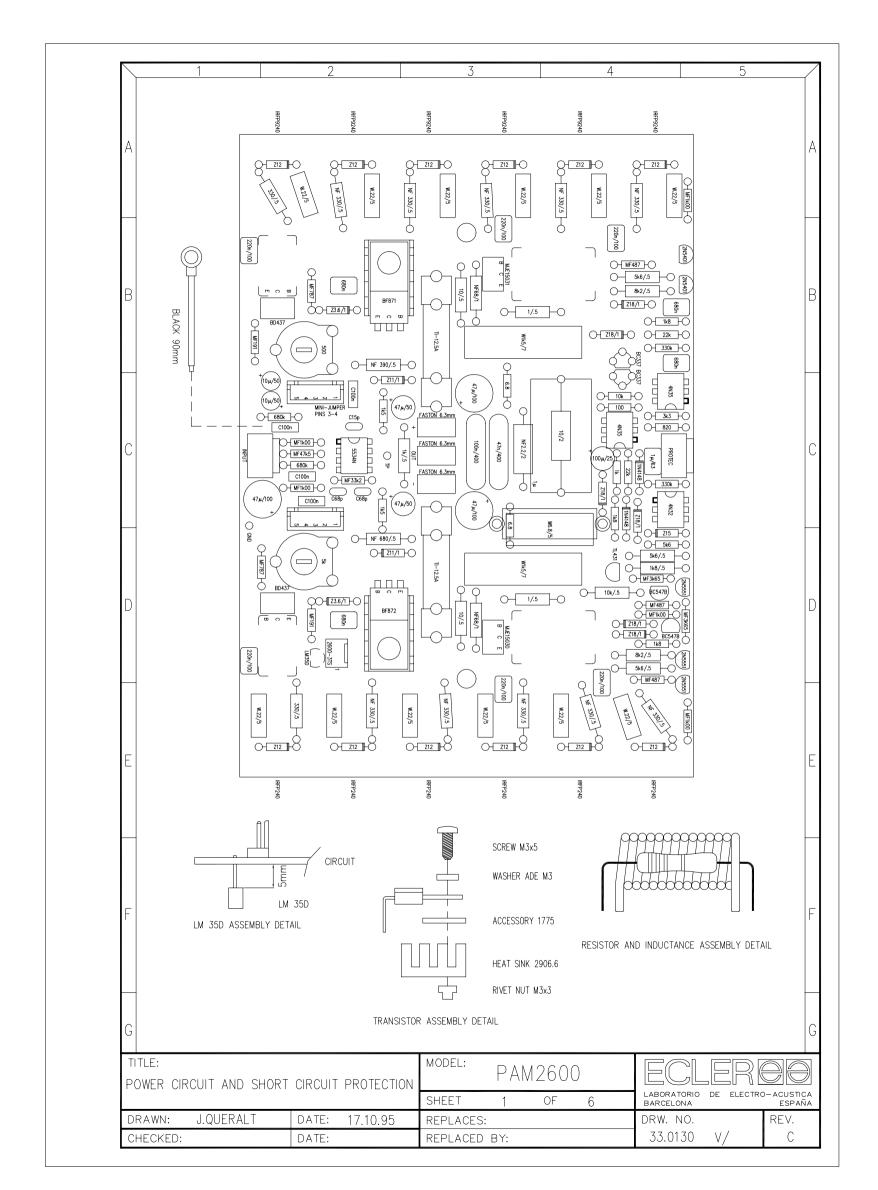












PARTS LIST: POWER CIRCUIT AND SHORT CIRCUIT PROTECTION

MODEL:PAM2600 DRW.N° 33.0130PL REV : A

DATE: 000621 SHEET 1 OF 4 REPLACED BY:

### REFERENCE VALUE

C101  $47\mu/100$ C102 C100n C103  $10\mu/50$ C104  $10\mu/50$ C105 C15p C106 C100n C107 C100n C108 C100n C109 C56p C110 C56p C111  $47\mu/100$ C112  $47\mu/100$ C113 100n/400 C114 47n/400 C115  $47\mu/50$ C116  $47\mu/50$ C117 680n C118 680n C119 220n/100 C120 220n/100 C121 220n/100 C122 220n/100 C123 220n/100 C124 220n/100 C125 680n C126 680n C127  $1\mu/63$ C128  $100 \mu / 25$ D101 Z3.6/1 D102 Z3.6/1 D103 Z11/1 D104 Z11/1 D105 Z12 D106 Z12 Z12 D107 D108 Z12 Z12 D109 D110 Z12 D111 Z12 Z12 D112 D113 Z12 Z12 D114 D115 Z12 D116 Z12 D117 Z18/1 D118 Z18/1 D119 Z18/1 D120 Z18/1 D121 Z18/1 D122 1N4148 D123 1N4148 D124 Z18/1 D125 Z15 D126 TL431 F101 TI-12.5A F102 TI-12.5A IC101 5534N IC102 4N35

PARTS LIST: POWER CIRCUIT AND SHORT CIRCUIT PROTECTION

MODEL:PAM2600 DRW.Nº 33.0130PL REV: A

SHEET 2 OF 4 REPLACED BY: DATE: 000621

### REFERENCE **VALUE**

IC103 4N35 IC104 4N32 IC105 LM35D

J101 FASTON 6.3mm J102 FASTON 6.3mm J103 FASTON 6.3mm

J104 B3P-VH J105 B3P-VH J107 B5B-XH J108 B5B-XH J109 2600-3TS Q101 BF871 Q102 BF872 Q103 MJE15031 Q104 MJE15030 Q105 IRFP240 Q106 IRFP240 IRFP240 Q107 IRFP240 Q108 Q109 IRFP240 Q110 IRFP240 Q111 IRFP9240 Q112 IRFP9240 Q113 IRFP9240 Q114 IRFP9240 Q115 **IRFP9240** Q116 IRFP9240 Q117 2N5401 Q118 2N5401 Q119 BC337 Q120 BC337 Q121 2N5551 2N5551 Q122 Q123 2N5551 Q124 BC547B Q125 BC547B Q126 **BD437** Q127 **BD437** R101 MF1k R102 MF47k5 R103 MF1k00

R104 680k R105 680k R106 MF38k3 R107 1k5 R108 1k5 R109 1k/.5 R110 5k R111  $500 \Omega$ R112 NF390  $\Omega$  /.5 R113 NF680  $\Omega$  /.5 R114 MF787  $\Omega$ R115 MF191  $\Omega$ R116 MF191 $\Omega$ R117 MF787  $\Omega$ R118 NF68  $\Omega$  /1

 $10 \Omega /.5$ 

NF68  $\Omega$  /1

R119

R120

PARTS LIST: POWER CIRCUIT AND SHORT CIRCUIT PROTECTION

MODEL:PAM2600 DRW.N° 33.0130PL REV : A

DATE: 000621 SHEET 3 OF 4 REPLACED BY:

### REFERENCE VALUE

R121  $10 \Omega /.5$ R122  $1 \Omega /.5$ R123  $1 \Omega /.5$ R124  $W.22 \Omega /5$ R125  $W.22 \Omega /5$ R126  $W.22 \Omega /5$ R127  $W.22 \Omega /5$ R128  $W.22 \Omega /5$ R129  $W.22 \Omega /5$ R130 330  $\Omega$  /.5 R131  $330 \Omega /.5$ R132 330  $\Omega$  /.5 R133  $330~\Omega$  /.5 R134  $330 \Omega /.5$ R135 330  $\Omega$  /.5 R136 330  $\Omega$  /.5 R137  $330 \Omega /.5$ R138  $330~\Omega$  /.5 R139 330  $\Omega$  /.5 R140 330  $\Omega$  /.5 R141 330  $\Omega$  /.5 R142  $W.22 \Omega /5$ R143  $W.22 \Omega /5$ R144  $W.22 \Omega /5$ R145  $W.22~\Omega$  /5 R146  $W.22 \Omega /5$  $W.22 \Omega /5$ R147 R148 NF2.2  $\Omega$  /2 R149  $6.8 \Omega$ R150  $6.8 \Omega$ R151  $10 \Omega / 2$ R152 W1k5/7 R153 W6.8  $\Omega$  /5 R154 W1k5/7 R155 MF1k00 R156 MF487  $\Omega$ R157 5k6/.5 R158 8k2/.5 R159 1k8 R160 22k R161 330k R162 10k R163  $100 \Omega$ R164 3k3 R165  $820 \Omega$ R166 330k R167 5k6 R168 5k6/.5 R169 1k8/.5 R170 MF3k65 R171 10k/.5 R172 MF487  $\Omega$ R173 MF1k00 R174 1k8 R175 8k2/.5 R176 5k6/.5

R177

R178

MF487  $\Omega$ 

MF1k00

PARTS LIST: POWER CIRCUIT AND SHORT CIRCUIT PROTECTION

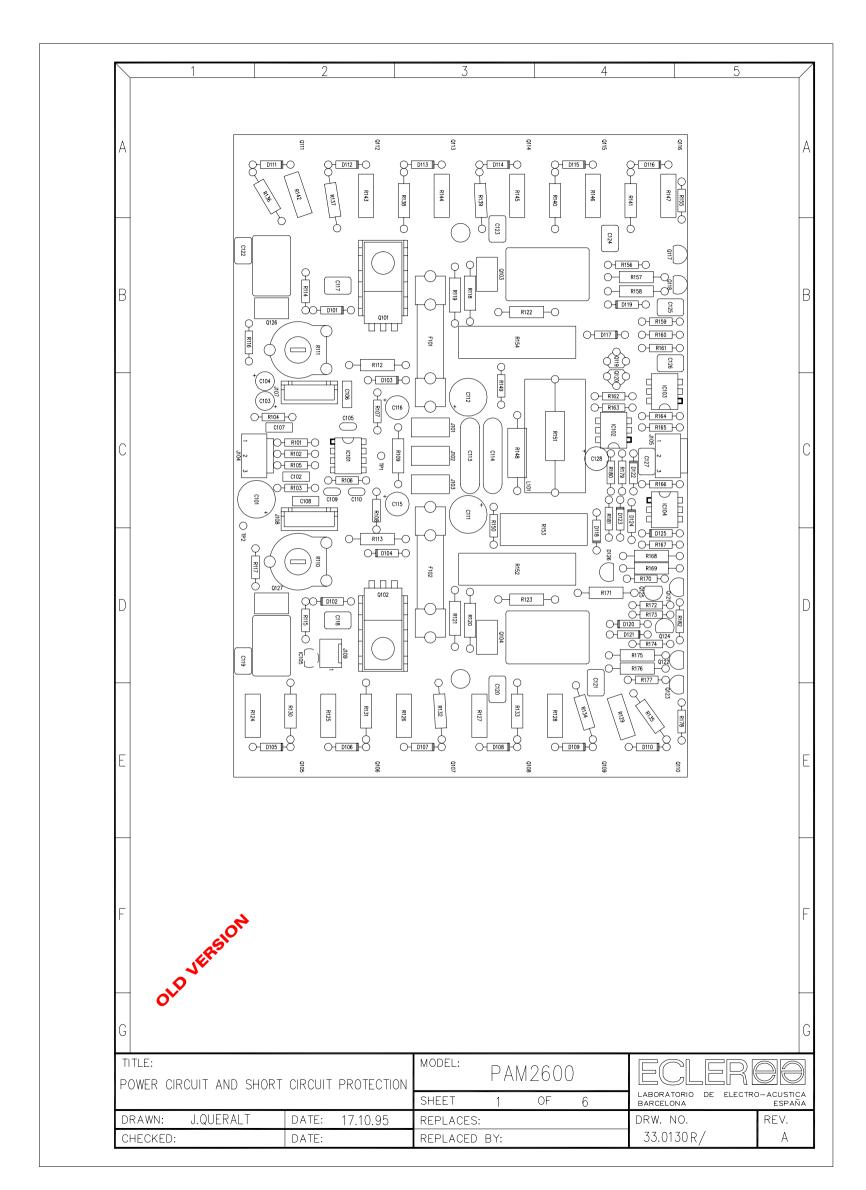
MODEL:PAM2600 DRW.N° 33.0130PL REV : A

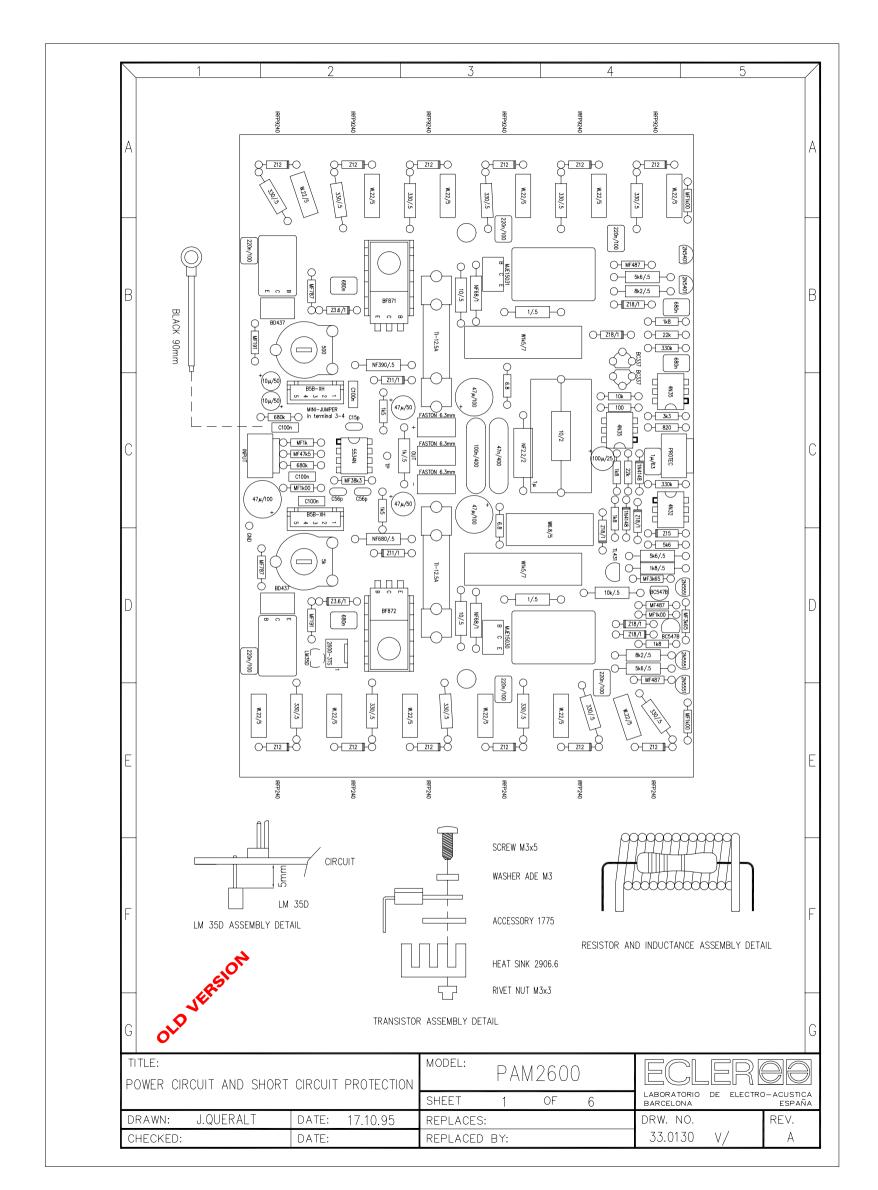
DATE: 000621 SHEET 4 OF 4 REPLACED BY:

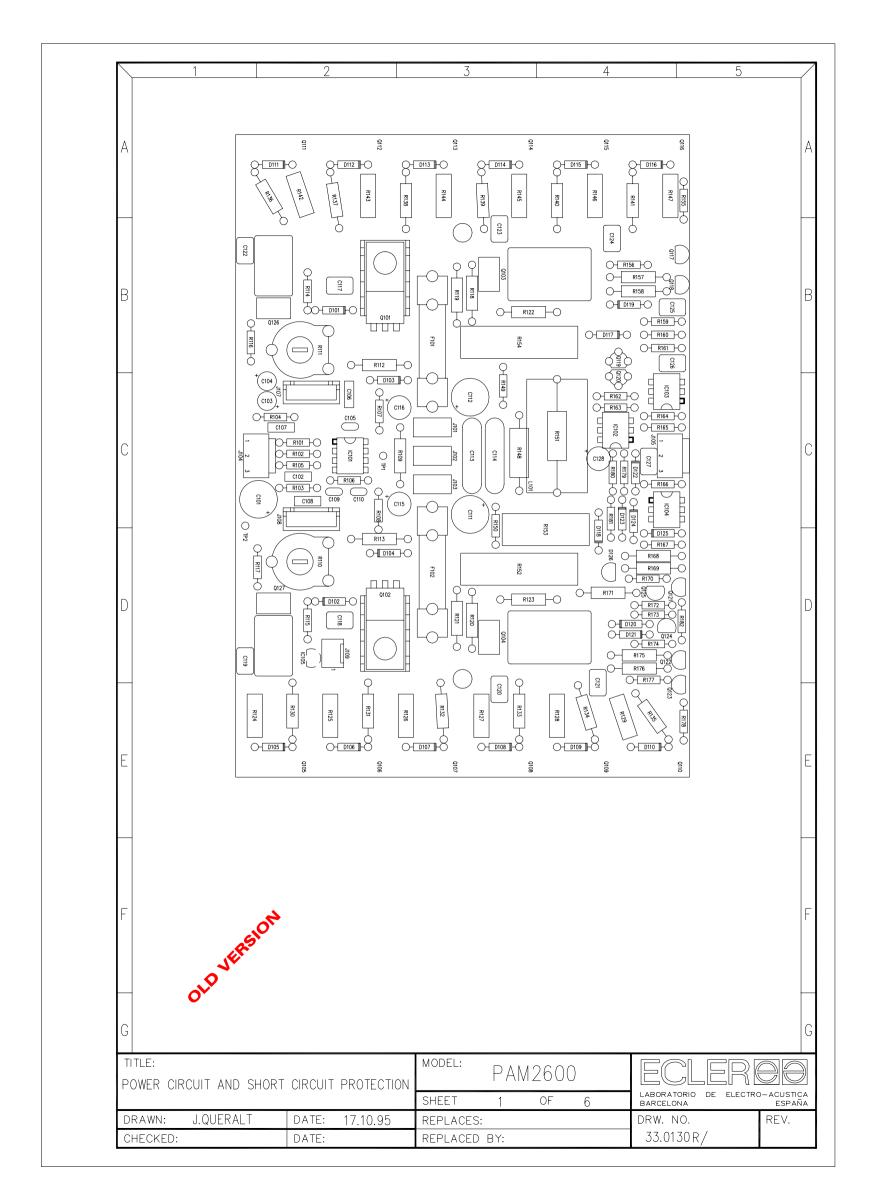
REFERENCE VALUE

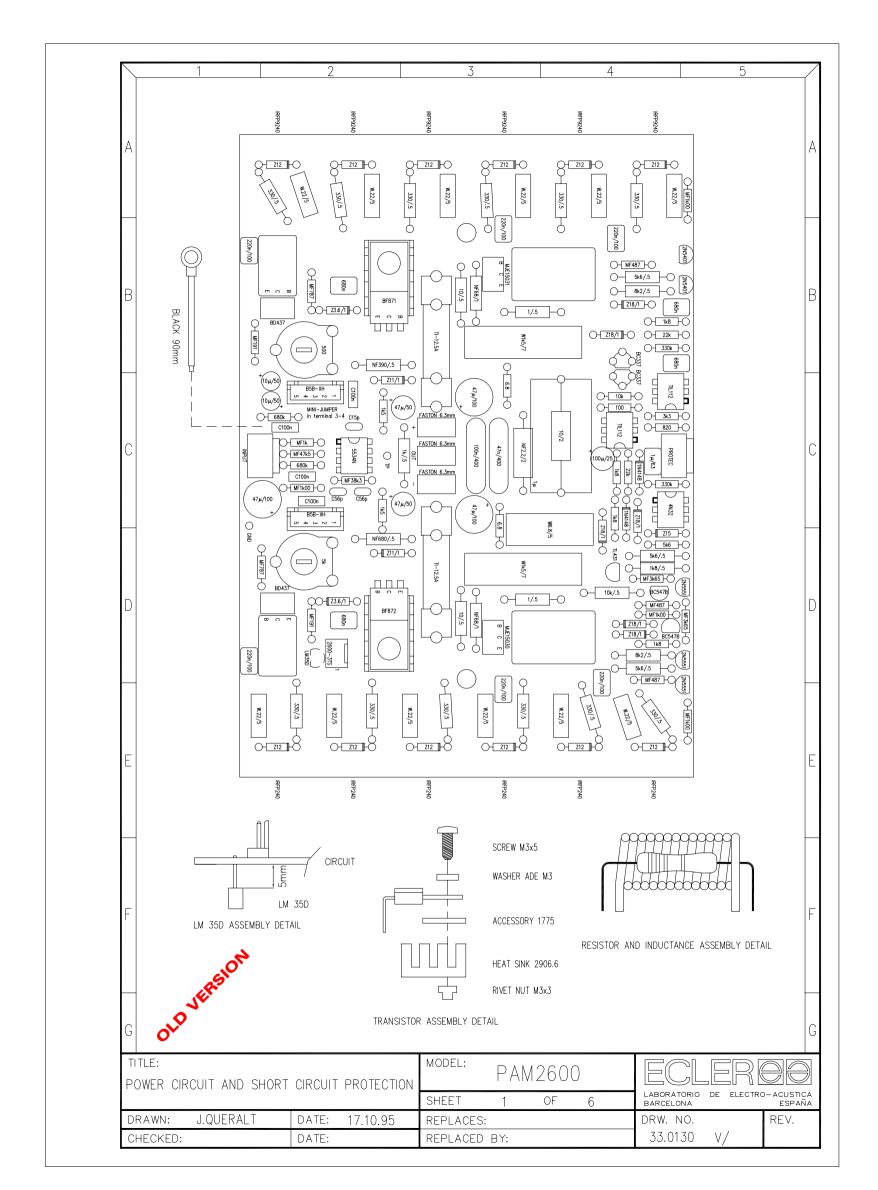
R179 22k R180 1k8 R181 1k8 R182 MF3k65

PC 11.0504B PRINTED CIRCUIT WIRE BLACK 90mm whit TER.









POWER CIRCUIT AND PARTS LIST:

MODEL:PAM2600 DRW.N° 33.0130PL

DATE: 000621 SHEET 1 OF 4 REPLACED BY:

REFERENCE **VALUE** C101  $47\mu/100$ C102 C100n C103  $10\mu/50$ C104  $10\mu/50$ C105 C15p C106 C100n C107 C100n C108 C100n C109 C56p C110 C56p C111  $47\mu/100$ C112  $47\mu/100$ C113 100n/400 C114 47n/400 C115  $47\mu/50$ C116  $47\mu/50$ C117 680n C118 680n C119 220n/100 C120 220n/100 C121 220n/100 C122 220n/100 C123 220n/100 C124 220n/100 C125 680n C126 680n C127  $1\mu/63$ C128  $100 \mu / 25$ D101 Z3.6/1 D102 Z3.6/1 D103 Z11/1 D104 Z11/1 D105 Z12 D106 Z12

Z12 D107 D108 Z12 Z12 D109 D110 Z12 D111 Z12 Z12 D112 D113 Z12 Z12 D114 D115 Z12 D116 Z12 D117 Z18/1 D118 Z18/1 D119 Z18/1 D120 Z18/1 D121 Z18/1 D122 1N4148 D123 1N4148 D124 Z18/1 D125 Z15

TL431

TI-12.5A

TI-12.5A

5534N

**TIL112** 

D126

F101

F102

IC101

IC102

SHORT CIRCUIT PROTECTION

REV:

PARTS LIST: POWER CIRCUIT AND SHORT CIRCUIT PROTECTION

MODEL:PAM2600 DRW.N° 33.0130PL REV:

DATE: 000621 SHEET 2 OF 4 REPLACED BY:

### REFERENCE VALUE

IC103 TIL112 IC104 4N32 IC105 LM35D

J101 FASTON 6.3mm J102 FASTON 6.3mm J103 FASTON 6.3mm

J104 B3P-VH J105 B3P-VH J107 B5B-XH J108 B5B-XH J109 2600-3TS Q101 BF871 Q102 BF872 Q103 MJE15031 Q104 MJE15030 Q105 IRFP240 Q106 IRFP240 IRFP240 Q107 Q108 IRFP240 Q109 IRFP240 Q110 IRFP240 Q111 IRFP9240 Q112 IRFP9240 Q113 IRFP9240 Q114 IRFP9240 Q115 **IRFP9240** Q116 IRFP9240 Q117 2N5401 Q118 2N5401 Q119 BC337 Q120 BC337 Q121 2N5551 2N5551 Q122 Q123 2N5551 Q124 BC547B Q125 BC547B Q126 **BD437** Q127 **BD437** R101 MF1k R102 MF47k5 R103 MF1k00 R104 680k R105 680k R106 MF38k3 R107 1k5 R108 1k5 1k/.5 R109 R110 5k R111  $500 \Omega$ R112 NF390  $\Omega$  /.5 R113 NF680  $\Omega$  /.5 R114 MF787  $\Omega$ 

MF191  $\Omega$ 

MF191 $\Omega$ 

MF787  $\Omega$ 

NF68  $\Omega$  /1 10  $\Omega$  /.5

NF68  $\Omega$  /1

R115

R116

R117

R118

R119 R120

PARTS LIST: POWER CIRCUIT AND

MODEL:PAM2600 DRW.Nº 33.0130PL

DATE: 000621 3 OF 4 REPLACED BY: SHEET

REFERENCE **VALUE** R121  $10 \Omega /.5$ R122  $1 \Omega /.5$ R123  $1 \Omega /.5$ R124  $W.22 \Omega /5$ R125  $W.22 \Omega /5$ R126  $W.22 \Omega /5$ R127  $W.22 \Omega /5$ R128  $W.22 \Omega /5$ R129  $W.22 \Omega /5$ R130 330  $\Omega$  /.5 R131  $330 \Omega /.5$ R132  $330 \Omega /.5$ R133  $330~\Omega$  /.5 R134  $330 \Omega /.5$ R135 330  $\Omega$  /.5 R136 330  $\Omega$  /.5 R137  $330 \Omega /.5$ R138  $330~\Omega$  /.5 R139  $330 \Omega /.5$ R140 330  $\Omega$  /.5 R141 330  $\Omega$  /.5 R142  $W.22 \Omega /5$ R143  $W.22 \Omega /5$ R144  $W.22 \Omega /5$ R145  $W.22~\Omega$  /5 R146  $W.22 \Omega /5$  $W.22 \Omega /5$ R147 R148 R149

NF2.2  $\Omega$  /2  $6.8 \Omega$ R150  $6.8 \Omega$ R151  $10 \Omega / 2$ R152 W1k5/7 R153 W6.8  $\Omega$  /5 R154 W1k5/7 R155 MF1k00 R156 MF487  $\Omega$ R157 5k6/.5 R158 8k2/.5 R159 1k8

R160 22k R161 330k R162 10k R163  $100 \Omega$ R164 3k3 R165  $820 \Omega$ R166 330k R167 5k6 R168 5k6/.5 R169 1k8/.5 R170 MF3k65 R171 10k/.5 R172 MF487  $\Omega$ R173 MF1k00 R174 1k8 R175 8k2/.5

5k6/.5

MF487  $\Omega$ 

MF1k00

R176

R177

R178

SHORT CIRCUIT PROTECTION

REV:

PARTS LIST: POWER CIRCUIT AND SHORT CIRCUIT PROTECTION

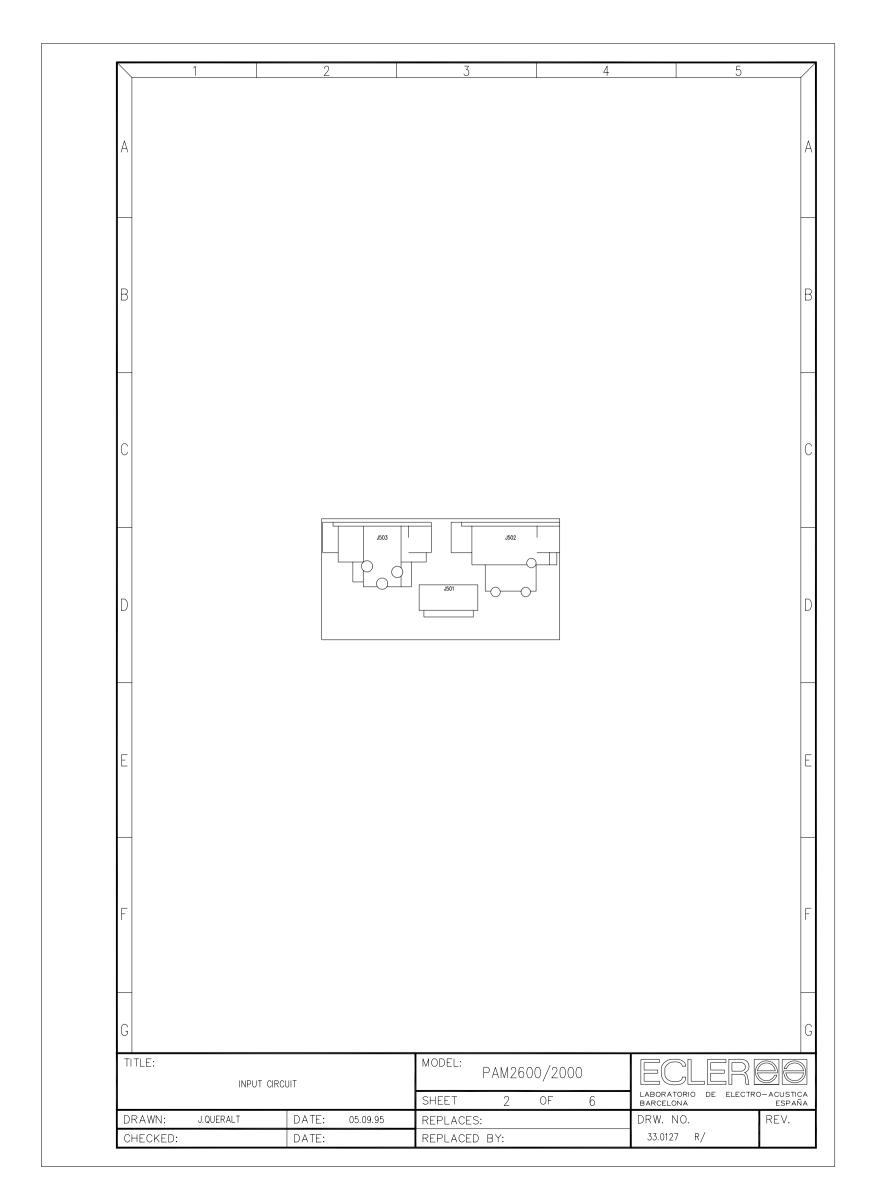
MODEL:PAM2600 DRW.N° 33.0130PL REV:

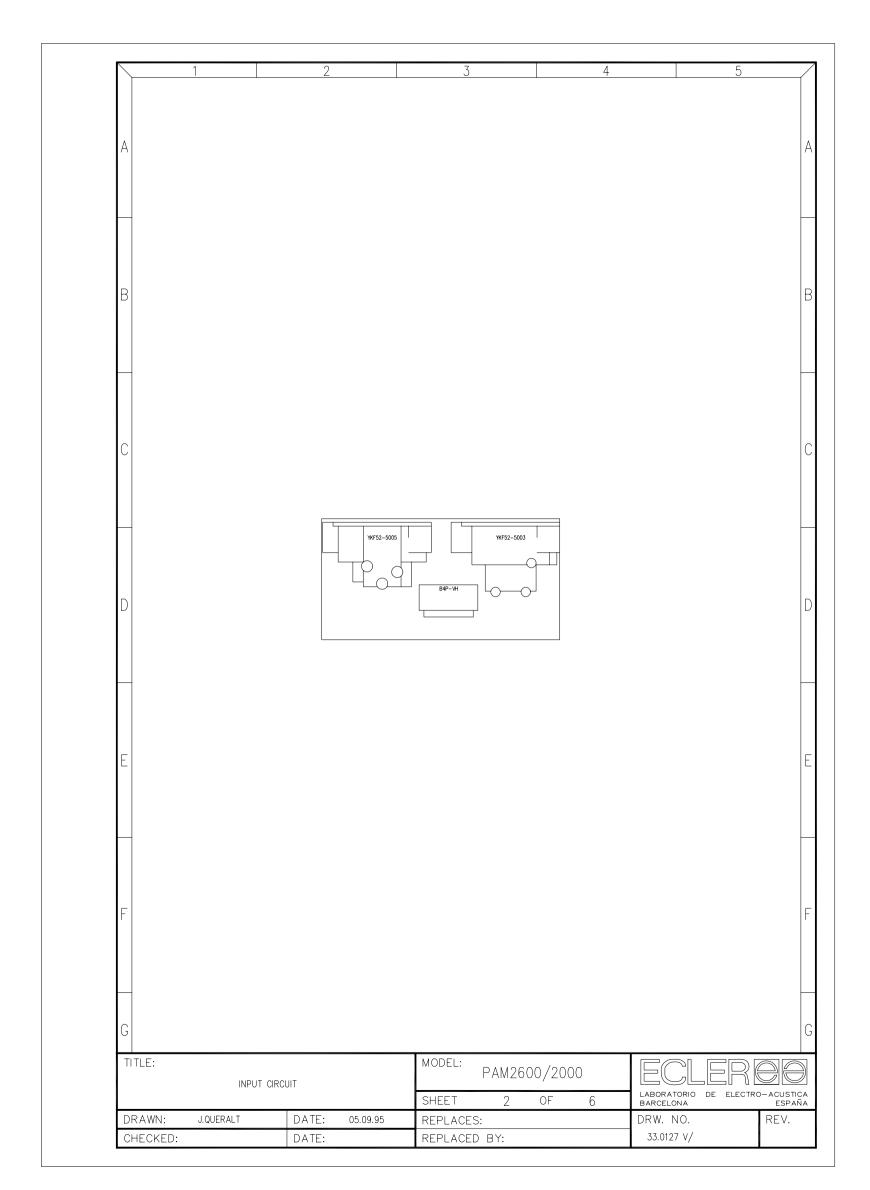
DATE: 000621 SHEET 4 OF 4 REPLACED BY:

REFERENCE VALUE

R179 22k R180 1k8 R181 1k8 R182 MF3k65

PC 11.0504B PRINTED CIRCUIT WIRE BLACK 90mm whit TER.





PARTS LIST: INPUT CIRCUIT MODEL: PAM2600/2000 DRW. No 33.0127PL

DATE: 050995 SHEET 1 OF 1 REPLACES:

REV:

REPLACED BY:

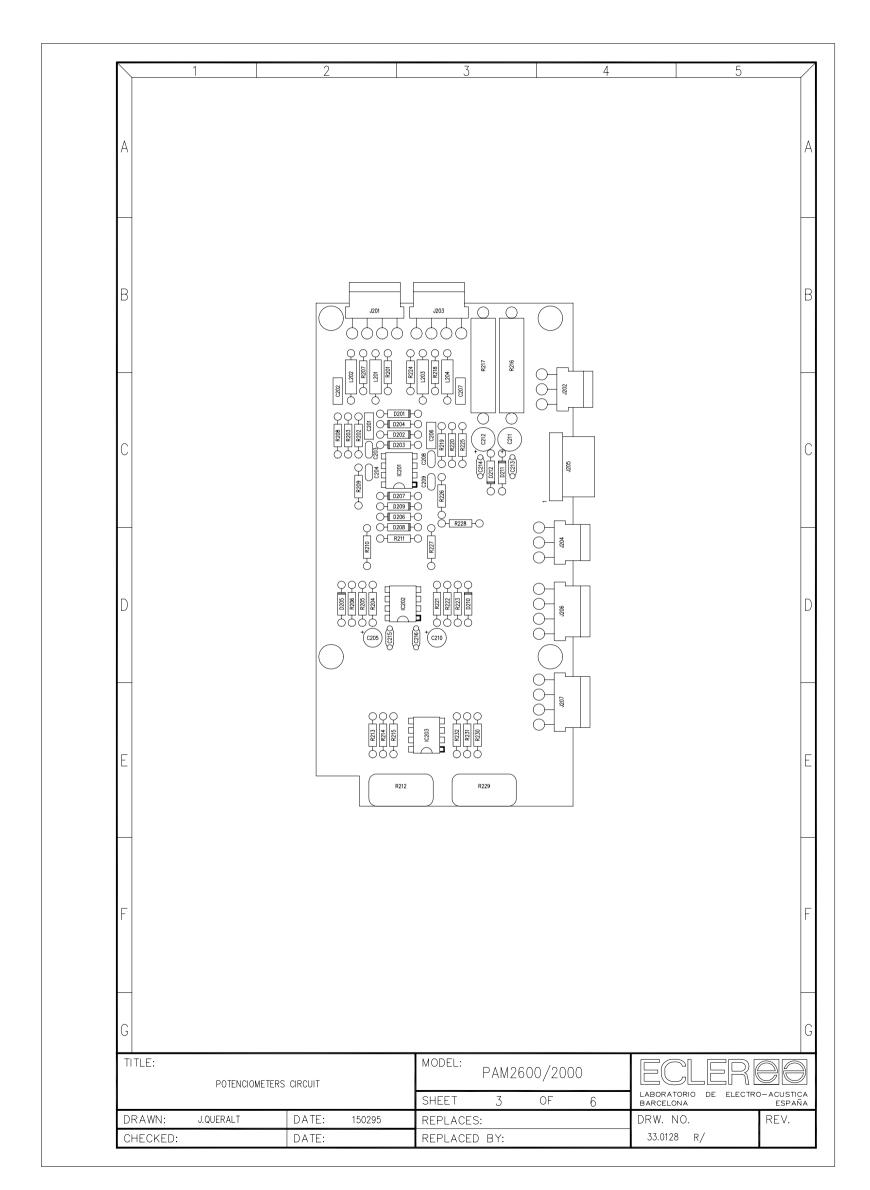
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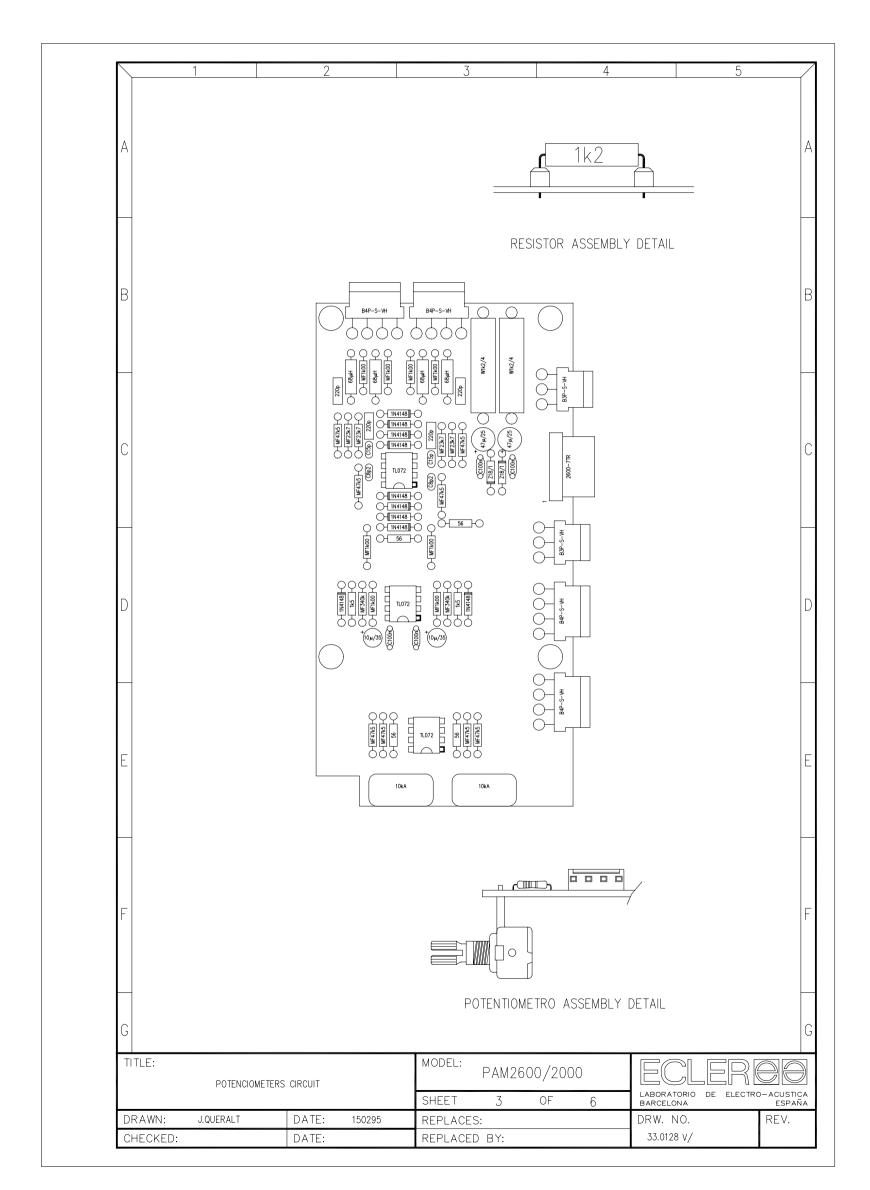
 J501
 B4P-VH

 J502
 YKF52-5003

 J503
 YKF52-5005

PC 11.0538 PRINTED CIRCUIT





PARTS LIST: POTENTIOMETERS CIRCUIT

MODEL: PAM2600/2000 DRW. No 33.0128PL

DATE: 150295 SHEET 1 OF 2 REPLACES: REPLACED BY:

REV:

### REFERENCE VALUE

C201 220p C202 220p C203 C15p C204 C8p2 C205  $10\mu/35$ C206 220p C207 220p C208 C15p C209 C8p2 C210  $10\mu/35$ C211  $47\mu/25$ C212  $47\mu/25$ C213 C100n C214 C100n C215 C100n C216 C100n D201 1N4148 D202 1N4148 D203 1N4148 1N4148 D204 D205 1N4148 D206 1N4148 D207 1N4148 D208 1N4148 D209 1N4148 1N4148 D210 D211 Z18/1 D212 Z18/1 IC201 TL072 IC202 TL072 IC203 TL072 J201 B4P-S-VH J202 B3P-S-VH J203 B4P-S-VH J204 B3P-S-VH J205 2600-7TR J206 B4P-S-VH J207 B4P-S-VH L201 68µH L202 68µH L203 68µH L204 68µH R201 MF1k00 R202 MF23k7 R203 MF23k7 R204 MF1k00 R205 MF340k R206 1k5 R207 MF1k00 R208 MF47k5 R209 MF47k5 R210 MF1k00 R211  $56\Omega$ R212 10kA MF47k5 R213

MF47k5

R214

PARTS LIST: POTENTIOMETERS CIRCUIT

MODEL: PAM2600/2000 DRW. No 33.0128PL

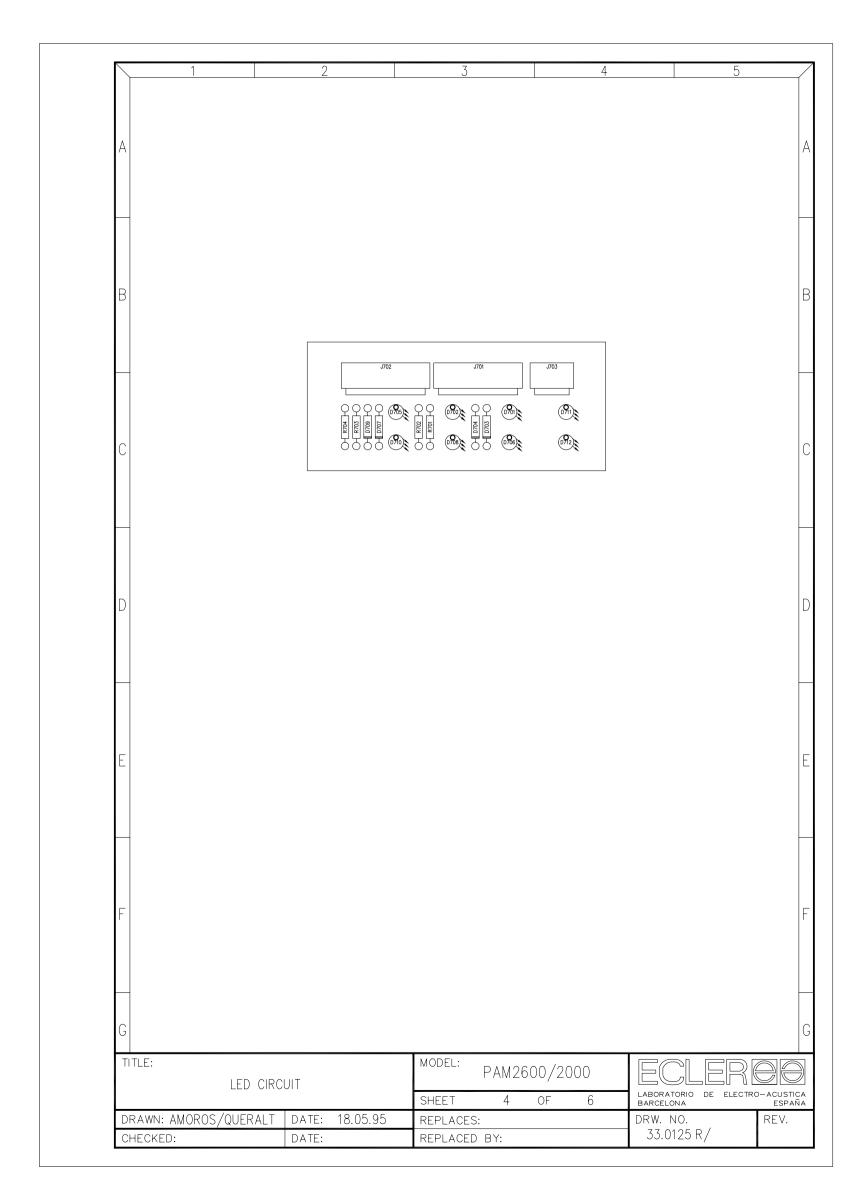
DATE: 150295 SHEET 2 OF 2 REPLACES: REPLACED BY:

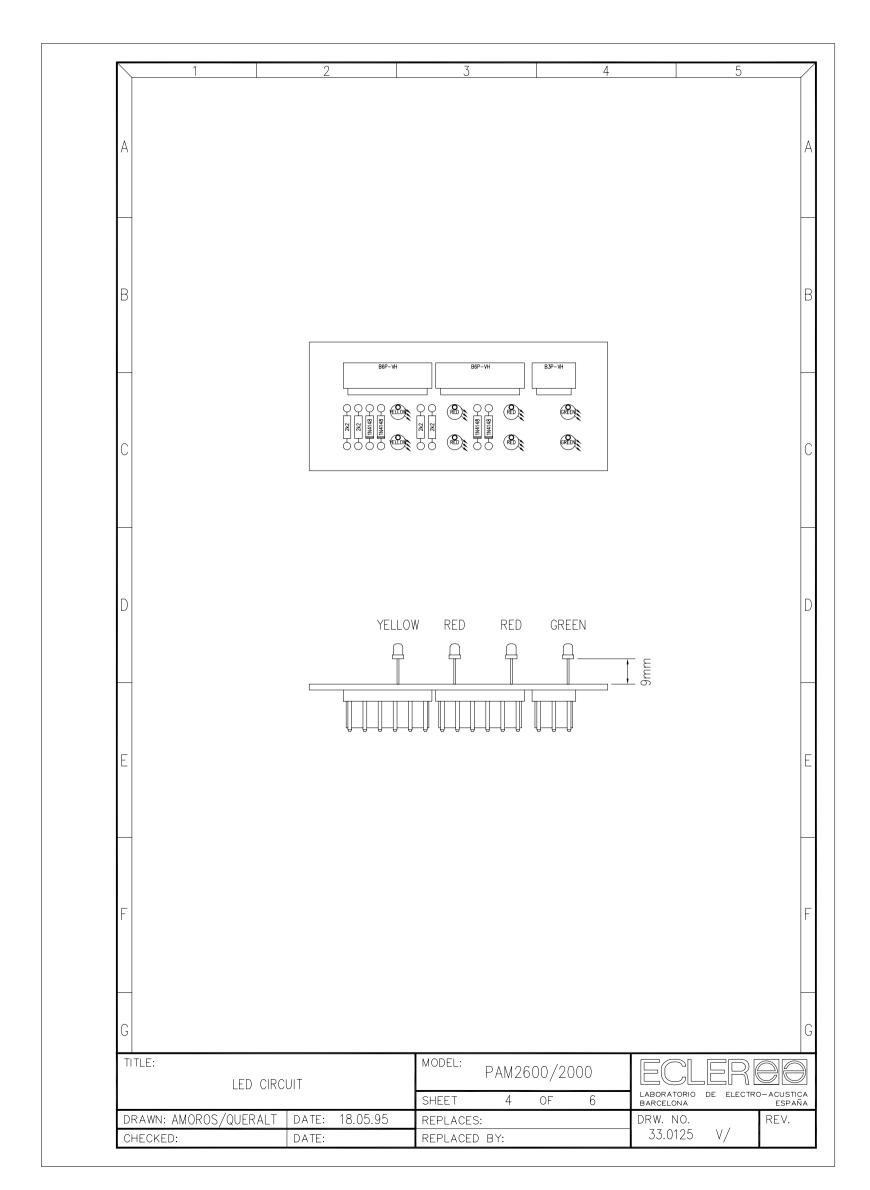
REV:

REFERENCE VALUE

R215  $56\Omega$ R216 W1k2/4 R217 W1k2/4 R218 MF1k00 R219 MF23k7 R220 MF23k7 R221 MF1k00 R222 MF340k R223 1k5 R224 MF1k00 R225 MF47k5 R226 MF47k5 R227 MF1k00 R228  $56\Omega$ R229 10kA R230 MF47k5 R231 MF47k5 R232  $56\Omega$ 

PC 11.0546 PRINTED CIRCUIT





PARTS LIST: LED CIRCUIT

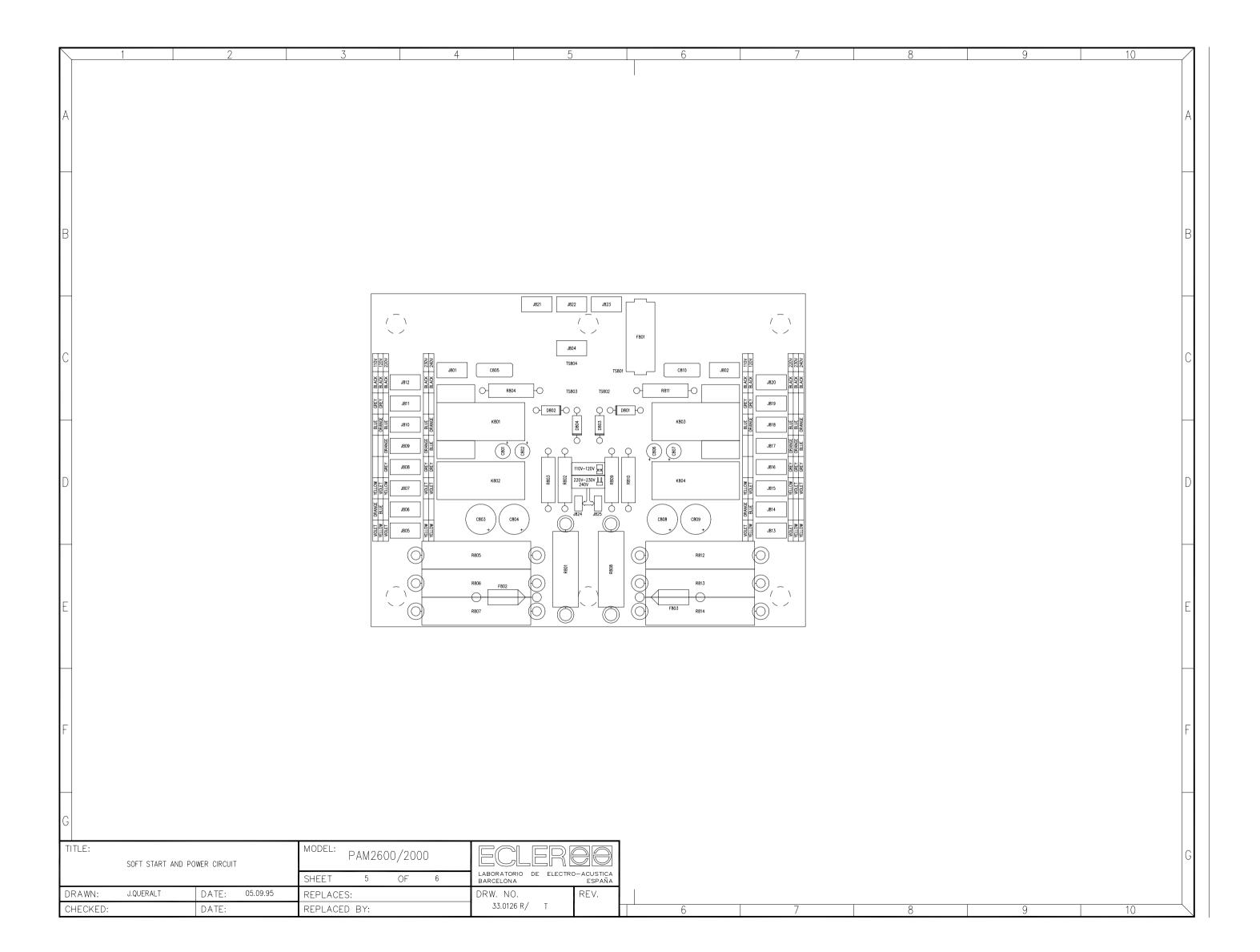
MODEL: PAM2600/2000 DRW. No 33.0125PL REV:

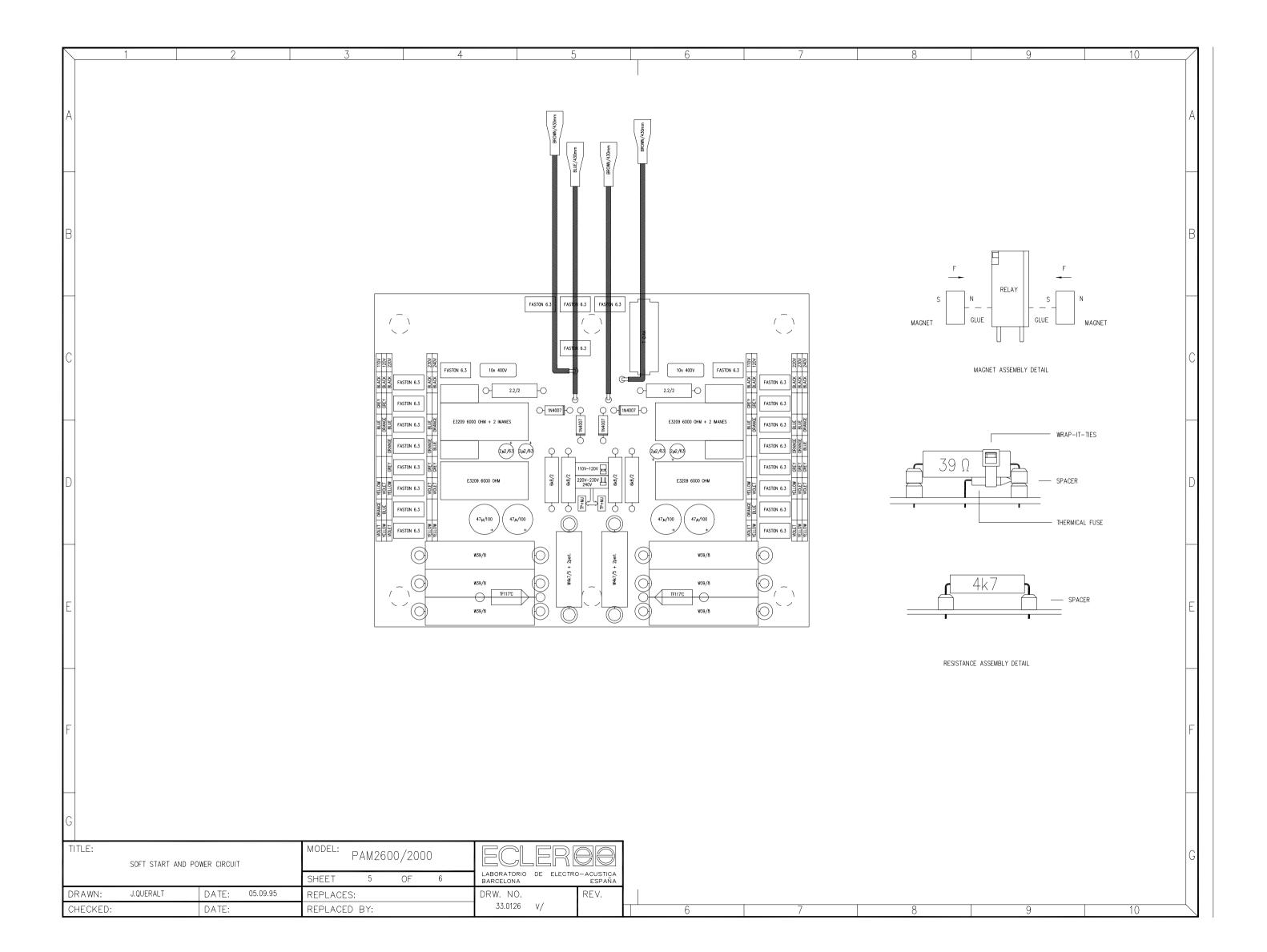
DATE: 180595 SHEET 1 OF 1 REPLACES: REPLACED BY:

REFERENCE VALUE

RED D701 D702 **RED** D703 1N4148 1N4148 D704 D705 YELLOW RED D706 D707 1N4148 D708 **RED** D709 1N4148 D710 **YELLOW** D711 **GREEN** D712 **GREEN** J701 B6P-VH J702 B6P-VH J703 B3P-VH R701 2k2 R702 2k2 R703 2k2 R704 2k2

PC 11.0537 PRINTED CIRCUIT





PARTS LIST: SOFT START AND POWER CIRCUIT

MODEL: PAM2600/2000 DRW. No 33.0126PL

DATE: 050995 SHEET 1 OF 2 REPLACES: REPLACED BY:

REV:

## REFERENCE VALUE

C801  $2\mu 2/63$ C802  $2\mu 2/63$ C803  $47\mu/100$ C804  $47\mu/100$ C805 10n 400V C806  $2\mu 2/63$ C807  $2\mu 2/63$ C808  $47\mu/100$ C809  $47\mu/100$ 10n 400V C810 D801 1N4007 D802 1N4007 D803 1N4007 D804 1N4007 F801 TI 0.25A F802 TF117°C TF117°C F803 J801 FASTON 6.3 J802 FASTON 6.3 J804 FASTON 6.3 J805 FASTON 6.3 J806 FASTON 6.3 FASTON 6.3 J807 J808 FASTON 6.3 J809 FASTON 6.3 J810 FASTON 6.3 J811 FASTON 6.3 J812 FASTON 6.3 J813 FASTON 6.3 J814 FASTON 6.3 J815 FASTON 6.3 J816 FASTON 6.3 J817 FASTON 6.3 J818 FASTON 6.3 J819 FASTON 6.3 J820 FASTON 6.3 J821 FASTON 6.3 J822 FASTON 6.3 J823 FASTON 6.3 J824 2JP+MJ J825 2JP+MJ K801 E3209  $6000\Omega$ E3209  $6000\Omega$ K802 K803 E3209  $6000\Omega$ E3209  $6000\Omega$ K804 R801 W4k7/5 R802 6k8/2 6k8/2 R803  $2.2\Omega/2$ R804 R805  $W39\Omega/8$ R806  $W39\Omega/8$  $W39\Omega/8$ R807 R808 W4k7/5 6k8/2 R809 6k8/2 R810 R811  $2.2\Omega/2$ 

PARTS LIST: SOFT START AND POWER CIRCUIT

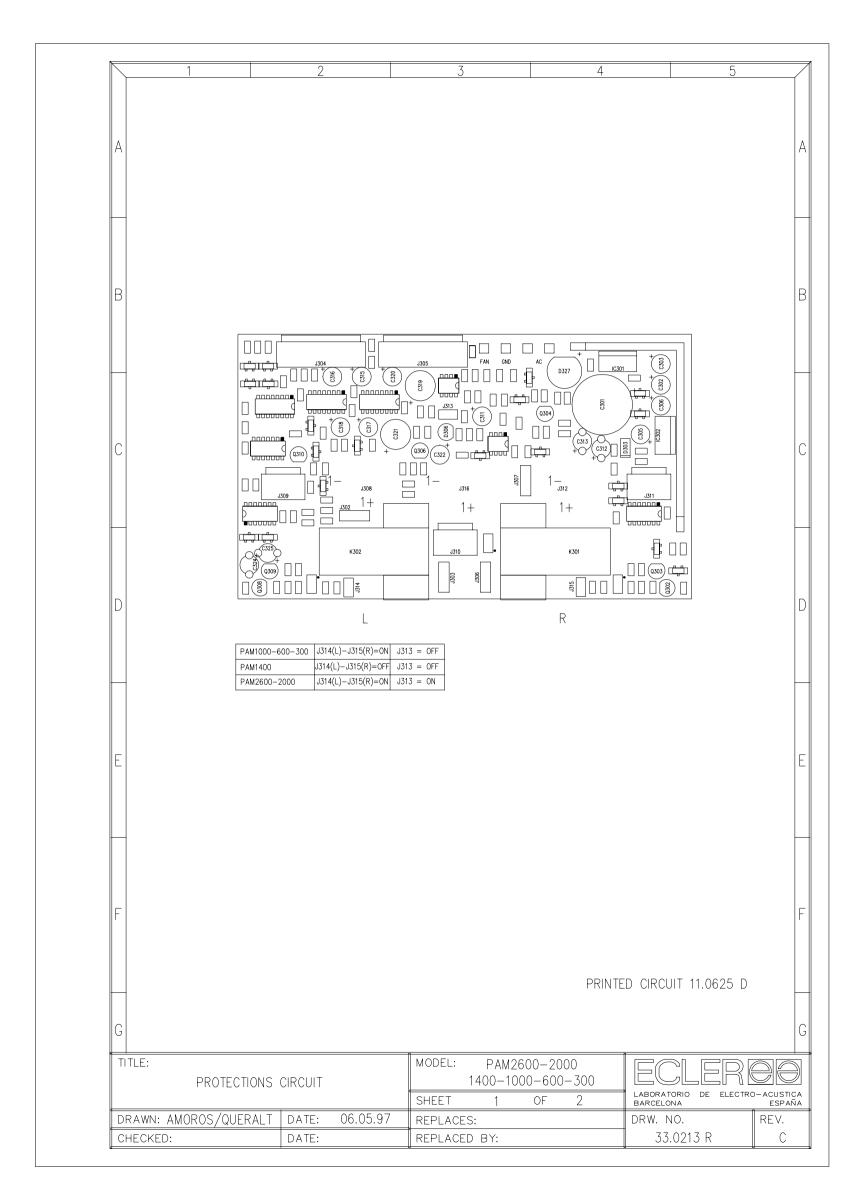
MODEL: PAM2600/2000 DRW. No 33.0126PL

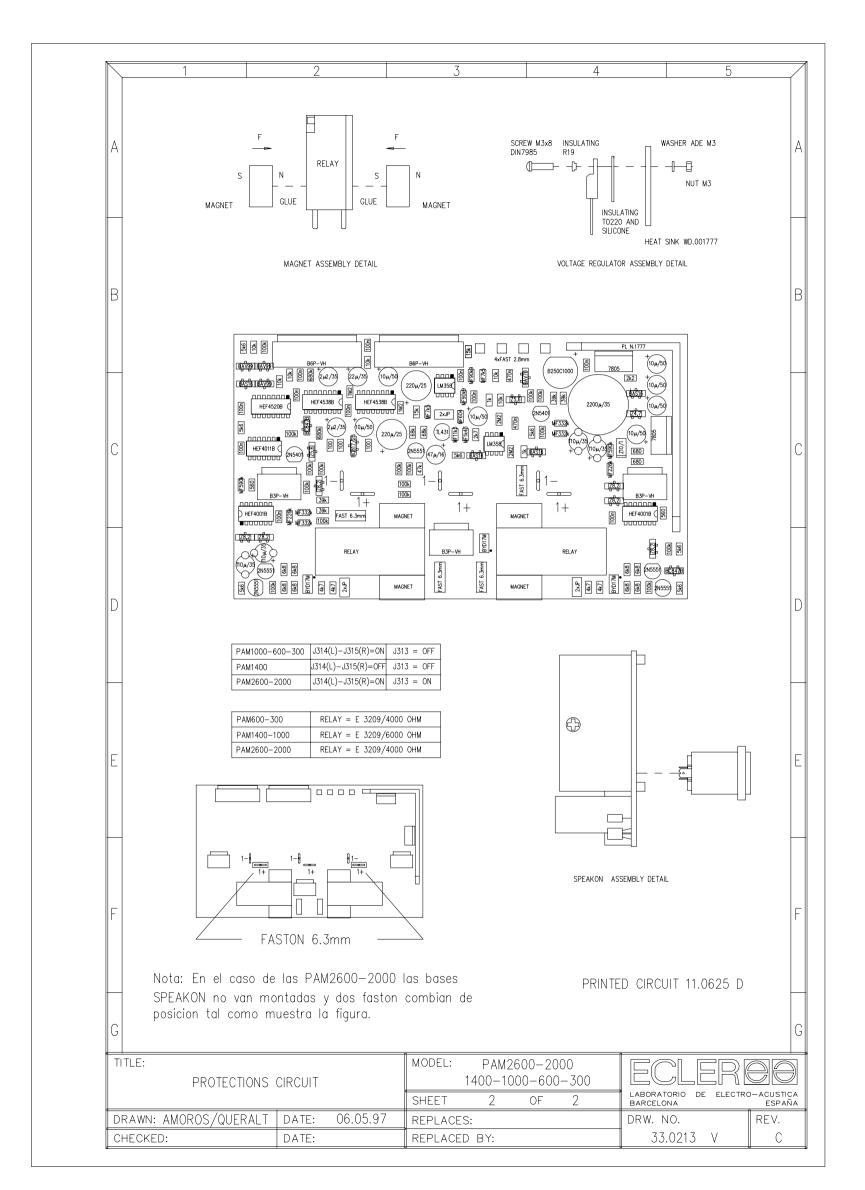
DATE: 050995 SHEET 2 OF 2 REPLACES: REPLACED BY:

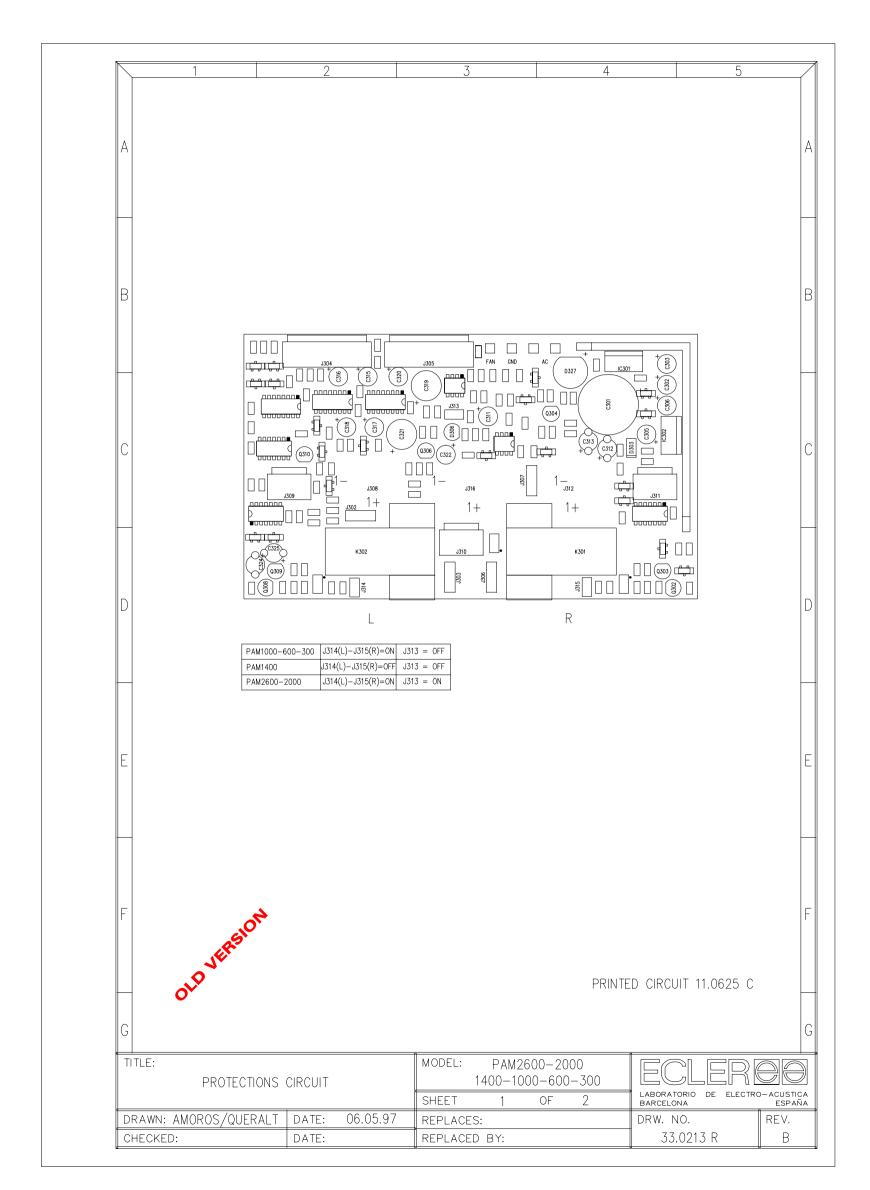
REV:

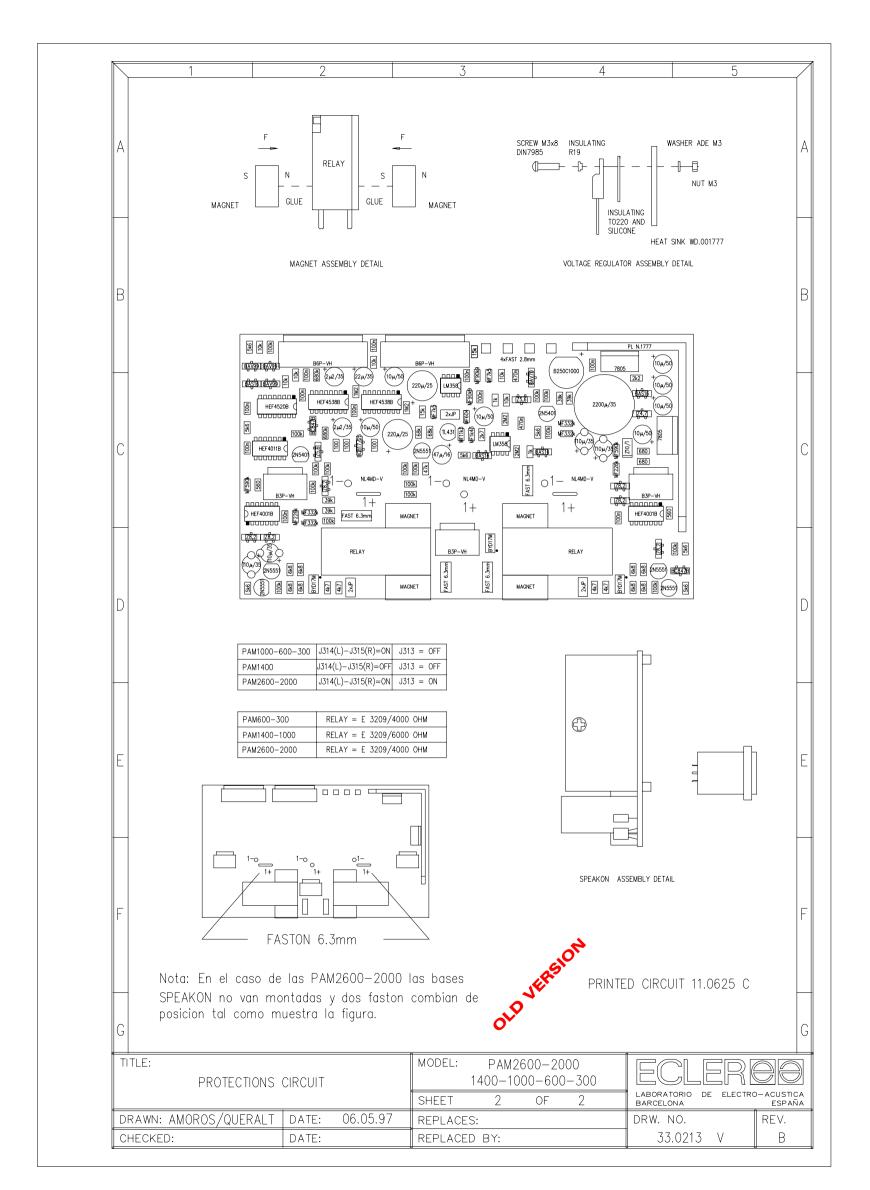
REFERENCE VALUE

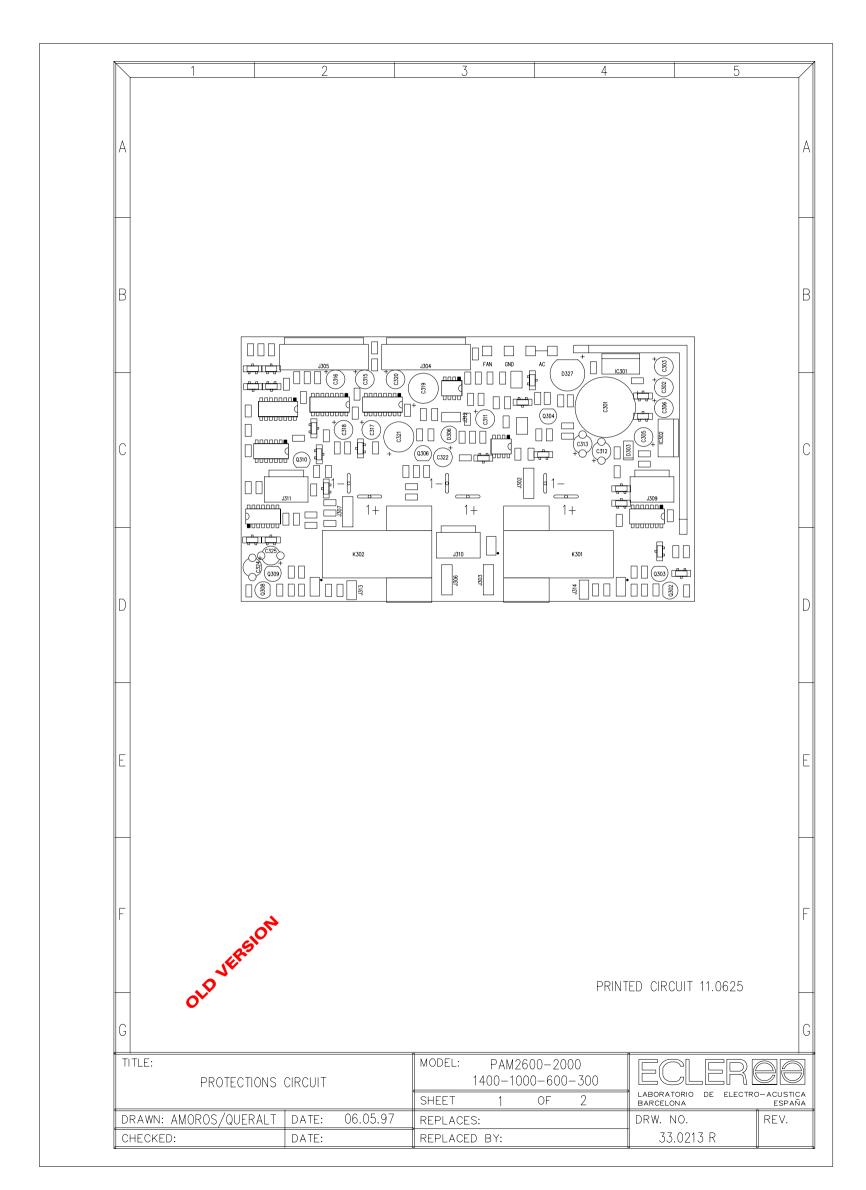
 $\begin{array}{ccc} \text{R812} & \text{W39}\Omega/8 \\ \text{R813} & \text{W39}\Omega/8 \\ \text{R814} & \text{W39}\Omega/8 \\ \text{WIRE8} & \text{BLUE/430mm} \\ \text{WIRE9} & \text{BROWN/430mm} \\ \text{WIRE9} & \text{BROWN/430mm} \\ \text{WIRE9} & \text{BROWN/430mm} \\ \end{array}$ 

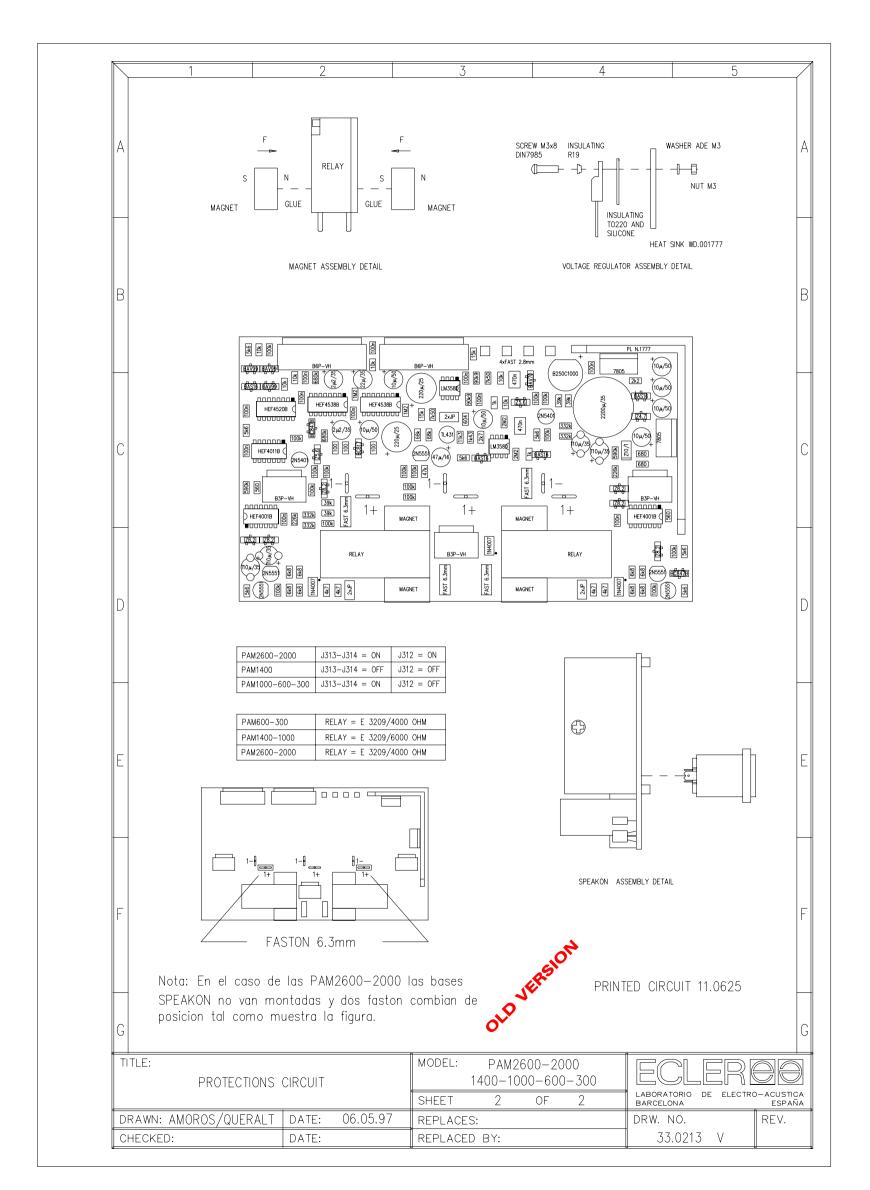


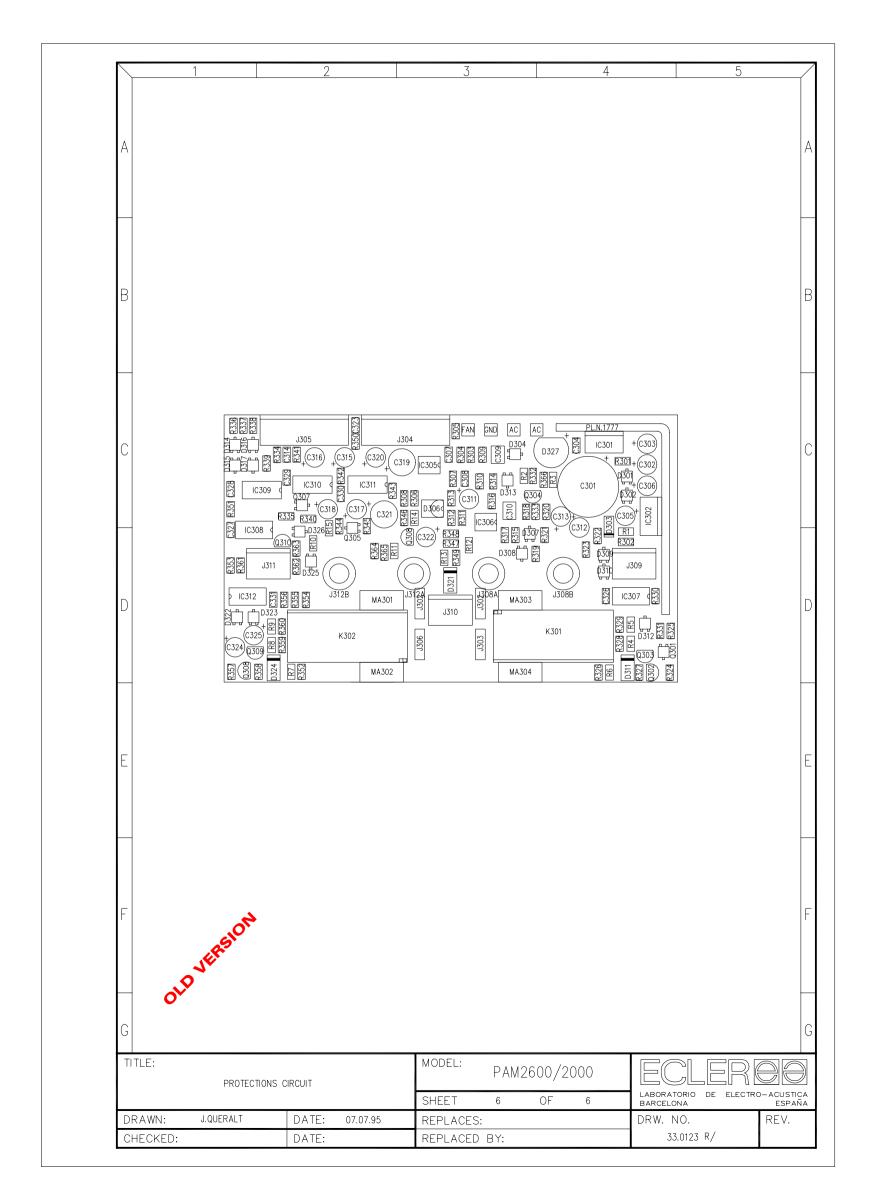


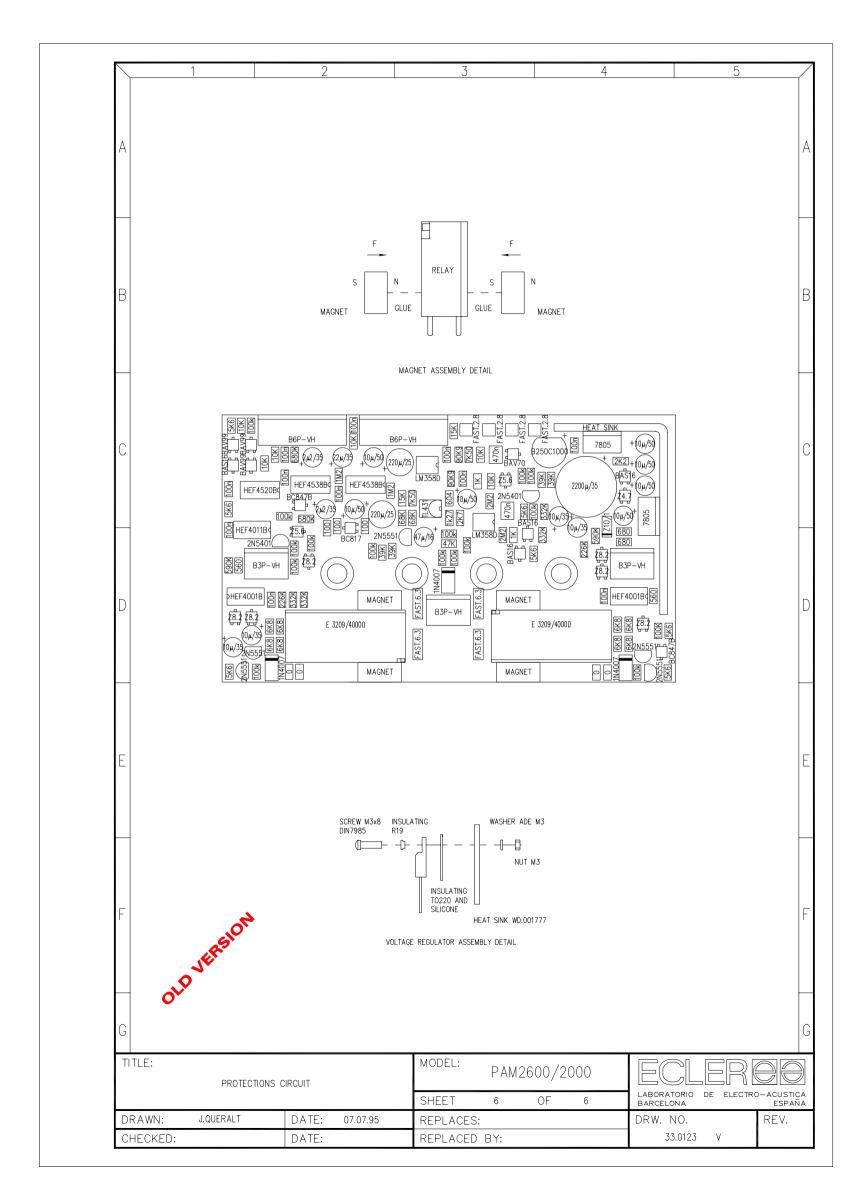












PARTS LIST: PROTECTIONS CIRCUIT

MODEL: PAM2600/2000 DRW. No 33.0123PL DATE: 070795 SHEET 1 OF 4 REPLACES:

REFERENCE VALUE

AC FAST.2.8 AC FAST.2.8 C301 2200µ/35 C302  $10\mu/50$ C303  $10\mu/50$ C304 100n C305  $10\mu/50$ C306  $10\mu/50$ C307 100n C308 100n C309 470n

C310 470n C311  $10\mu/50$ C312  $10\mu/35$ C313  $10\mu/35$ C314 100n C315  $22\mu/35$ C316  $2\mu 2/35$ C317  $10\mu/50$ C318  $2\mu 2/35$ C319 220µ/25 C320  $10\mu/50$ C321 220µ/25

C322  $47\mu/16$ C323 100n C324  $10\mu/35$ C325  $10\mu/35$ C326 100n C327 100n C328 100n C329 100n C330 100n C331 100n

D302 Z4.7 Z10/1 D303 D304 BAV70 D306 TL431 D307 **BAS16** D308 **BAS16** D309 Z8.2 Z8.2 D310

**BAS16** 

1N4007

D301

D311

 D312
 Z8.2

 D313
 Z5.6

 D314
 BAV99

 D315
 BAS16

 D316
 BAV99

 D317
 BAV99

 D321
 1N4007

D322 Z8.2 D323 Z8.2 D324 1N4007 D325 Z8.2

D326 Z5.6 D327 B250C1000 REV:

REPLACED BY:

PARTS LIST: PROTECTIONS CIRCUIT

MODEL: PAM2600/2000 DRW. No 33.0123PL
DATE: 070795 SHEET 2 OF 4 REPLACES:

**HEF4538B** 

**HEF4538B** 

REFERENCE VALUE

**FAN** FAST.2.8 **GND** FAST.2.8 IC301 7805 IC302 7805 IC305 LM358D IC306 LM358D IC307 HEF4001B IC308 HEF4011B IC309 HEF4520B

IC310

IC311

IC312 HEF4001B **INSULANT WASHER** R19 **INSULANT WASHER** R19 FAST.6.3 J302 J302 FAST.6.3 J303 FAST.6.3 J304 B6P-VH J305 B6P-VH J306 FAST.6.3 J309 B3P-VH J310 B3P-VH

J311 B3P-VH K301 E  $3209/4000\Omega$ K302 E  $3209/4000\Omega$ MA301 **MAGNET** MA302 **MAGNET** MA303 **MAGNET** MA304 **MAGNET** NUT М3

NUT М3 PL.N.1777 **HEAT SINK** Q301 BC847B Q302 2N5551 Q303 2N5551 Q304 2N5401 Q305 BC817 Q307 BC847B Q308 2N5551 Q308 2N5551 Q309 2N5551 Q310 2N5401 R1  $680\Omega$ R10 100k R11 39K R12 100k R13 100k R14 68K R15  $100\Omega$ R2 100k R3 39K R301 2K2  $680\Omega$ R302

> 7K50 90K9

15K

R303

R304 R305 REPLACED BY:

REV:

PARTS LIST: PROTECTIONS CIRCUIT

MODEL: PAM2600/2000 DRW. No 33.0123PL DATE: 070795

REFERENCE **VALUE** 

R306 7K50 R307 90K9 R308 15K R309 10K R310 1K 2K7 R311 R312 1k27 R313  $604\Omega$ 10K R314 1K R315

2M2 R316 R317 2M2 5K6 R318 R319 5K6 R320 332K 332K R321

R322 590K R323 226K R324 5K6 R325 5K6 R326  $0\Omega$ R327 100k R328 6K8 R329 6K8 R330  $560\Omega$ 

100K

 $100\Omega$  $100\Omega$ 

226K

5K6

100k

6K8 6K8

 $560\Omega$ 

R331

R344

R356

R357

R358

R359

R360 R361

R332 100k R333 100k R334 10K R335 100k R336 5K6 R337 10K R338 100k R339 10K R340 680K R341 680K R342 1M2 R343 1M2

R345 R346 68K R347 47K R348 100k R349 100k R350 10K R351 5K6 R352  $0\Omega$ 590K R353 R354 332K R355 332K

SHEET 3 OF 4 REPLACES:

REV: **REPLACED BY:** 

PARTS LIST: PROTECTIONS CIRCUIT MODEL: PAM2600/2000 DRW. No 33.0123PL

REPLACED BY: DATE: 070795 SHEET 4 OF 4 REPLACES:

**REFERENCE VALUE** 

R362 100k R363 100k 100k R364 R365 39K R366 39K 6K8 R4 R5 6K8 R6  $\Omega$ 0 R7  $\Omega$ 0 R8 6K8 R9 6K8

**SCREW** M3X8 DIN7985 NINE **SCREW** M3X8 DIN7985 NINE

ADE M3 **WASHER WASHER** ADE M3 OLD VERSION

REV:

#### PROFESSIONAL PAM SERIES - TESTING RULES

#### **PRELIMINARY**

## **GROUND LINK Testing.**

- Verify that when the switch is at the ON position there is continuity between the chassis ground and the speakers ground terminal and that the opposite happens at the OFF position. Leave it at ON.
- Put the power amplifier in stereo mode.
- We will need a 4000VA variac for our test purposes.
- Take off one of the fuses of the module in which the testing is being made and connect an ammeter (10A DC scale) in its place.
- Put the oscilloscope probe between TP-GND.

#### SET UP

- Unplug the fuses of the module that we are NOT setting up.
- Connect the power amplifier mains cable to the output of the variac. Set the variac output at 0V.
- Switch the power amplifier on with no load or signal. Turn the variac up progressively step by step until 220V. While mains voltage is growing up make sure the module's current does never exceed 0.8A. Once the circuit is stable make sure the current is 480mA/400mA respectively for PAM2600/ PAM2000 and the symmetry (measured up with the oscilloscope probe) is  $\leq$ 50mV. If your figures do not match these numbers adjust CURRENT (5K) and SYMMETRY (470 $\Omega$ ) untill you get the above mentioned numbers.
- Test the operational amplifier power supply ( $\pm 18V$ )  $\pm 1V$ .
- Put the fuse back in its place into the module (with the power amplifier turned off) and repeat the same procedure for the other channel.

### **CROSS DISTORTION**

By using a signal generator introduce a level of 100mV RMS at 1kHz and make sure there is no cross distortion at the output (attenuators at 0dB position).

# MOSFETS CONDUCTION

By using a signal generator introduce a level of 0.5V at 1kHz and load the amplifier with  $4\Omega$ Check that all MOSFETs are conducting approximately the same current level (measure this current with the oscilloscope probe by palcing it on the  $0.22\Omega$  source resistances). The maximum conduction difference between MOSFETs should be 100mV. When making this test be sure the oscilloscope ground is not connected to any other place of the circuit when making the reading; just to the  $0.22\Omega$  resistance. If you do not follow this rule you could produce a shortcircuit between two points of the circuit and therefore a very important damage.

# **POWER**

- Verify the amplifier's power at 8 and  $4\Omega$ .
- Maintain the mains voltage at 220V by means of the variac.
- Check that your own figures match the following at close-to-clip point:

		PAM2600	PAM2000
$\text{Vin}{\approx}\text{1VRMS/Vo}\text{4}\Omega$	≥	70 Vrms	60.5 Vrms
Vin≈1VRMS/Vo 8Ω	≥	81 Vrms	68 Vrms

### FREQUENCY RESPONSE

0.5V input signal.

Verify frequency response at 20Hz/2kHz/20kHz. We must get the same signal output for the actual load at any of the frequencies. Set the frequency at 50kHz; the output level should not decrease more than 1 or 2 dB and there should not be any noticeable distortion.

# CLIPPING AT 1kHz

Introduce such a signal that the amplifier is just about to clip. Measure the voltage up at the output (with the actual load) and check that when the voltage decreases between 0.5 and 1 dB the clipping LEDs light down. Check each LED corresponds to its fader.

#### DC OUT

For this test you must disconnect the load from the amplifier.

Introduce a 1V signal at  $\le$ 5Hz with the generator. Turn the output of the generator up untill the protection relays open and close.

### OVERHEATING PROTECTION

Disconnect the thermic sensor and shortcircuit the green and violet wires. Check that, first, the THERMAL led of the corresponding channel is lit; second, the fan is operating at maximum speed; and third, the two protection circuit relays are open. Connect again the connector.

Use a soldering iron to heat the thermic sensor lead and check that fan speed increases proportionally to the sensor temperature (do not heat excessively).

Remember that each module has two sensors.

Repeat the process for the other channel.

# **PROTECTIONS**

Disconnect the amplifier from the load and introduce with the signal generator a level of approximately 100mVRMS at 1KHz. Leave the attenuators at 0dB and shortcircuit the left channel output (just for a while) checking the PROTECT LED is lighting up and the relay opens the circuit (you can check this by placinf an oscilloscope probe at the amplifier's output and watching the signal disappear during the STAND BY time in which the protection circuit is working). Repeat the same process for the right channel.

# PROFESSIONAL PAM SERIES - QUALITY CONTROL

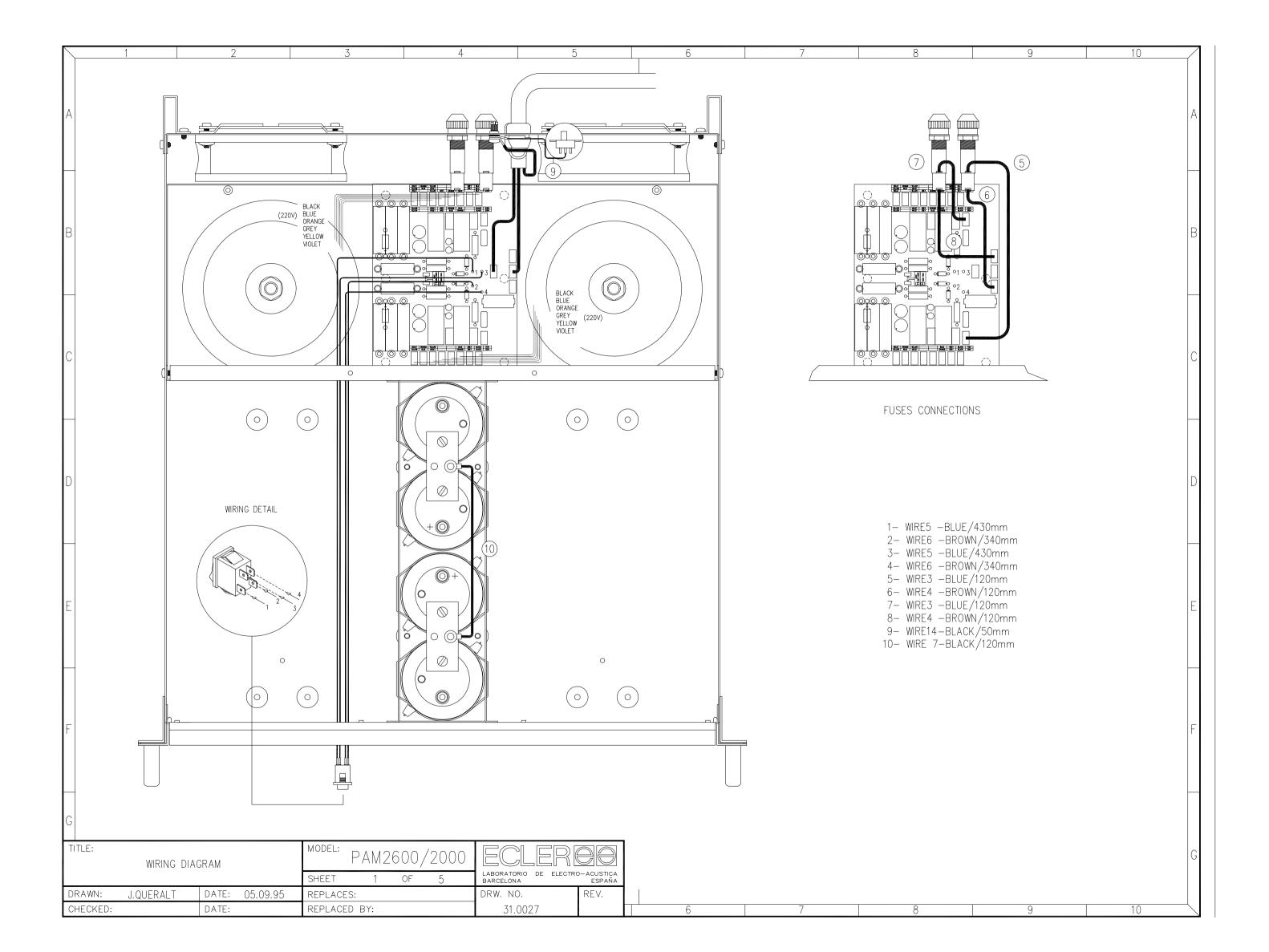
We will use a mixer with balanced output -if possible- and a nominal output level of 1V as the signal source for test purposes.

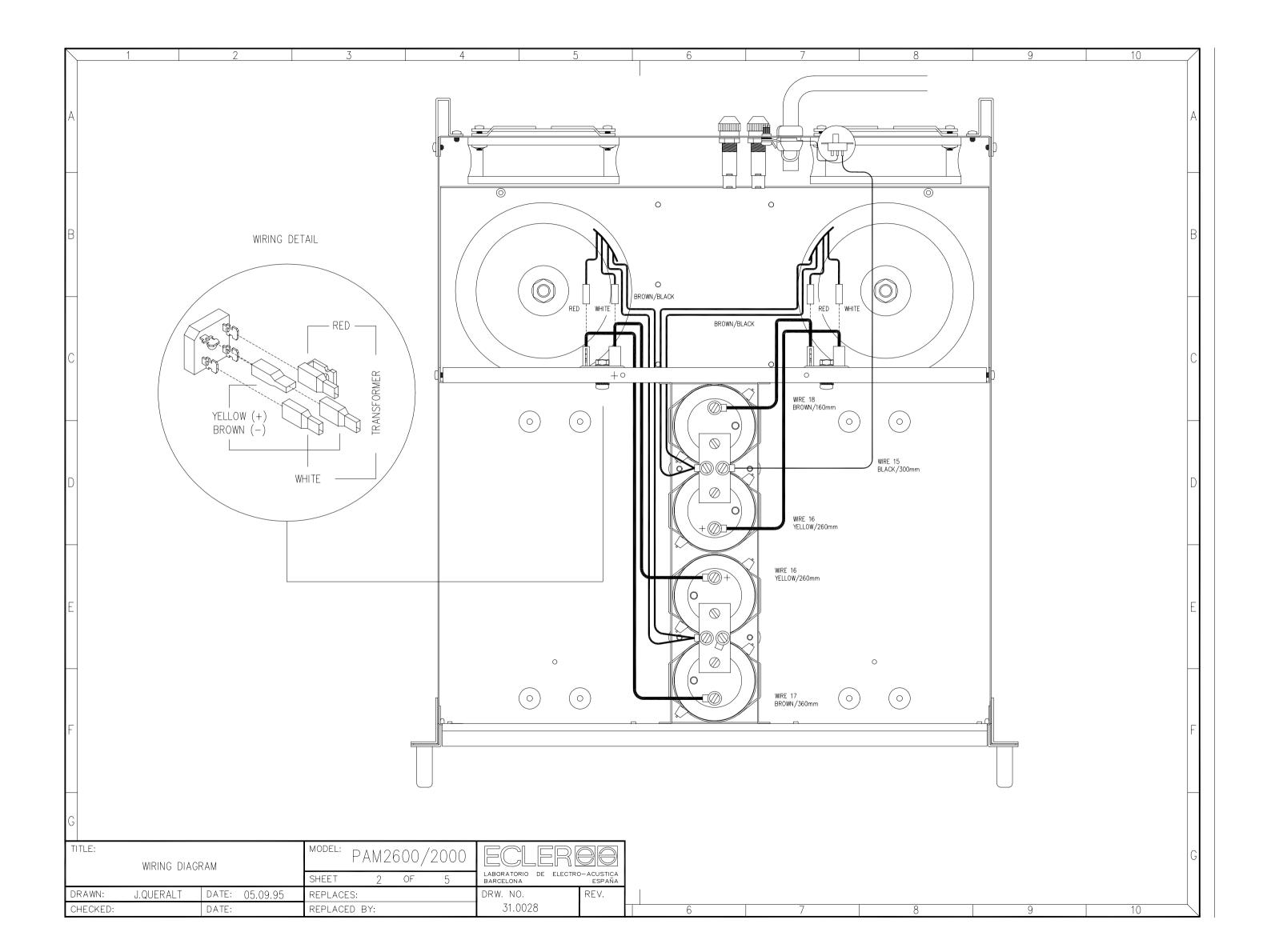
Connect the mixer outputs to the power amplifier inputs. Plug the power amplifier to mains (make sure its specified voltage matches that of mains) and make sure that PROTECT, ON and SIGNAL PRESENT LEDs all light up when you turn on the amplifier by pushing the ON button. Turn up the mixer output level untill the CLIP LEDs light up on the power amplifier. Turn down the mixer output and connect the loudspeakers.

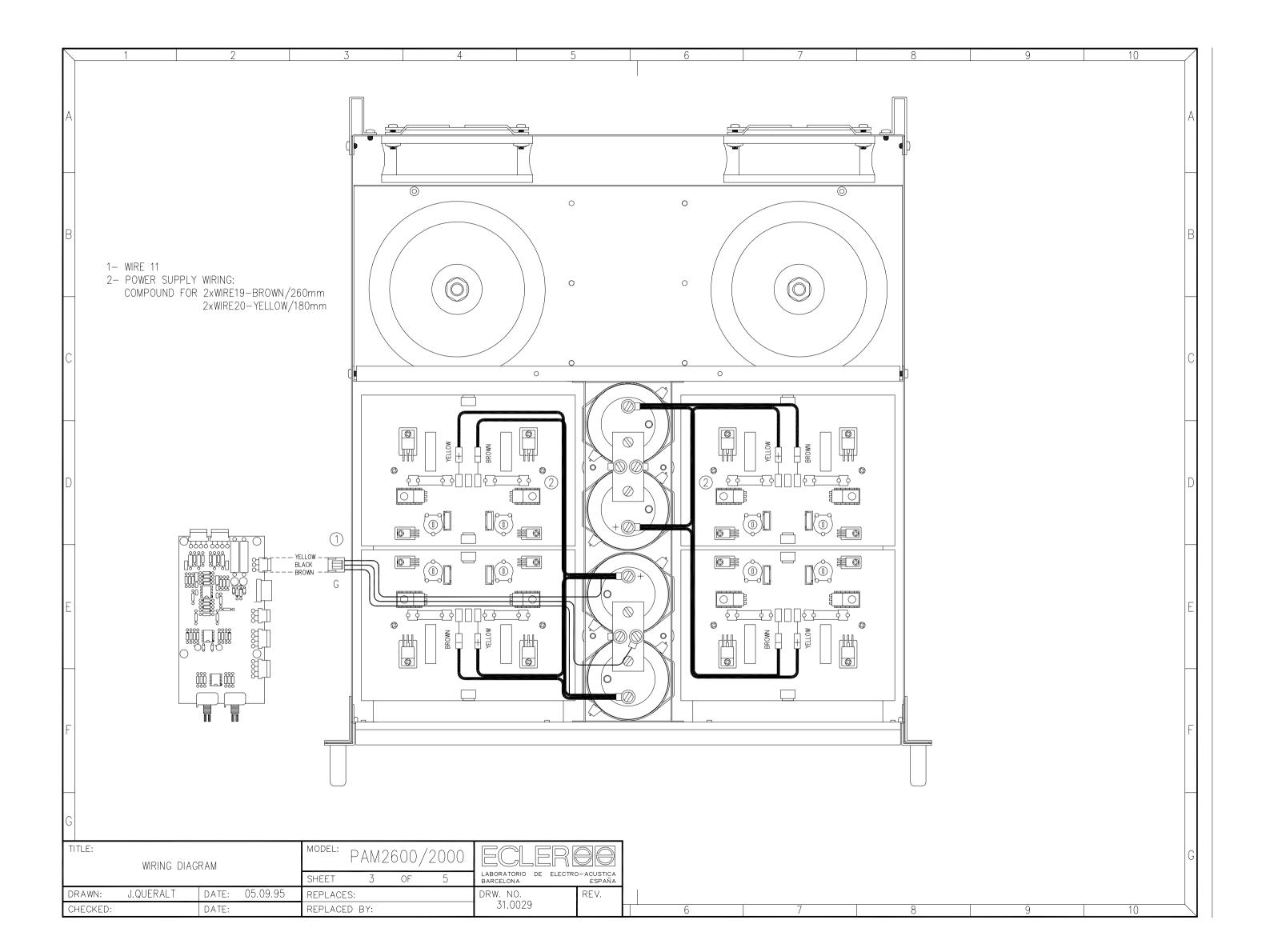
### Make an exhaustive test of:

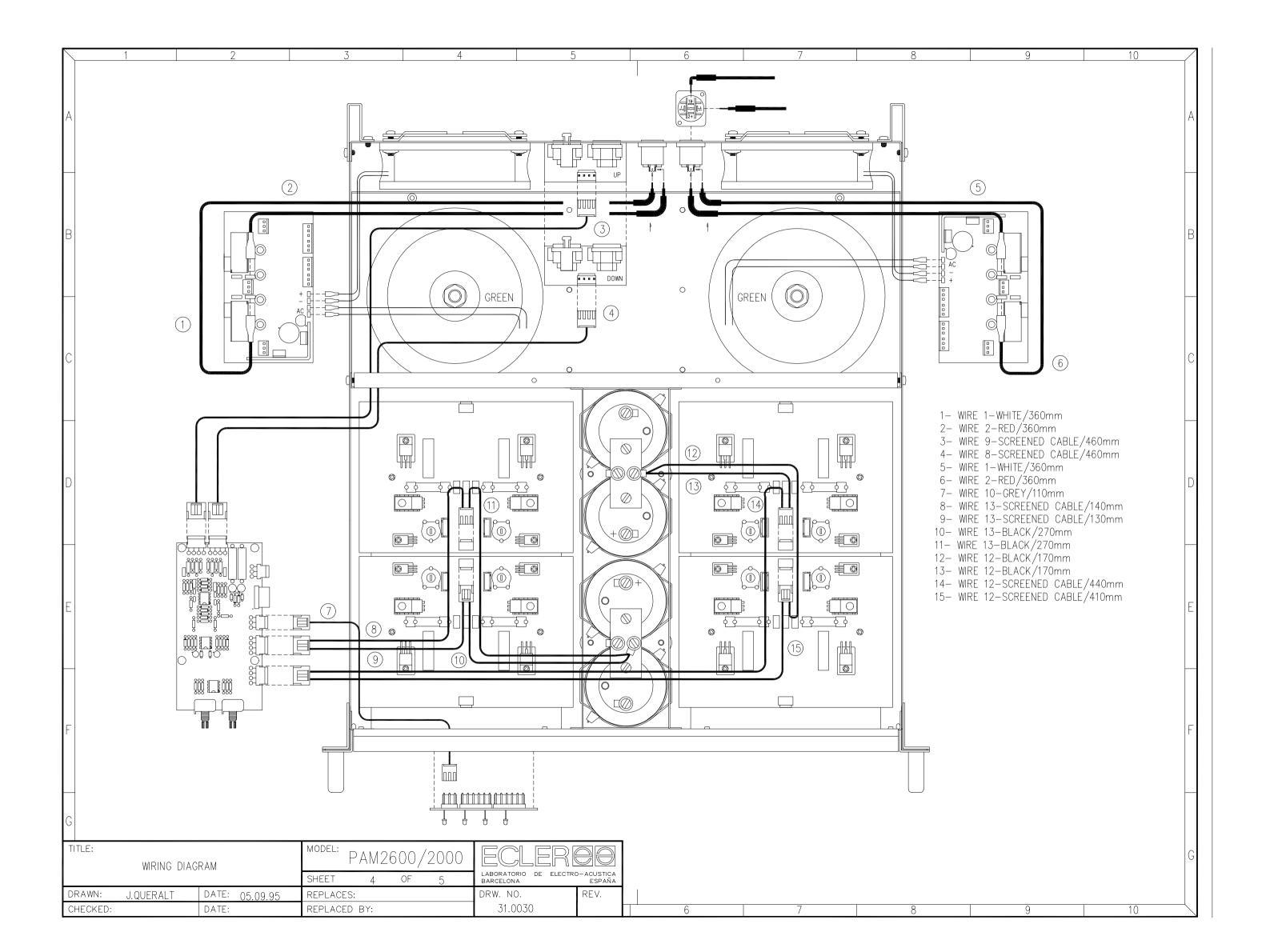
- Sound quality (no distorsions or noises)
- Faders action (fader travel, signal cut at their low end, no scratching or clicking noises and correct stereo channel for each one).
- Cooling fan operation.
- While the power amplifier is working shake it or throw it a table to make sure the output sound goes on playing correctly.
- Shortcircuit the power amplifier output and make sure the corresponding channel's PROTECT LED lights up, the relay opens and the output signal is cut for a short period of time (STAND BY) and returned back into normal operation. Repeat the same procedure four times more and then the STAND BY time should be about 5 minutes. Repeat the same steps for the other channel.

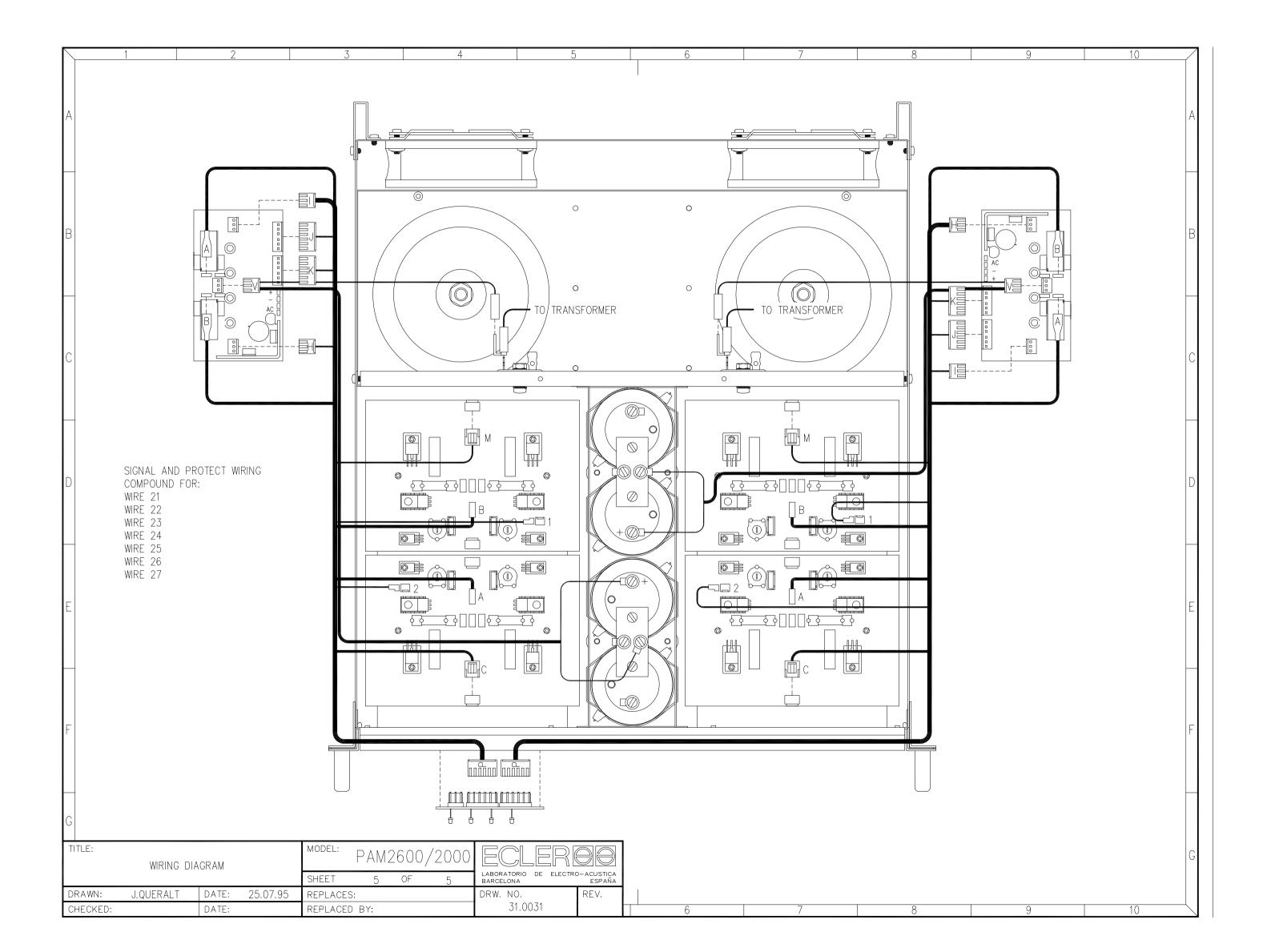
TECHNICAL CHARACTERISTICS	PAM2600	PAM2000		
Frequency response at max. power output.	7Hz to 60kHz +0 -1dB			
Harmonic distortion+noise from 20Hz to 20kHz meas.band	<0,02%	<0,02%		
Intermodulation distortion (SMPTE) using frequencies of 50Hz and 7kHz at 4:1 ratio, nominal power.	<0,03%	<0,03%		
TIM 100	<0,05%	<0,03%		
Signal noise ratio from 20Hz to 20kHz Ref.1W/4 $\Omega$ To 4 $\Omega$ nominal power.	>80 dB >111 dB	>80 dB >110 dB		
Damping factor at 1kHz $8\Omega$	>140	>140		
Slewrate	$_{\pm}98~\text{V/}~\text{s}$	$_{\pm}92~\text{V/}~\text{s}$		
Channel crosstalk at 1kHz	>65 dB	>65 dB		
Inputs balanced and provided with XLR3. CLIP indicators at -0,3dB	Sensitivity/load	0dBV/1V/47kΩ		
Outputs	These are provided with 2 speak on.			
Protections	-Delayed turn-on heavy duty relay with PROTECT indicator ON during standbyDC:4Hz or DC at 2V,PROTECT INDICATORThermal:A sensor activates a high temperature detection circuit,channel shut down at 90 ,THERMAL indicatorOverload:Protection against output short circuit.PROTECT indicatorAutoreset:Four automatic reset during five minutes in case of short circuit.After this period reset mustbe done manuallySoft start systemVarispeed Fan controled according to internal temperature.			
Power requirements 110V,120V 220V,230V,240V AC 50/60Hz	3650 VA	2730 VA		
Dimensions Front pannel Chassis	482,6x132,5mm 440x132,5x514mm			
Weight	31.2 kg	30.5 kg		

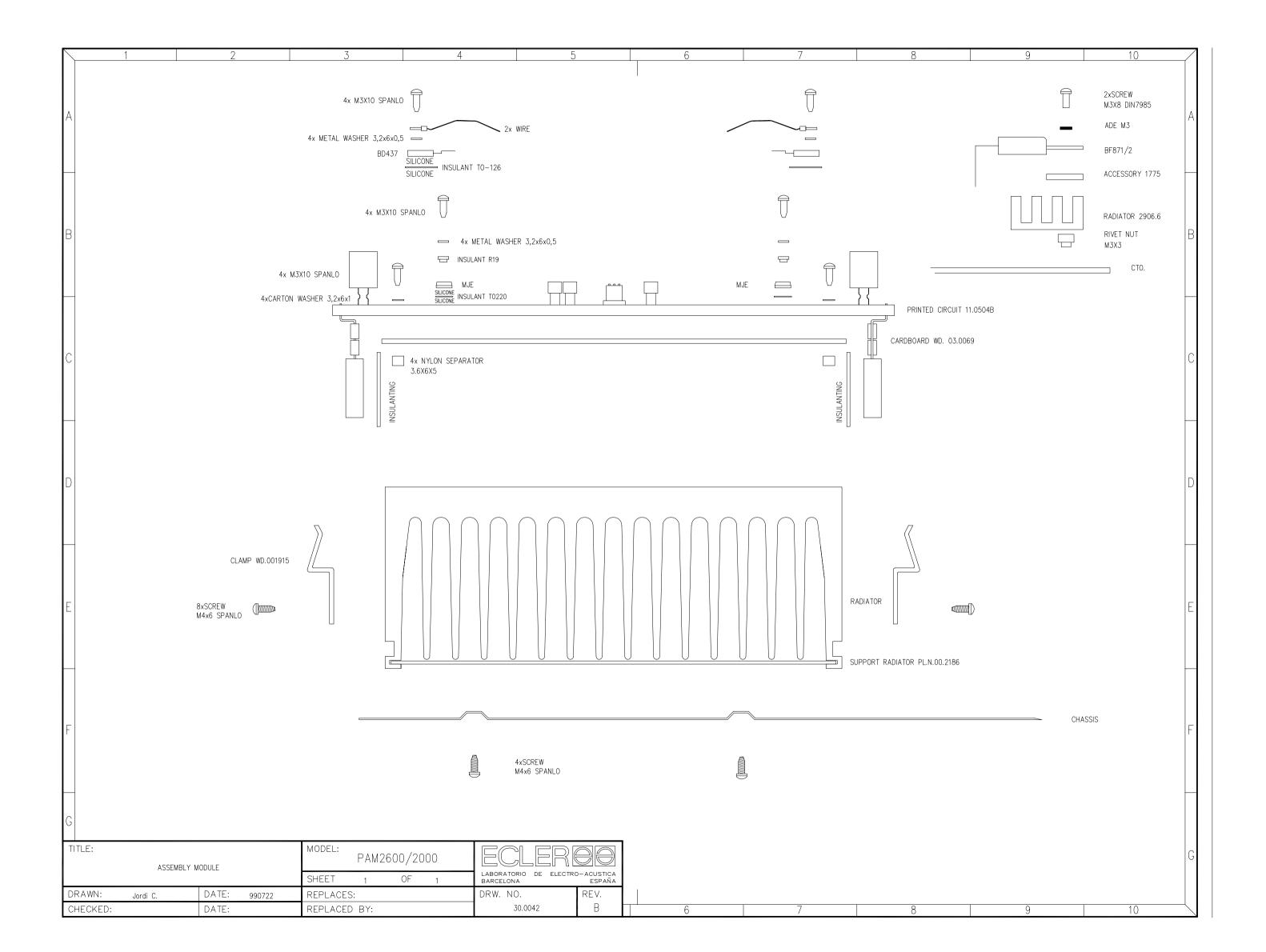


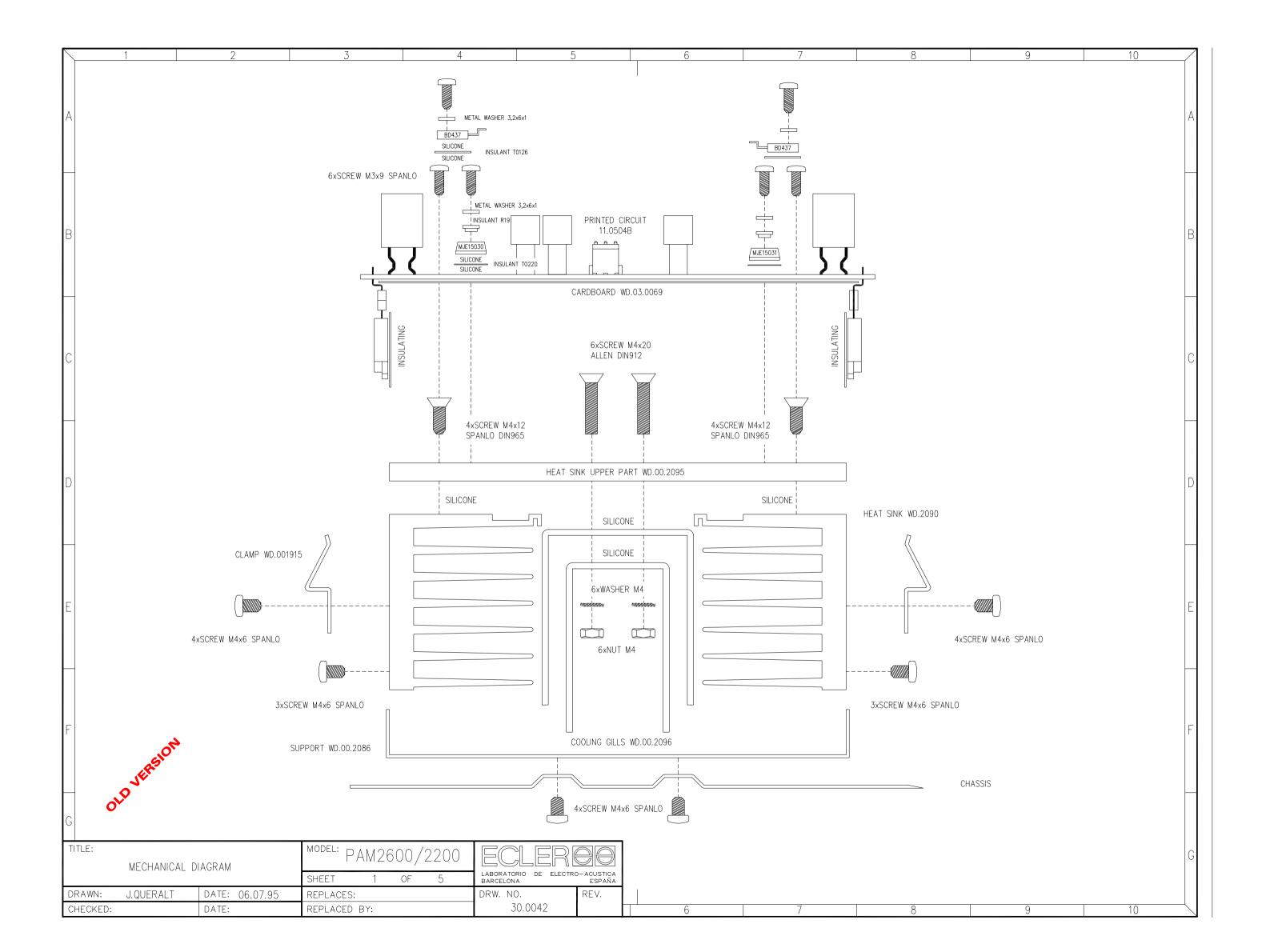










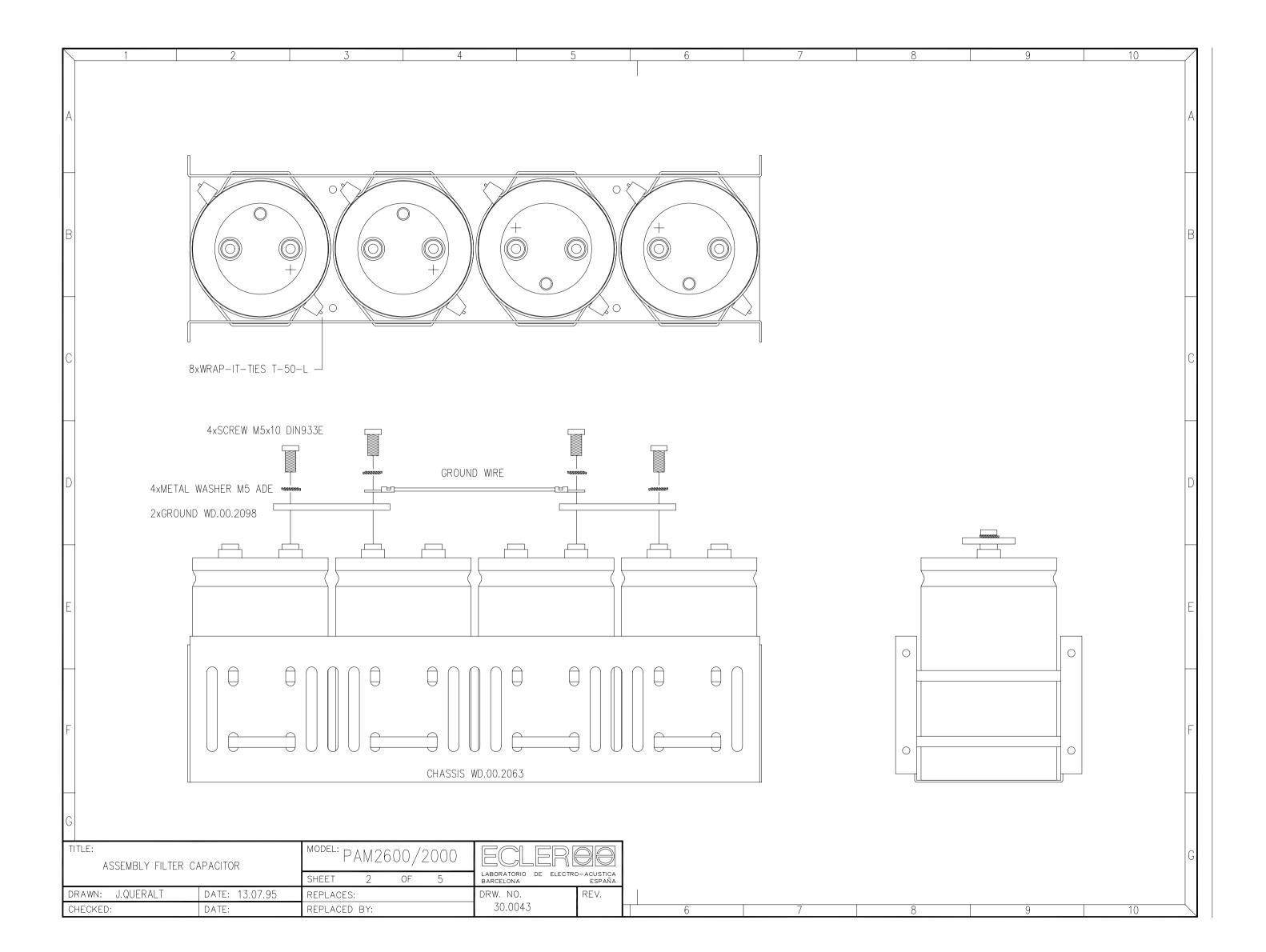


PARTS LIST: MECHANICAL DIAGRAM

MODEL : PAM2600/2000 DRW. No 30.0042PL REV: DATE: 060795 SHEET 1 OF 1 REPLACES: REPLACED BY:

## QUANTITY VALUE

- 18 SCREW M4x6 SPANLO DIN7985
- 6 SCREW M4x20 ALLEN DIN912
- 8 SCREW M4x12 SPANLO DIN965
- 16 SCREW M3x9 SPANLO DIN7985
- 8 METAL WASHER 3.2x6x1
- 4 INSULANT R19
- 2 CARDBOARD WD.03.0069
- 2 ASSEMBLED PRINTED CIRCUIT 11.504B
- 6 NUT M4
- 6 WASHER M4 ADE
- 1 HEAT SINK UPPER PART WD.00.2095
- 2 HEAT SINK WD.2090
- 1 SUPPORT WD.00.2086
- 4 CLAMP WD.00.1915
- 2 COOLING GILLS WD.00.2096
- 4 INSULANT TO126
- 4 INSULANT TO220



PARTS LIST: ASSEMBLY FILTER CAPACITOR

MODEL: PAM2600/2000 DRW. No 30.0043PL

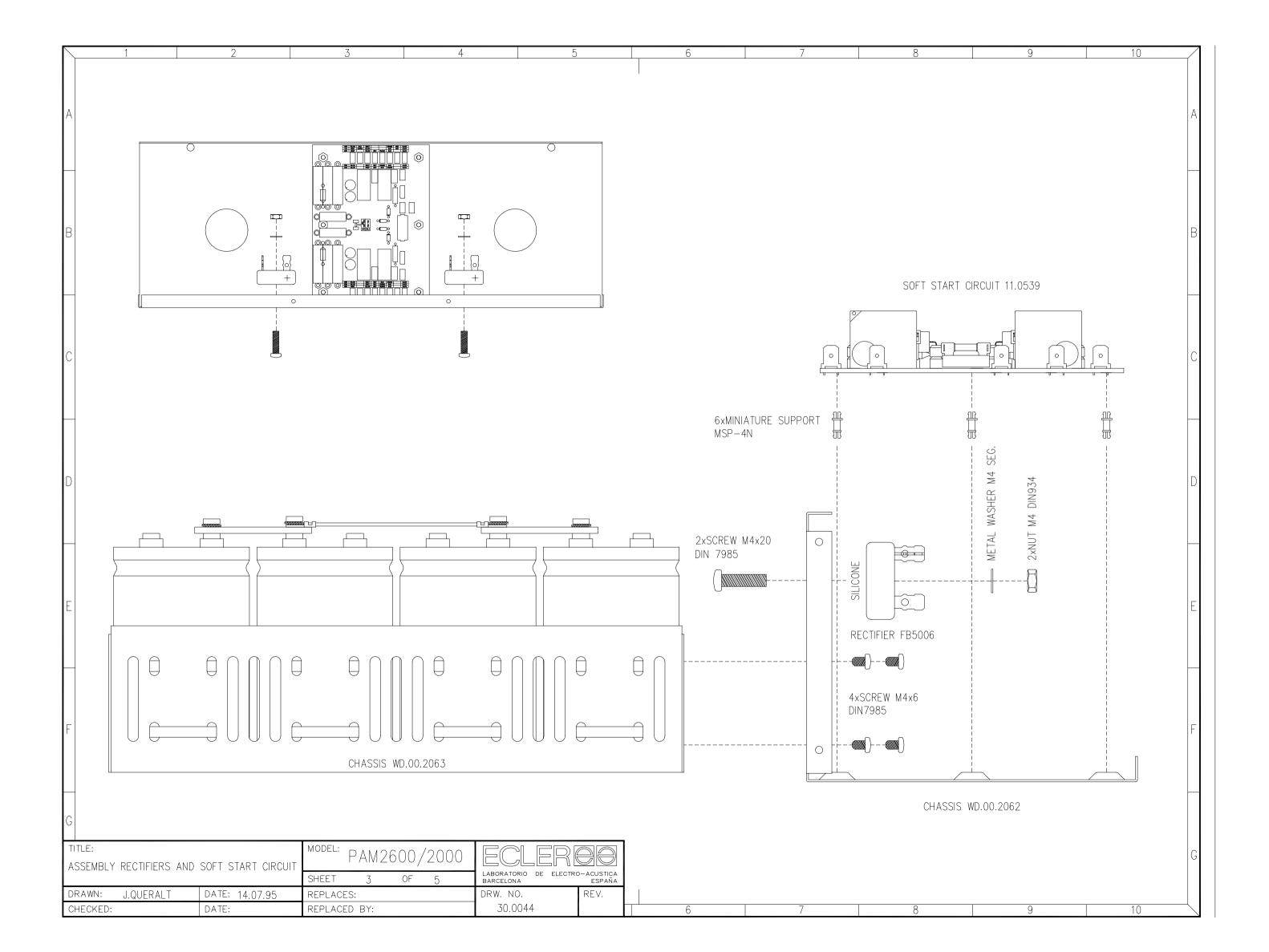
DATE: 130796 SHEET 1 OF 1 REPLACES: REPLACED BY:

REV:

# QUANTITY VALUE

1 CHASSIS WD.00.2063

- 8 WRAP-IT-TIES T-50-L
- 2 GROUND WD.00.2098
- 4 SCREW M5x10 DIN933E
- 4 METAL WASHER M5 ADE
- 1 GROUND WIRE7
- 4 CAPACITORS 22000µ/100V (PAM2600)
- 4 CAPACITORS 15000µ/80v (PAM2000)



PARTS LIST: ASSEMBLY RECTIFIERS AND SOFT START CIRCUIT

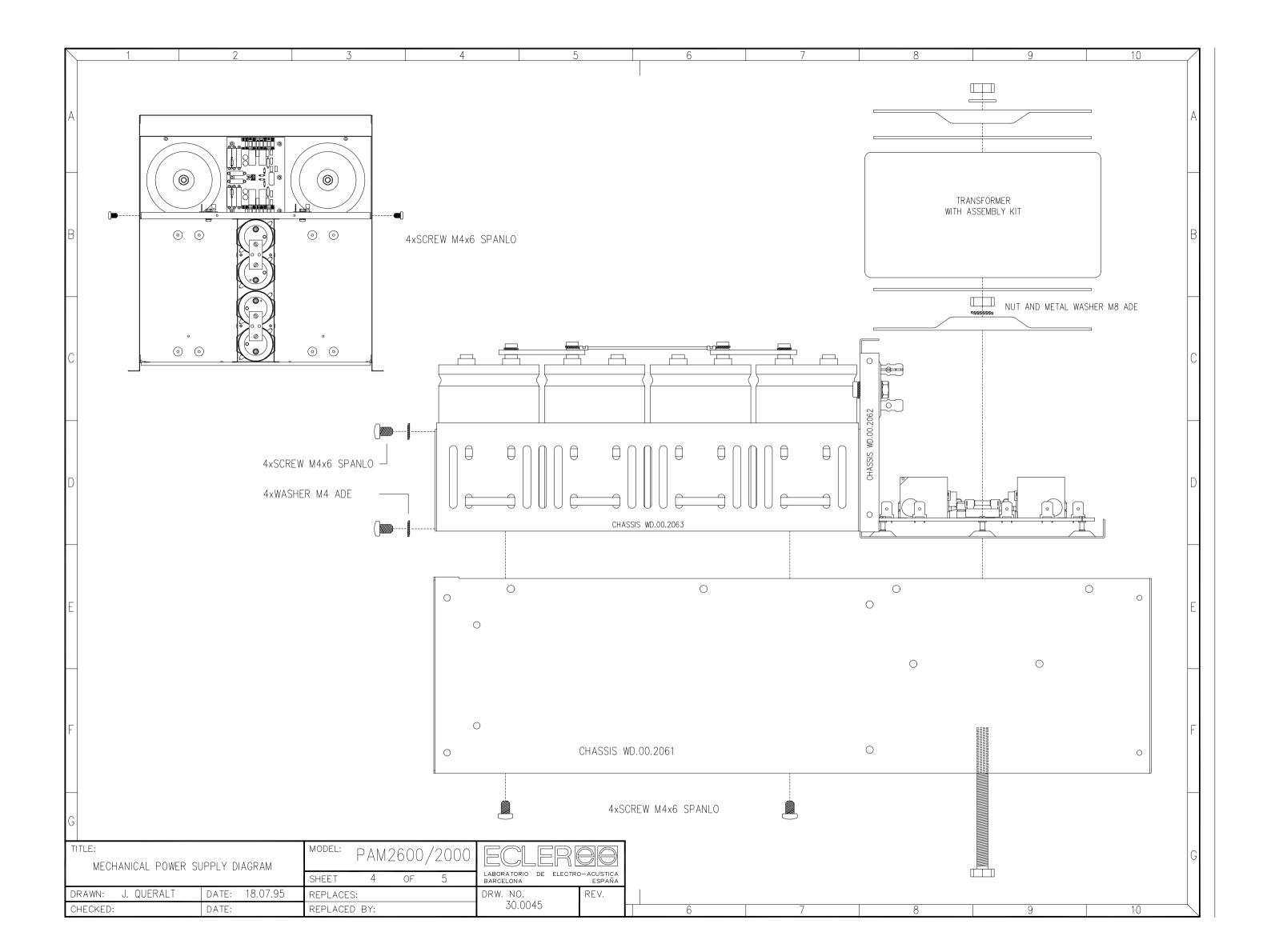
MODEL: PAM2600/2000 DRW. No 30.0044PL REV:

DATE: 140795 SHEET 1 OF 1 REPLACES: REPLACED BY:

## QUANTITY VALUE

1 ASSEMBLED CHASSIS WD.00.2063

- 1 CHASSIS WD.00.2062
- 1 ASSEMBLED SOFT START CIRCUIT 11.0539B
- 6 MINIATURE SUPPORT MSP-4N
- 2 SCREW M4x20 DIN7985
- 2 METAL WASHER M4 SEG.
- 2 NUT M4 DIN934
- 4 SCREW M4x6 DIN7985
- 2 RECTIFIER FB5006 (PAM2600)
- 2 RECTIFIER FB3506 (PAM2000)



PARTS LIST: MECHANICAL POWER SUPPLY DIAGRAM

MODEL: PAM2600/2000 DRW. No 30.0045PL REV:

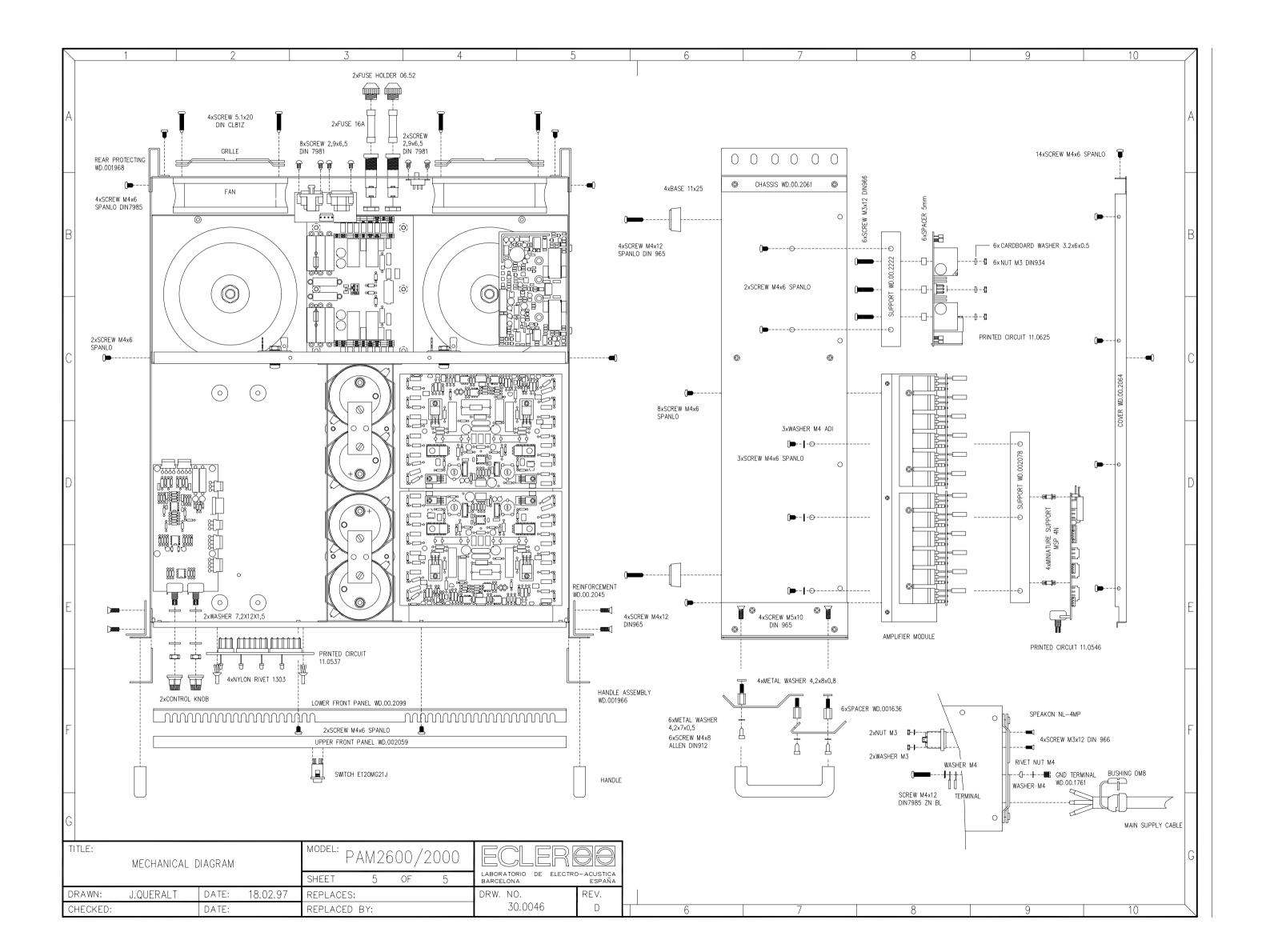
DATE: 180795 SHEET 1 OF 1 REPLACES: REPLACED BY:

# QUANTITY VALUE

1 ASSEMBLED CHASSIS 2063 AND CHASSIS 2062

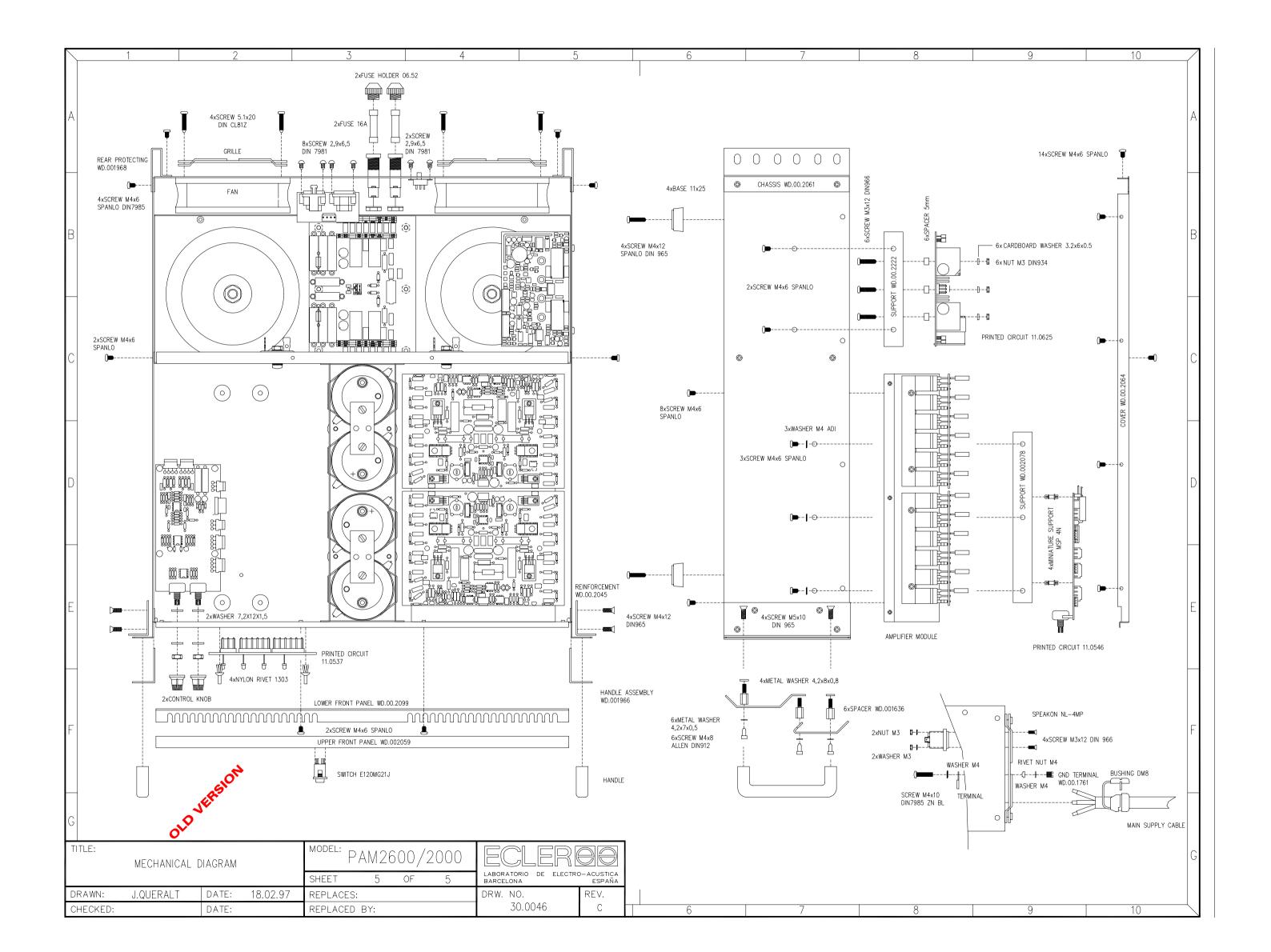
12 SCREW M4x6 SPANLO DIN7985

- 4 METAL WASHER M4 ADE
- 2 TRANSFORMER 64AD211 (PAM2600)
- 2 TRANSFORMER 51AD180 (PAM2000)
- 2 TRANSFORMER ASSEMBLY KIT



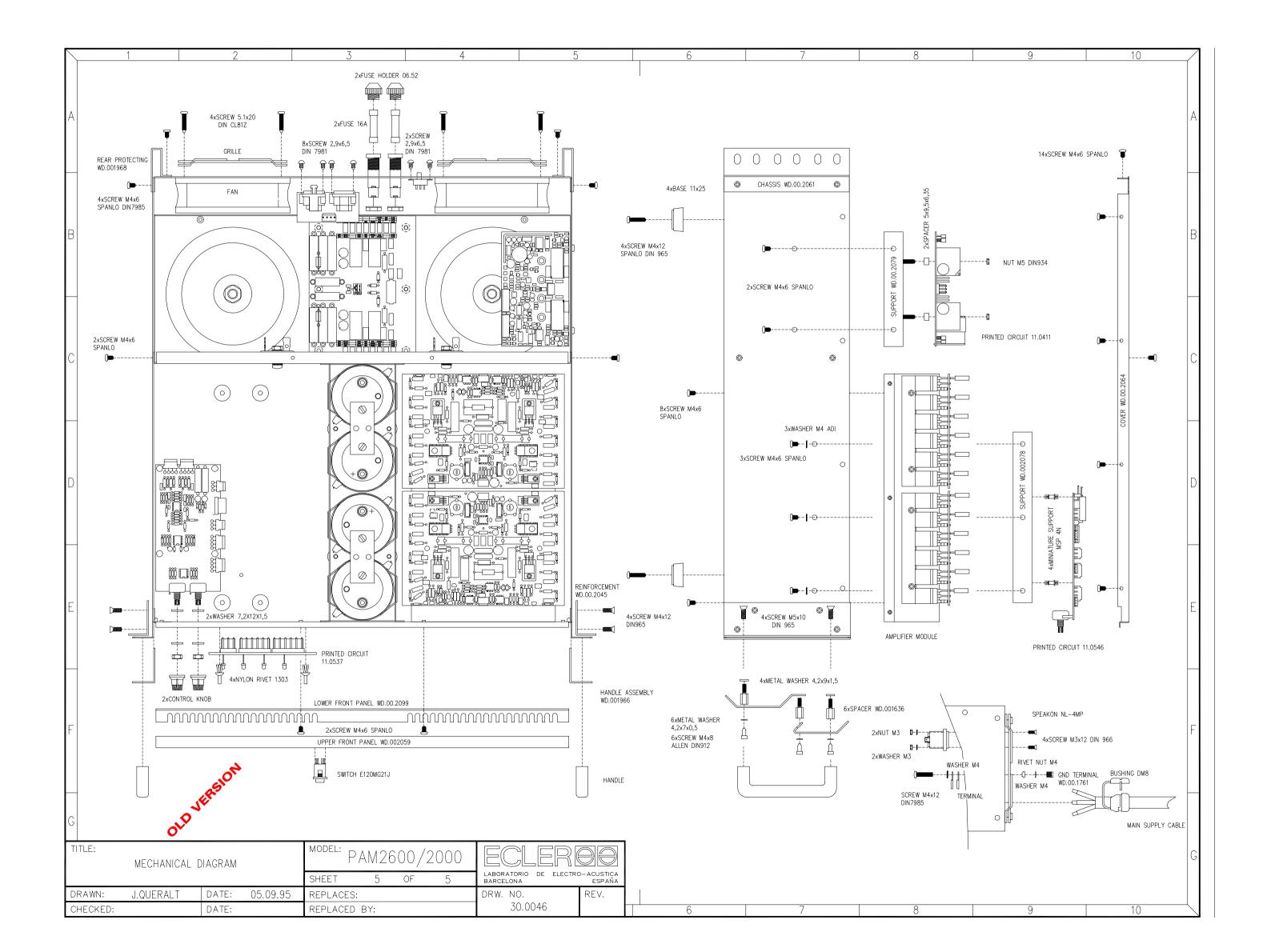
PARTS LIST: MECHANICAL DIAGRAM REV: D
MODEL:PAM2600/2000 DRW.N° 300046PL REPLACES:
DATE: 200599 SHEET 1 OF 1 REPLACED BY:

QUANTITY	DESCRIPT
8 43 8 4 1 10 10 6 1 1 4 3 1 1 10 6 4 6 2 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	SCREW 5.1x20 DIN CL81Z SCREW M4x6 SPANLO DIN7985 SCREW M4x12 DIN965 SCREW M4x12 SPANLO DIN965 SCREW M4x12 DIN7985 SCREW M3x12 DIN966 SCREW 2.9x6.5 DIN7981 SCREW M4x8 ALLEN DIN912 WASHER M4 ADE WASHER M4 ADE WASHER M4 ADI RIVET NUT M4 GND TERMINAL WD.00.1761 NUT M3 DIN934 SPACER WD.00.1636 METAL WASHER 4.2x9x1.5 METAL WASHER 4.2x7x0.5 NYLON RIVET 1303 SPACER 5mm WHITE D15 CONTROL KNOB REINFORCEMENT WD.00.2045 HANDLE ASSEMBLY WD.00.1966 ASSEMBLY PRINTED CIRCUIT 11.0537 LOWER FRONT PANEL WD.00.2099 UPPER FRONT PANEL WD.00.2099 UPPER FRONT PANEL WD.00.2059 SWITCH E120MG21J BASE 11x25 SUPPORT WD.00.2222 SUPPORT WD.00.2078 ASSEMBLY AMPLIFIER MODULE MINIATURE SUPPORT MSP 4N ASSEMBLED PRINTED CIRCUIT 11.0546 BUSHING DM8 MAIN SUPPLY CABLE CHASSIS WD.00.2061
2 2	REAR PROTECTING WD.00.1968 PAPST 4312 FAN
2 2 2 2	FAN GRILLE FUSE HOLDER 06.52 FUSE T16A ASSEMBLED PRINTED CIRCUIT 11.0625
1 1 2 6	ASSEMBLED PRINTED CIRCUIT 11.0538 SWITCH 17120 HANDLE 1578 CARDBOARD WASHER 3.2x6x0.5



PARTS LIST: MECHANICAL DIAGRAM REV: C
MODEL:PAM2600/2000 DRW.N° 300046PL REPLACES:
DATE: 200599 SHEET 1 OF 1 REPLACED BY:

QUANTITY	DESCRIPT
QUANTITY  8 43 8 4 1 10 10 6 1 1 4 3 1 1 10 6 4 6 4 6 2 2 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	DESCRIPT  SCREW 5.1x20 DIN CL81Z SCREW M4x6 SPANLO DIN7985 SCREW M4x12 DIN965 SCREW M4x12 SPANLO DIN965 SCREW M4x10 DIN7985 SCREW M3x12 DIN966 SCREW 2.9x6.5 DIN7981 SCREW M4x8 ALLEN DIN912 WASHER M4 ADE WASHER M4 ADE WASHER M4 ADI RIVET NUT M4 GND TERMINAL WD.00.1761 NUT M3 DIN934 SPACER WD.00.1636 METAL WASHER 4.2x7x0.5 NYLON RIVET 1303 SPACER 5mm WHITE D15 CONTROL KNOB REINFORCEMENT WD.00.2045 HANDLE ASSEMBLY WD.00.1966 ASSEMBLY PRINTED CIRCUIT 11.0537 LOWER FRONT PANEL WD.00.2099 UPPER FRONT PANEL WD.00.2099 UPPER FRONT PANEL WD.00.2059 SWITCH E120MG21J BASE 11x25 SUPPORT WD.00.2078 ASSEMBLY AMPLIFIER MODULE MINIATURE SUPPORT MSP 4N ASSEMBLED PRINTED CIRCUIT 11.0546 BUSHING DM8 MAIN SUPPLY CABLE CHASSIS WD.00.2061
2 2 2	REAR PROTECTING WD.00.1968 PAPST 4312 FAN FAN GRILLE
2 2 2 1 1 2 6	FUSE HOLDER 06.52 FUSE T16A ASSEMBLED PRINTED CIRCUIT 11.0625 ASSEMBLED PRINTED CIRCUIT 11.0538 SWITCH 17120 HANDLE 1578 CARDBOARD WASHER 3.2x6x0.5



PARTS LIST: MECHANICAL DIAGRAM

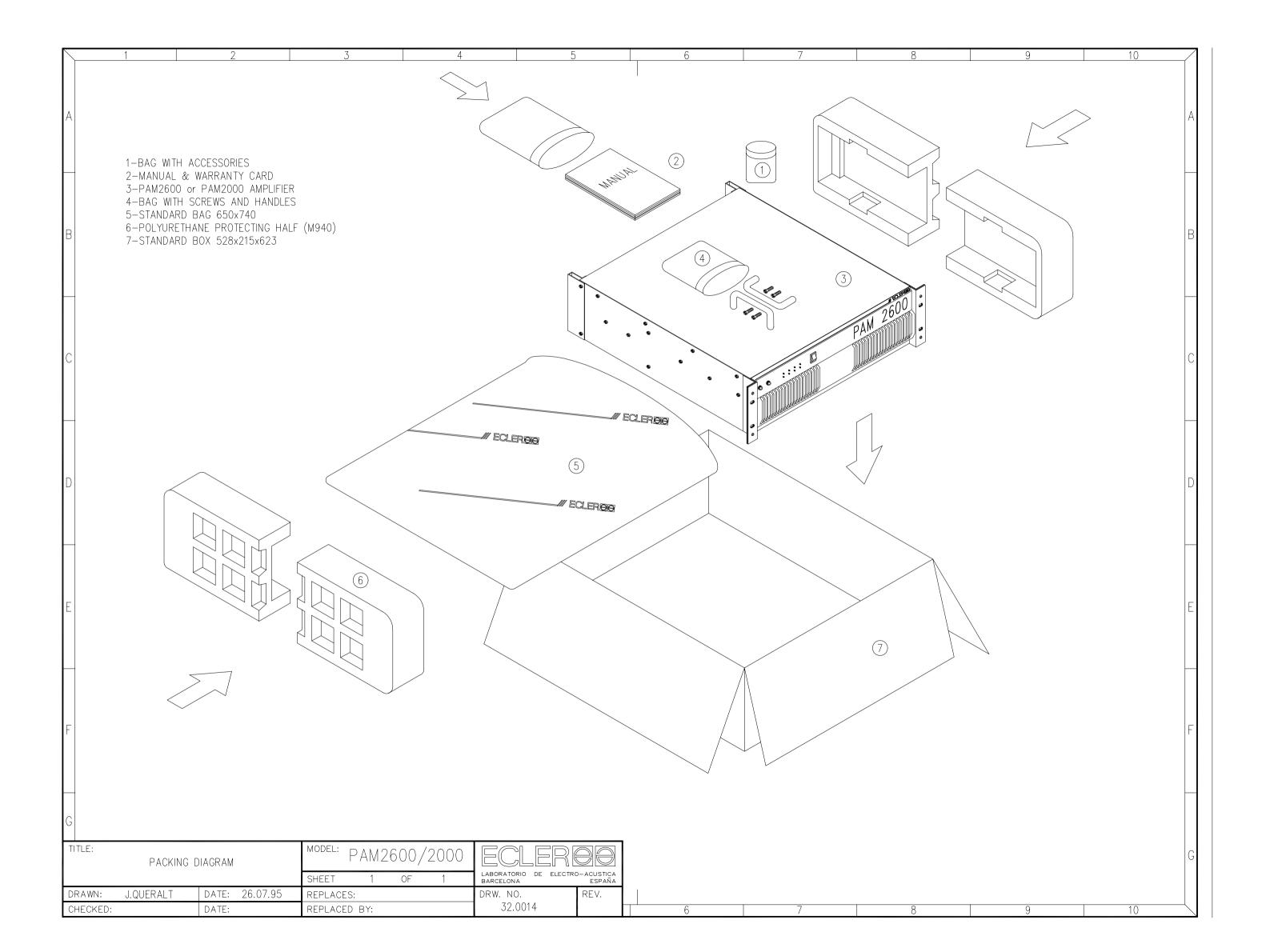
MODEL : PAM2600/2000 DRW. No 30.0046PL REV:

DATE: 050995 SHEET 1 OF 1 REPLACES: REPLACED BY:

#### QUANTITY VALUE

- 8 SCREW 5.1x20 DIN CL81Z
- 43 SCREW M4x6 SPANLO DIN7985
- 8 SCREW M4x12 DIN965
- 4 SCREW M4x12 SPANLO DIN965
- 1 SCREW M4x12 DIN7985
- 4 SCREW M3x12 DIN966
- 10 SCREW 2.9x6.5 DIN7981
- 4 SCREW M5x10 DIN965
- 6 SCREW M4x8 ALLEN DIN912
- 1 WASHER M4 ADE
- 1 WASHER M4 SEG.
- 4 WASHER M3 ADE
- 3 WASHER M4 ADI
- 1 RIVET NUT M4
- 1 GND TERMINAL WD.00.1761
- 4 NUT M3 DIN934
- 4 NUT M5 DIN934
- 6 SPACER WD.00.1636
- 4 METAL WASHER 4.2x9x1.5
- 6 METAL WASHER 4.2x7x0.5
- 4 NYLON RIVET 1303
- 4 SPACER 5x9.5x6.35
- 2 WHITE D15 CONTROL KNOB
- 2 REINFORCEMENT WD.00.2045
- 2 HANDLE ASSEMBLY WD.00.1966
- 1 ASSEMBLY PRINTED CIRCUIT 11.0537
- 1 LOWER FRONT PANEL WD.00.2099
- 1 UPPER FRONT PANEL WD.00.2059
- 1 SWITCH E120MG21J
- 4 BASE 11x25
- 2 SUPPORT WD.00.2079
- 1 SUPPORT WD.00.2078
- 2 ASSEMBLY AMPLIFIER MODULE
- 4 MINIATURE SUPPORT MSP 4N
- 1 ASSEMBLED PRINTED CIRCUIT 11.0546
- 1 BUSHING DM8
- 1 MAIN SUPPLY CABLE
- 1 CHASSIS WD.00.2061
- 2 REAR PROTECTING WD.00.1968
- 2 PAPST 4312 FAN
- 2 FAN GRILLE
- 2 FUSE HOLDER 06.52
- 2 FUSE T16A
- 2 ASSEMBLED PRINTED CIRCUIT 11.0411
- 1 ASSEMBLED PRINTED CIRCUIT 11.0538
- 1 SWITCH 17120
- 2 HANDLE 1578





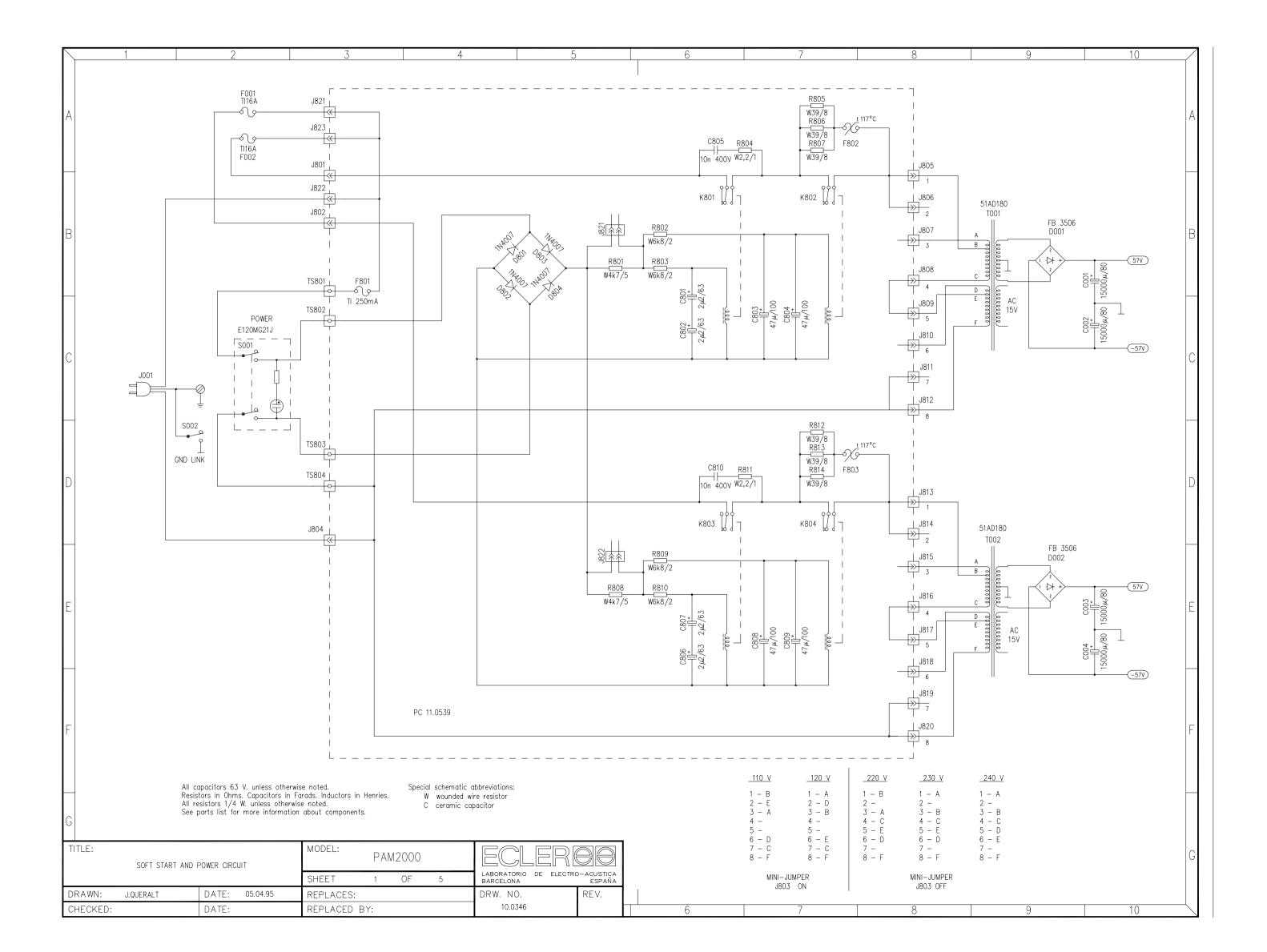
PARTS LIST: PACKING DIAGRAM MODEL: PAM2600/2000 DRW. No 32.0014PL

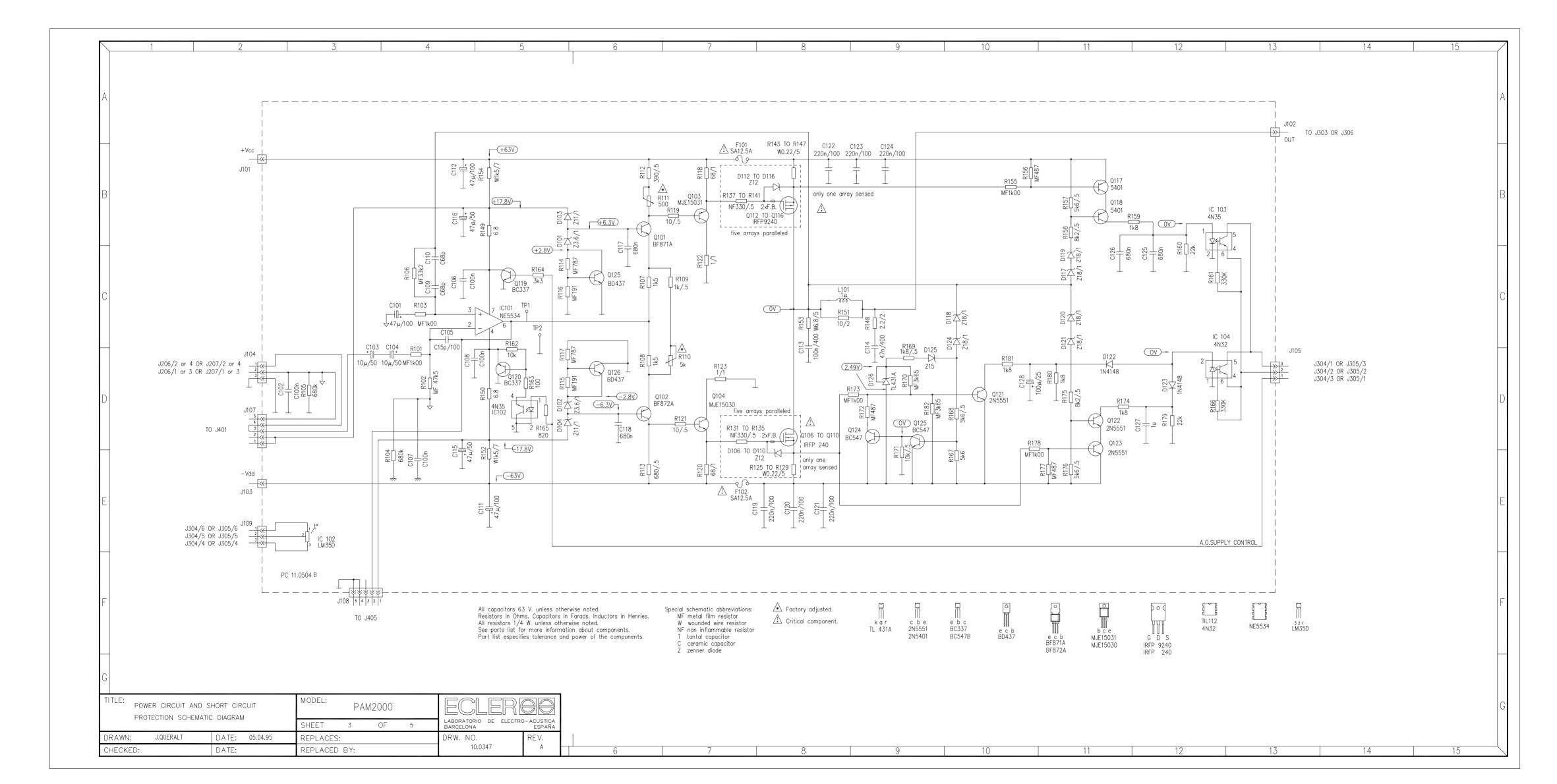
DATE: 260795 SHEET 1 OF 1 REPLACES: REPLACED BY:

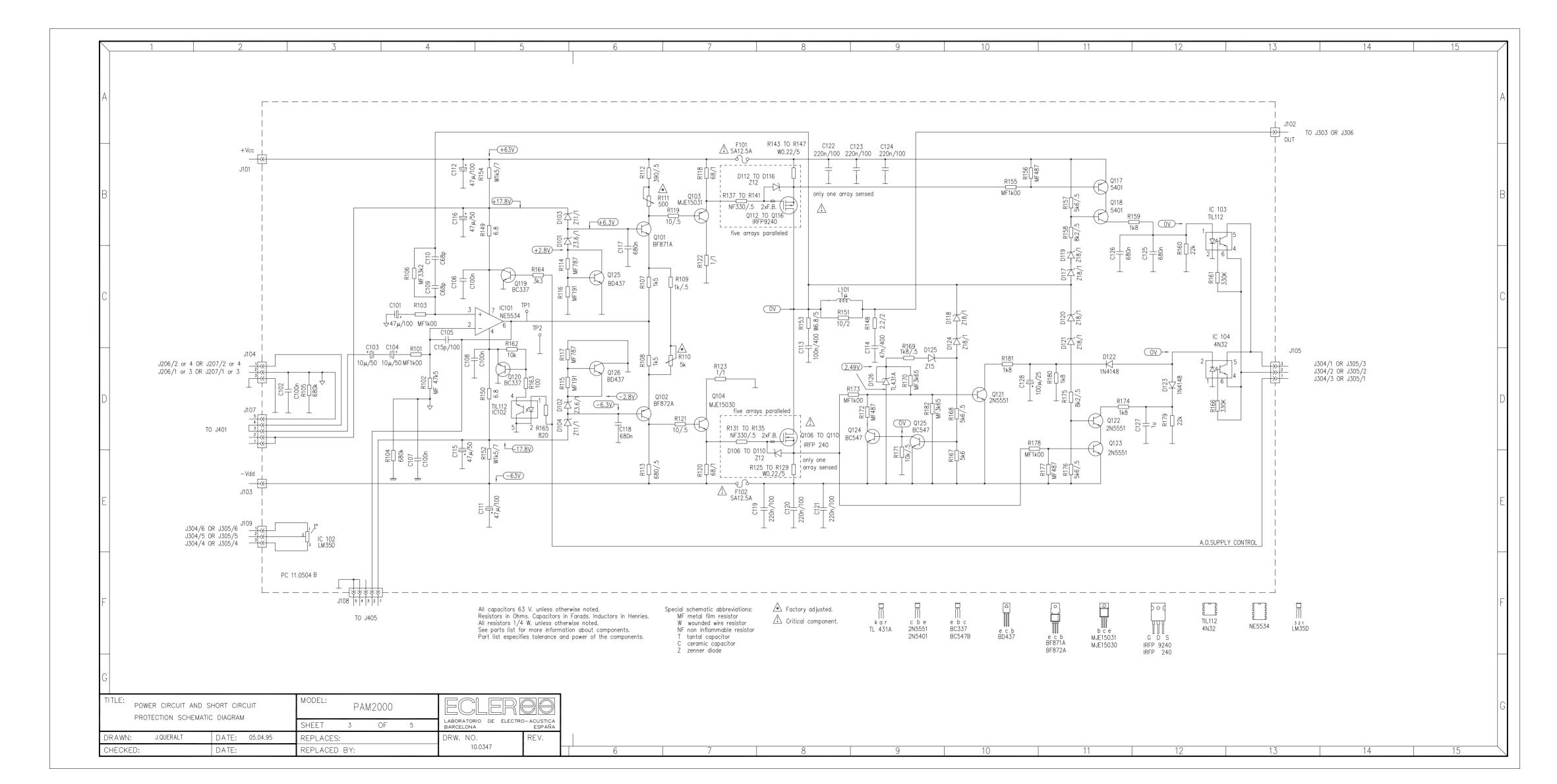
REV:

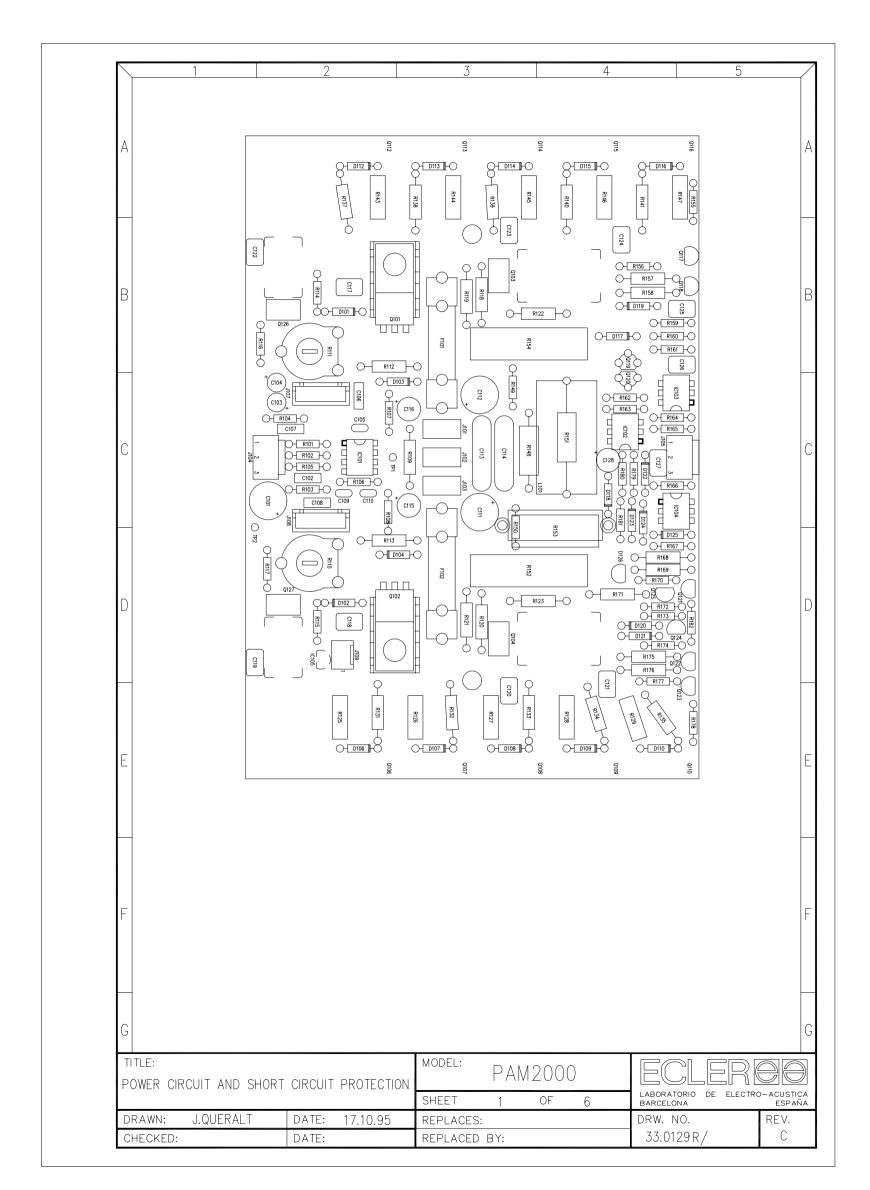
# **QUANTITY VALUE**

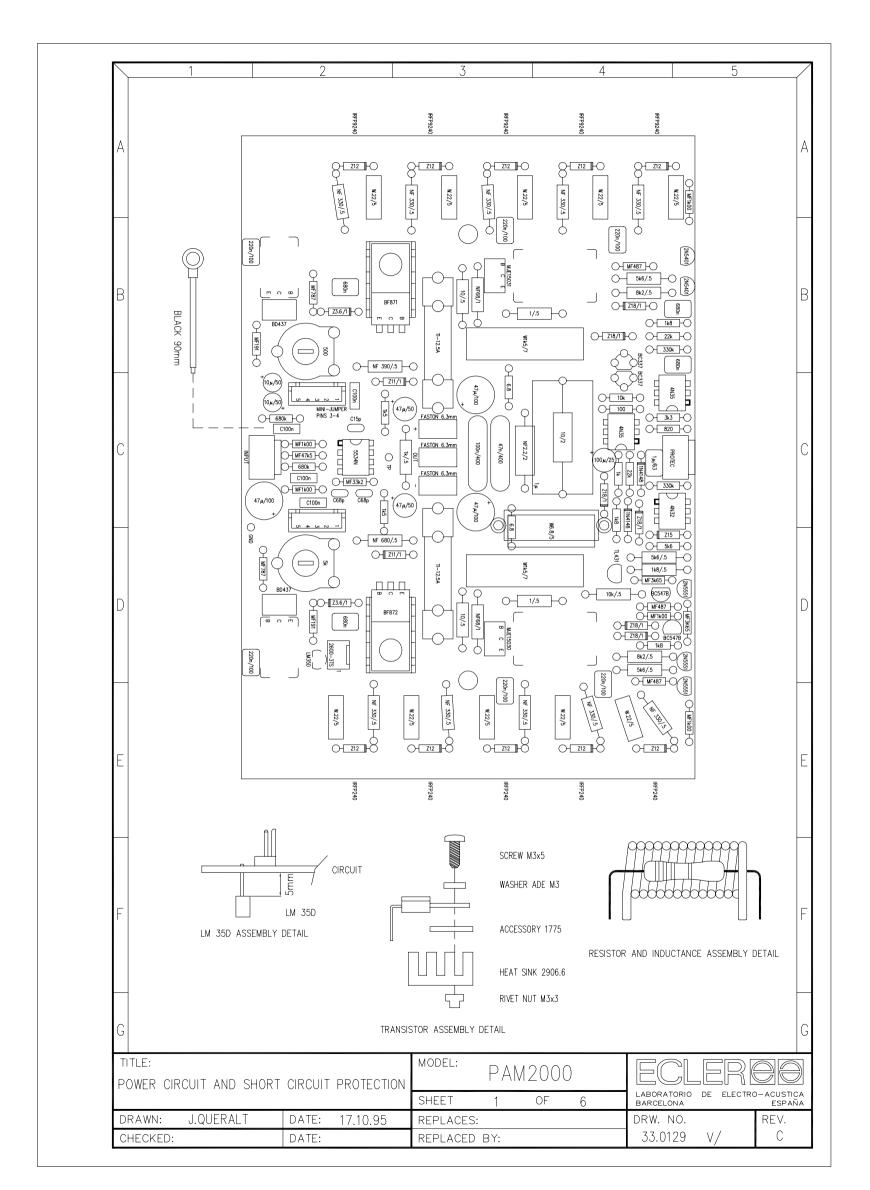
- 4 METAL WASHER 5x11.5x0.8
- 4 WASHER AT 5x11.5x3.5 ABS BLACK
- 2 FUSE T16A
- 1 STANDARD BOX 528x215x623
- 4 POLYURETHANE PROTECTING HALF (M940)
- 1 STANDARD BAG 650x740
- 1 BAG 60x80
- 4 SCREW M5x10 DIN965
- 2 HANDLE 1578
- 1 MANUAL
- 1 WARRANTY CARD











MODEL:PAM2000 DRW.N° 33.0129PL REV : A

DATE: 000621 SHEET 1 OF 3 REPLACED BY:

## REFERENCE VALUE

C101  $47\mu/100$ C102 C100n C103  $10\mu/50$ C104  $10\mu/50$ C105 C15p C106 C100n C107 C100n C108 C100n C109 C68p C110 C68p C111  $47\mu/100$ C112  $47\mu/100$ C113 100n/400 C114 47n/400 C115  $47\mu/50$ C116  $47\mu/50$ C117 680n C118 680n C119 220n/100 C120 220n/100 C121 220n/100 C122 220n/100 C123 220n/100 C124 220n/100 C125 680n C126 680n C127  $1\mu/63$ C128  $100 \mu / 25$ D101 Z3.6/1 D102 Z3.6/1 D103 Z11/1 D104 Z11/1 D106 Z12 D107 Z12 Z12 D108 D109 Z12 Z12 D110 Z12 D112 D113 Z12 Z12 D114 D115 Z12 Z12 D116 D117 Z18/1 D118 Z18/1 D119 Z18/1 D120 Z18/1 D121 Z18/1 D122 1N4148 D123 1N4148 D124 Z18/1 D125 Z15 D126 TL431 F101 TI-12.5A F102 TI-12.5A IC101 5534N IC102 4N35 IC103 4N35

IC104

4N32

MODEL:PAM2000 DRW.Nº 33.0129PL REV: A

SHEET 2 OF REPLACED BY: DATE: 000621 3

#### REFERENCE **VALUE**

IC105 LM35D

J101 FASTON 6.3mm J102 FASTON 6.3mm J103 FASTON 6.3mm

J104 B3P-VH J105 B3P-VH J107 B5B-XH J108 B5B-XH J109 2600-3TS Q101 BF871 Q102 BF872 Q103 MJE15031 Q104 MJE15030 Q106 IRFP240 Q107 IRFP240 Q108 IRFP240 Q109 IRFP240 IRFP240 Q110 Q112 IRFP9240 Q113 IRFP9240 Q114 IRFP9240 Q115 IRFP9240 Q116 IRFP9240 Q117 2N5401 Q118 2N5401 Q119 BC337 Q120 BC337 Q121 2N5551 Q122 2N5551 Q123 2N5551 Q124 BC547B

Q125 BC547B Q126 BD437 Q127 **BD437** R101 MF1k R102 MF47k5 R103 MF1k00 R104 680k R105 680k R106 MF33k2 R107 1k5 R108 1k5 R109 1k/.5

R110

R111

R112

R125

R113 NF680  $\Omega$  /.5 R114 MF787  $\Omega$ R115 MF191  $\Omega$ MF191  $\Omega$ R116 R117 MF787  $\Omega$ R118 NF68  $\Omega$  /1 R119  $10 \Omega /.5$ R120 NF68  $\Omega$  /1 R121  $10 \Omega$  /.5 R122  $1 \Omega /.5$ R123  $1 \Omega /.5$ 

5k

 $500 \Omega$ 

NF390/.5

 $W.22 \Omega /5$ 

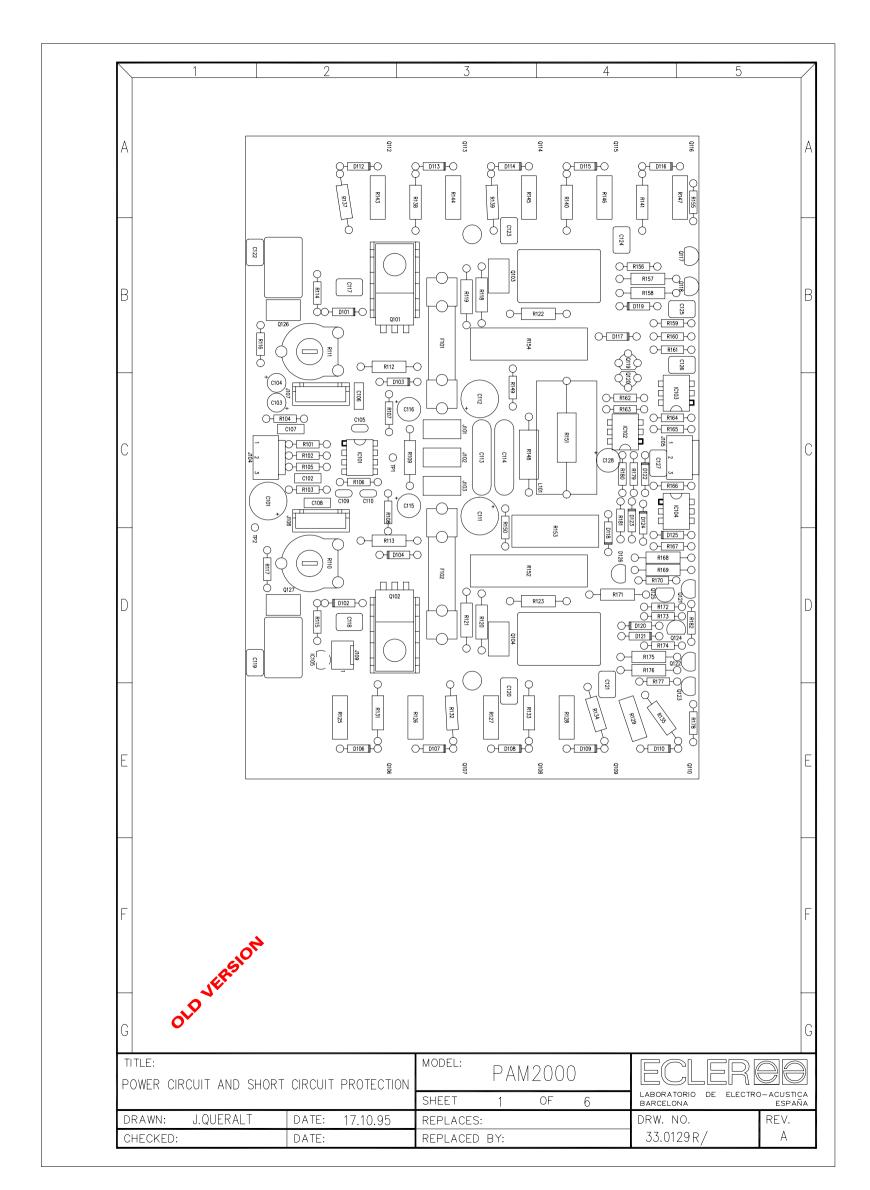
MODEL:PAM2000 DRW.N° 33.0129PL REV : A

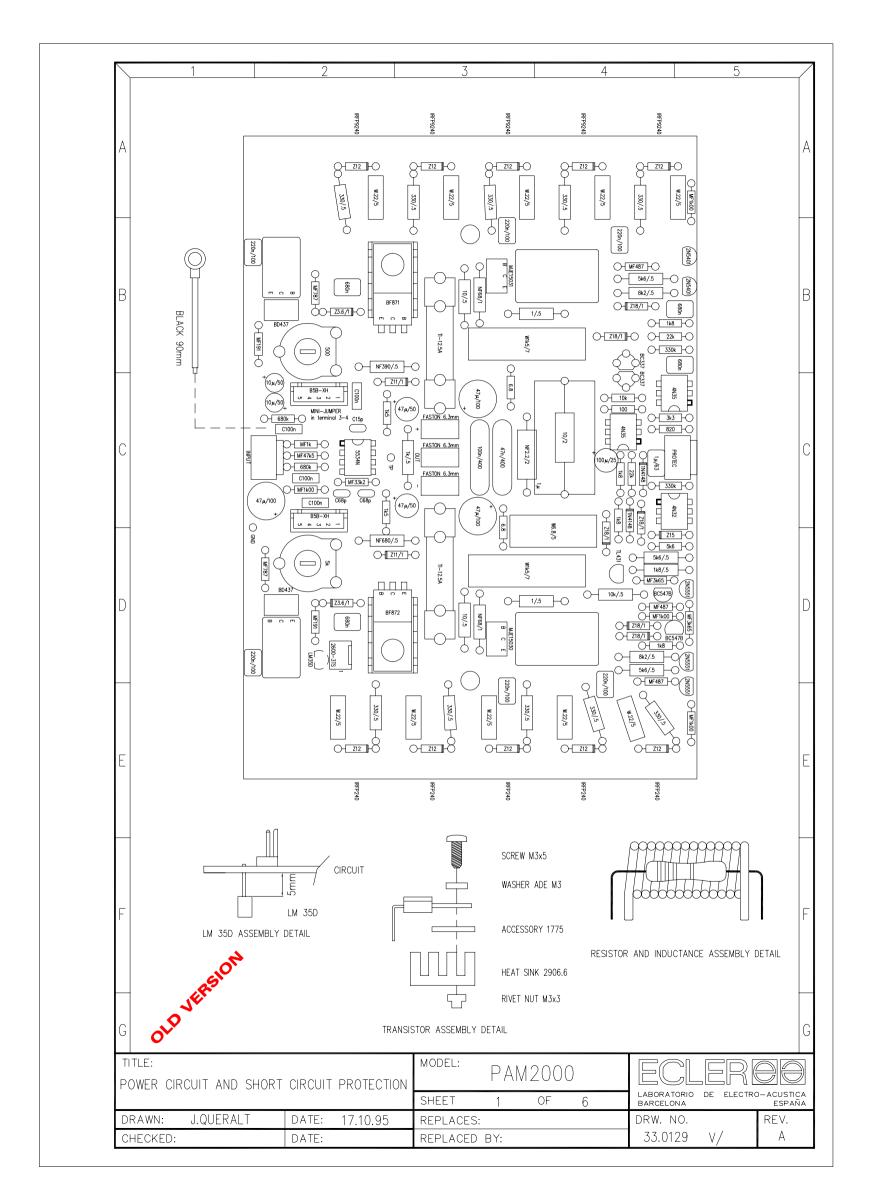
DATE: 000621 SHEET 3 OF 3 REPLACED BY:

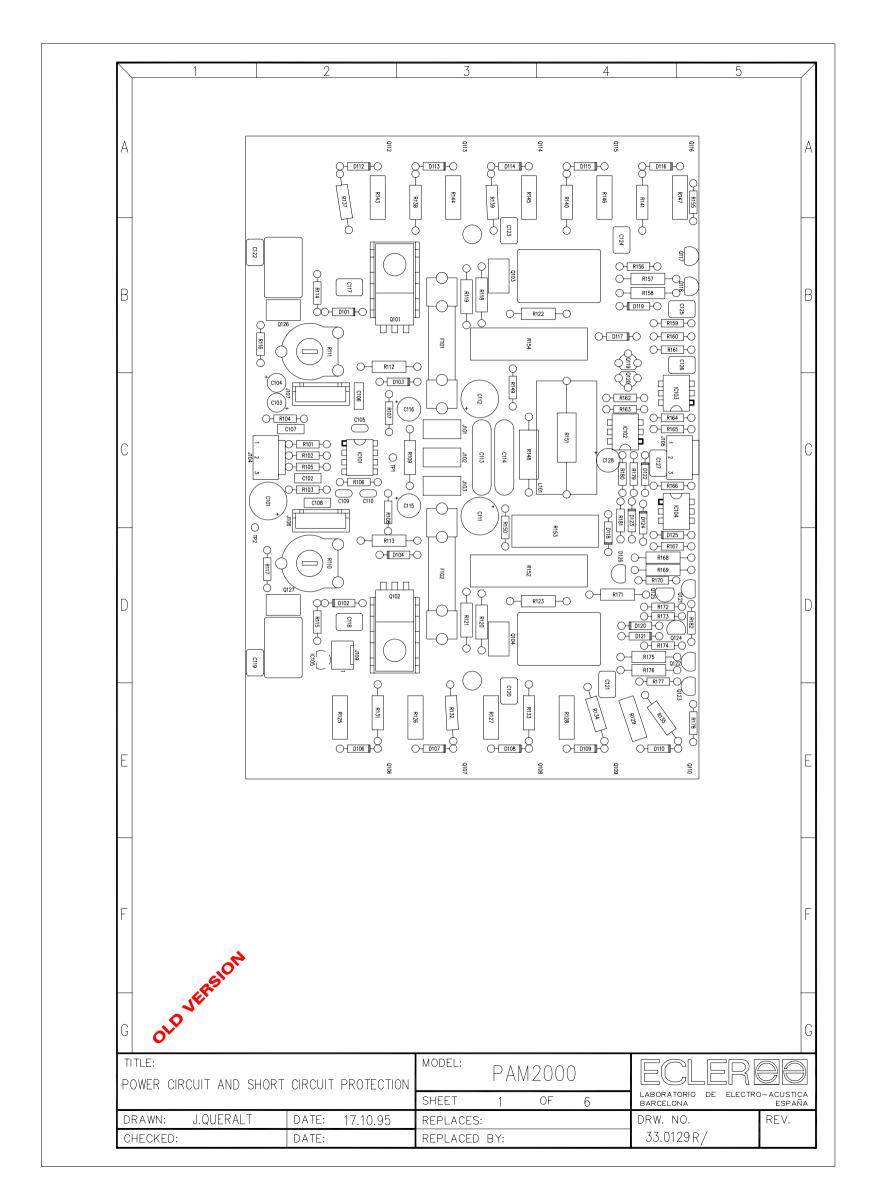
#### REFERENCE VALUE

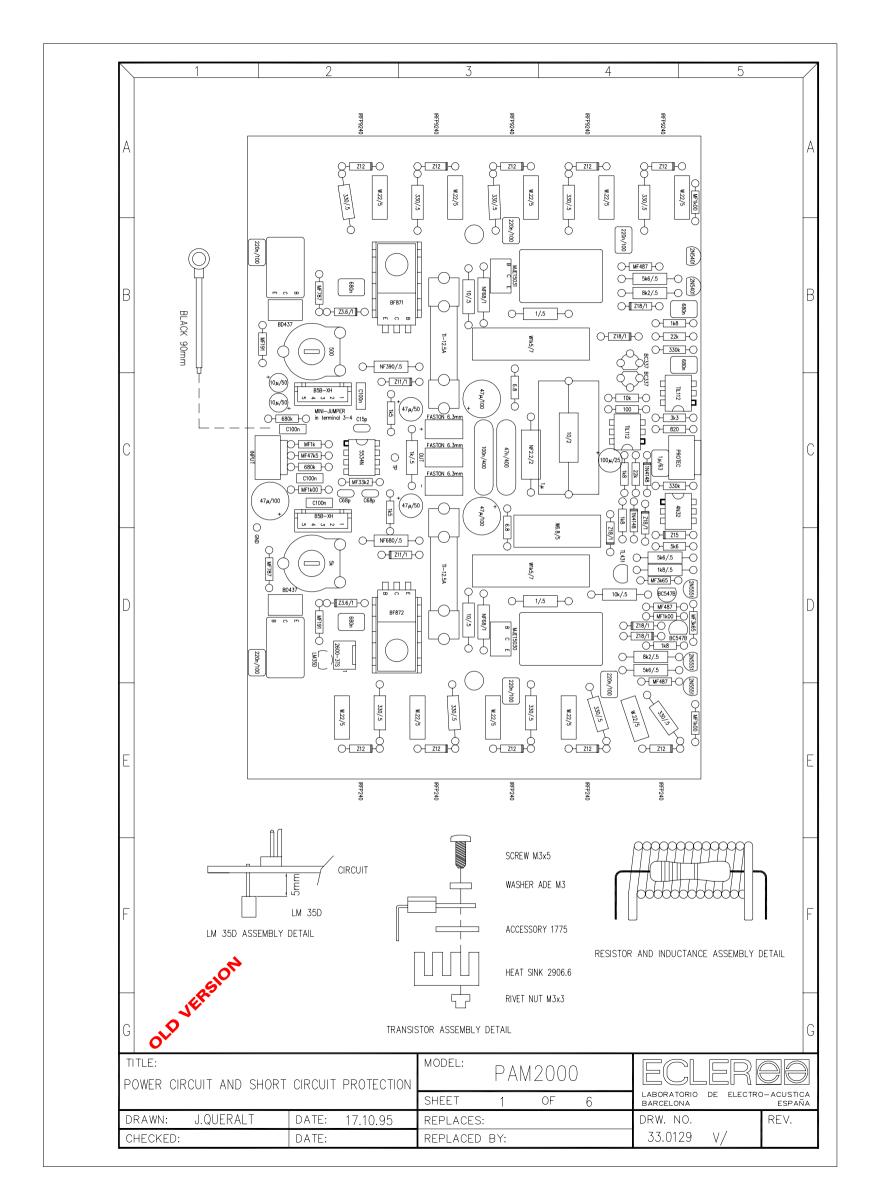
R126  $W.22 \Omega /5$ R127  $W.22 \Omega /5$ R128  $W.22~\Omega$  /5 R129  $W.22 \Omega /5$ R131 330  $\Omega$  /.5 R132  $330 \Omega /.5$ R133  $330 \Omega /.5$ R134  $330 \Omega /.5$ R135  $330 \Omega /.5$ R137  $330 \Omega /.5$ R138  $330 \Omega /.5$ R139 330  $\Omega$  /.5 R140  $330~\Omega$  /.5 R141  $330 \Omega /.5$ R143  $W.22 \Omega /5$ R144  $W.22 \Omega /5$ R145  $W.22 \Omega /5$  $W.22 \Omega /5$ R146 R147  $W.22 \Omega /5$ NF2.2  $\Omega$  /2 R148 R149  $6.8 \Omega$ R150  $6.8 \Omega$ R151  $10 \Omega / 2$ R152 W1k5/7 W6.8  $\Omega$  /5 R153 R154 W1k5/7 R155 MF1k00 R156 MF487  $\Omega$ R157 5k6/.5 R158 8k2/.5 R159 1k8 R160 22k 330k R161 R162 10k R163  $100 \Omega$ R164 3k3 R165  $820 \Omega$ 330k R166 R167 5k6 R168 5k6/.5 R169 1k8/.5 R170 MF3k65 R171 10k/.5 MF487  $\Omega$ R172 R173 MF1k00 R174 1k8 R175 8k2/.5 R176 5k6/.5 R177 MF487  $\Omega$ R178 MF1k00 R179 22k R180 1k8 R181 1k8 R182 MF3k65

PC 11.0504B PRINTED CIRCUIT WIRE BLACK 90mm whit TER.









MODEL:PAM2000 DRW.N° 33.0129PL REV:

DATE: 000621 SHEET 1 OF 3 REPLACED BY:

## REFERENCE VALUE

C101  $47\mu/100$ C102 C100n C103  $10\mu/50$ C104  $10\mu/50$ C105 C15p C106 C100n C107 C100n C108 C100n C109 C68p C110 C68p C111  $47\mu/100$ C112  $47\mu/100$ C113 100n/400 C114 47n/400 C115  $47\mu/50$ C116  $47\mu/50$ C117 680n C118 680n C119 220n/100 C120 220n/100 C121 220n/100 C122 220n/100 C123 220n/100 C124 220n/100 C125 680n C126 680n C127  $1\mu/63$ C128  $100 \mu / 25$ D101 Z3.6/1 D102 Z3.6/1 D103 Z11/1 D104 Z11/1 D106 Z12 D107 Z12 Z12 D108 D109 Z12 Z12 D110 D112 Z12 D113 Z12 Z12 D114 D115 Z12 Z12 D116 D117 Z18/1 D118 Z18/1 D119 Z18/1 D120 Z18/1 D121 Z18/1 D122 1N4148 D123 1N4148 D124 Z18/1 D125 Z15 D126 TL431 F101 TI-12.5A F102 TI-12.5A IC101 5534N IC102 **TIL112** 

IC103

IC104

**TIL112** 

4N32

MODEL:PAM2000 DRW.N° 33.0129PL REV:

DATE: 000621 SHEET 2 OF 3 REPLACED BY:

#### REFERENCE VALUE

IC105 LM35D

 J101
 FASTON 6.3mm

 J102
 FASTON 6.3mm

 J103
 FASTON 6.3mm

J103 J104 B3P-VH J105 B3P-VH J107 B5B-XH J108 B5B-XH J109 2600-3TS Q101 BF871 Q102 BF872 Q103 MJE15031 Q104 MJE15030 Q106 IRFP240 Q107 IRFP240 Q108 IRFP240 Q109 IRFP240 IRFP240 Q110 Q112 IRFP9240 Q113 IRFP9240 Q114 IRFP9240 Q115 IRFP9240 Q116 IRFP9240 Q117 2N5401 Q118 2N5401 Q119 BC337 Q120 BC337 Q121 2N5551 Q122 2N5551 Q123 2N5551 Q124 BC547B Q125 BC547B Q126 BD437 Q127 **BD437** R101 MF1k R102 MF47k5 R103 MF1k00 R104 680k R105 680k R106 MF33k2 R107 1k5 R108 1k5 R109 1k/.5 R110 5k R111  $500 \Omega$ R112 NF390/.5 NF680  $\Omega$  /.5 R113 R114 MF787  $\Omega$ R115 MF191  $\Omega$ R116 MF191  $\Omega$ R117 MF787  $\Omega$ R118 NF68  $\Omega$  /1 R119  $10 \Omega /.5$ R120 NF68  $\Omega$  /1

 $10 \Omega$  /.5

 $1 \Omega /.5$ 

 $1 \Omega /.5$ 

 $W.22 \Omega /5$ 

R121

R122

R123

R125

MODEL:PAM2000 DRW.N° 33.0129PL REV:

DATE: 000621 SHEET 3 OF 3 REPLACED BY:

## REFERENCE VALUE

R126  $W.22 \Omega /5$ R127  $W.22 \Omega /5$ R128  $W.22 \Omega /5$ R129  $W.22 \Omega /5$ R131 330  $\Omega$  /.5 R132  $330 \Omega /.5$ R133  $330 \Omega /.5$ R134  $330 \Omega /.5$ R135  $330 \Omega /.5$ R137  $330 \Omega /.5$ R138  $330 \Omega /.5$ R139 330  $\Omega$  /.5 R140  $330~\Omega$  /.5 R141  $330 \Omega /.5$ R143  $W.22 \Omega /5$ R144  $W.22 \Omega /5$ R145  $W.22 \Omega /5$ R146  $W.22 \Omega /5$ R147  $W.22 \Omega /5$ NF2.2  $\Omega$  /2 R148 R149  $6.8 \Omega$ R150  $6.8 \Omega$ R151  $10 \Omega / 2$ R152 W1k5/7 W6.8  $\Omega$  /5 R153 R154 W1k5/7 R155 MF1k00 R156 MF487  $\Omega$ R157 5k6/.5 R158 8k2/.5 R159 1k8 R160 22k 330k R161 R162 10k R163  $100 \Omega$ R164 3k3 R165  $820 \Omega$ 330k R166 R167 5k6 R168 5k6/.5 R169 1k8/.5 R170 MF3k65 R171 10k/.5 MF487  $\Omega$ R172 R173 MF1k00 R174 1k8 R175 8k2/.5

PC 11.0504B PRINTED CIRCUIT WIRE BLACK 90mm whit TER.

5k6/.5

MF487  $\Omega$ 

MF1k00

MF3k65

22k

1k8

1k8

R176

R177

R178

R179

R180

R181

R182