

TYPE

79-02A DUAL TRACE PLUG-IN
Instruction Manual

Serial No. _____

This Plug-In Module is designed for use
with the Fairchild Type 766H/F Series
Oscilloscope.

FAIRCHILD

INSTRUMENTATION

A DIVISION OF FAIRCHILD CAMERA AND INSTRUMENT CORPORATION

50 SOMERSET PLACE, CLIFTON, NEW JERSEY, U.S.A.

TABLE OF CONTENTS

<u>Section</u>	<u>Title</u>	<u>Page</u>
1.	TECHNICAL SUMMARY	
1-1	Introduction	1-1
1-2	Features	1-1
1-3	Technical Summary (Specifications)	1-2
	Type 79-02A Nominal Frequency Response Curve	1-5
2.	OPERATING INSTRUCTIONS	
2-1	First Time Operation	2-1
2-2	Applying a Signal	2-1
2-3	DC Balance Adjustment	2-1
2-4	Setting Gain of Dual-Trace Amplifier	2-2
2-5	Input-Selector Switch	2-4
2-6	Obtaining a Display	2-7
2-7	Cabling Techniques in the Nanosecond Realm	2-8
2-8	Use of Probes	2-16
2-9	Dual-Trace Operation	2-20
2-10	Dual Trace Triggering	2-21
2-11	Setting Up Amplifier for Greater Input Sensitivity	2-22
2-12	Voltage Measurements	2-22
2-14	Measuring Short Rise Times	2-26
3.	FUNCTIONAL BLOCK DIAGRAMS	
4.	PERFORMANCE ASSURANCE TEST	
4-1	Maintenance Check to Assure Performance	4-1
4-2	Checking DC Balance Adjustment	4-2
4-3	Checking Sensitivity of Channels 1 & 2	4-2
4-4	Checking Fast Rise Time of Channels 1 & 2	4-3
4-5	Checking Mode Switch	4-4
4-6	Checking Chopped Operation	4-4
5.	MAINTENANCE AND RECALIBRATION	
5-1	Introduction	5-1
5-2	Removal and Replacement of Parts	5-1
5-3	Servicing Hints	5-1
5-4	Gaining Access to Chassis	5-4
5-5	Test Equipment Required for Service Adjustments	5-4
5-6	Gas Compensation Adjustments	5-6

TABLE OF CONTENTS
(Continued)

<u>Section</u>	<u>Title</u>	<u>Page</u>
5. (concluded)		
5-7	DC and Bridge Bal Adjustment	5-6
5-8	Invert Balance Adjustment	5-7
5-9	X10 Level Adjustment	5-8
5-10	Output Current Adjustment	5-9
5-11	Gain Adjustments	5-9
5-12	X10 Cal Adjustment	5-10
5-13	Trigger DC Level Adjustment	5-10
5-14	Channel 2 Output Level Adjustment	5-11
5-15	High Frequency Adjustments	5-11
5-16	Input Capacitance Standardization and Attenuator Adjustment	5-17

6. ELECTRICAL PARTS LIST AND SCHEMATICS
LIST OF RECOMMENDED VENDORS

TABLE

<u>Number</u>	<u>Title</u>	<u>Page</u>
5-1	Attenuator Compensation Trimmers	5-21

ILLUSTRATIONS

<u>Figure</u>	<u>Title</u>	<u>Page</u>
1-1	Type 79-02A Dual Trace 100 Mc Amplifier	1-0
2-1	Function of Type 79-02A Dual Channel Controls	2-3
2-2	Function of Type 79-02A Input Channel Switching Facilities	2-5
2-3	Type 79-02A Calibrator Display	2-6
2-4 to 2-8	Waveform Displays	2-9 to 2-13
2-9 to 2-11	Waveform Displays	2-18 & 2-19
2-12	Peak-to-Peak Voltage Measurements	2-24
2-13	Instantaneous Voltage Measurement with Respect to a Reference Potential	2-26

TABLE OF CONTENTS
(Concluded)

ILLUSTRATIONS
(concluded)

<u>Figure</u>	<u>Title</u>	<u>Page</u>
3-1	Type 79-02A Input Circuit, Simplified Functional Block Diagram	3-2
3-2	Type 79-02A Channels 1 & 2 Pre-Amplifiers, Functional Block Diagram	3-3
3-3	Type 79-02A X10 Amplifiers, Functional Block Diagram	3-4
3-4	Type 79-02A Electronic Switching Circuit, Functional Block Diagram	3-5
3-5	Type 79-02A Y Deflection Amplifier, Functional Block Diagram	3-6
3-6	Type 79-02A Trigger Amplifiers, Functional Block Diagram	3-7
5-1	Type 79-02A Over-All System Block Diagram	5-2
5-2	Test Setup For Adjusting High Frequency Trimmers	5-12
5-3	Appearance of Waveform when Making High Frequency Adjustments	5-14
5-4	Left Side View Showing HF Trimmers	5-16
5-5	Test Setup for Adjusting Input Capacitance and Volts/Div Trimmers	5-18
5-6	Standardizing the Input Capacitance	5-19
5-7	Left Side View Showing Channel 1 and Channel 2 Attenuator Adjustments	5-20
5-8	Right Side View Showing Nuvisitors & Transistors	5-22
5-9	Left Side View Showing Transistors	5-23
5-10	Left Side View Showing Trimmers and Pot Adjustments	5-24
5-11	Top View Showing Delay Line Trimmer and Pot Adjustments	5-25
6-1	Front Panel Replaceable Parts	6-0

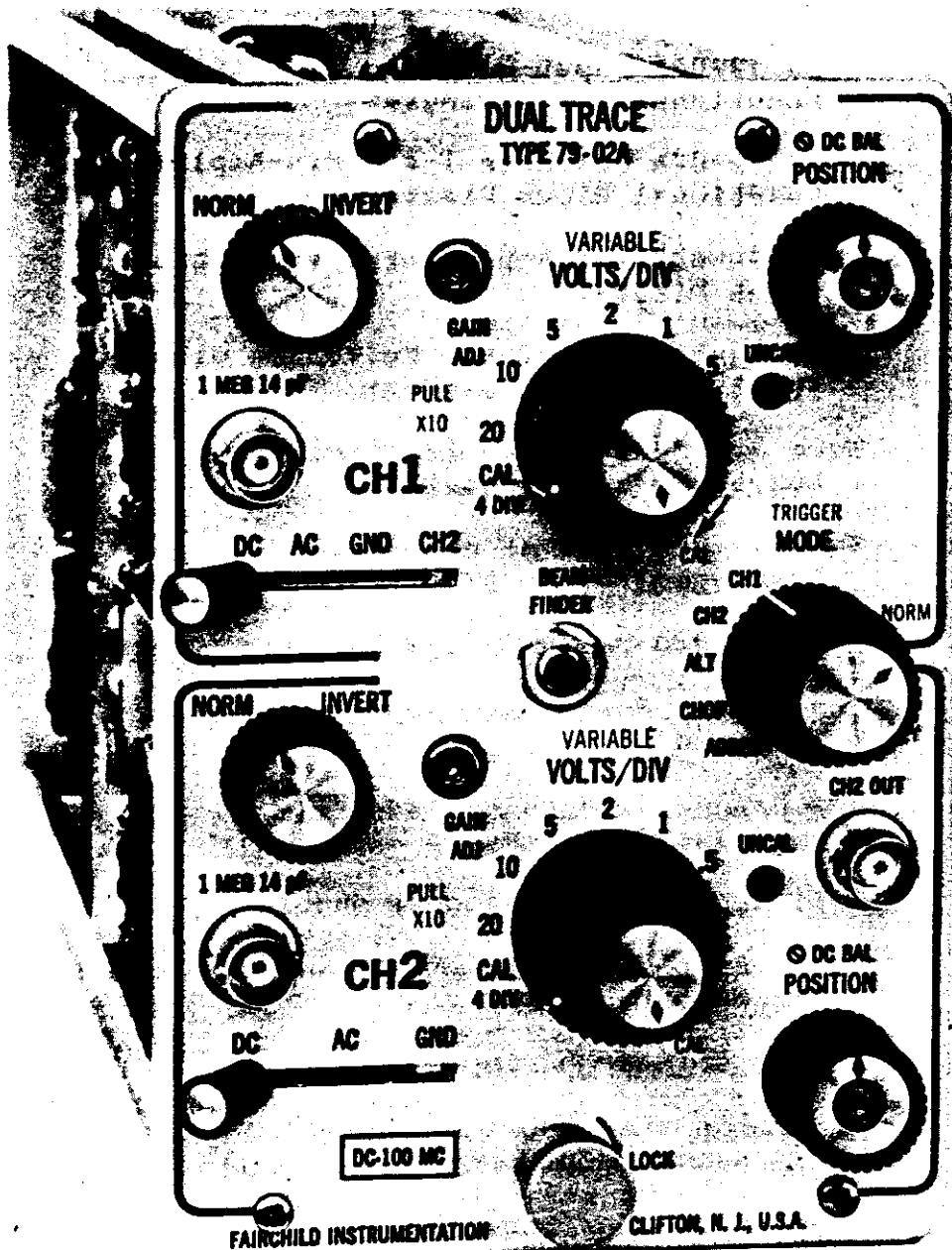


FIGURE 1-1. TYPE 79-02A DUAL TRACE 100 MC AMPLIFIER PLUG-IN

SECTION 1

TECHNICAL SUMMARY

1-1. INTRODUCTION

The Type 79-02A Amplifier is a dual-channel amplifier and is provided with two basic amplifier sensitivities and bandwidths for X1 and X10 calibrated operation as follows:

100 millivolts/division sensitivity with a dc to 100 megacycle bandwidth.

10 millivolts/division sensitivity with a dc to 90 megacycle bandwidth.

Operation of this plug-in unit enables the user to obtain two vertical signals on the screen simultaneously or to display either channel individually.

The VARIABLE gain control, located concentrically with the VOLTS/DIV switch, has a range of greater than 2-1/2 to 1. This VARIABLE gain control provides continuous overlap between steps of the attenuator (VOLTS/DIV) switch. A detented stop position is provided when the VARIABLE gain control is set to CAL.

A MODE switch is provided which enables the selection of either Channel 1 or Channel 2 for separate display or the combination of both channels for dual display. In addition, ALTERNATE or CHOPPED modes of operation are available. Use of the Polarity Inversion switch may give Channel 1 minus Channel 2 or Channel 2 minus Channel 1 presentation when MODE switch is set to ADDED.

The Type 79-02A Amplifier is intended for use in the Y cavity of the Type 766H/F Series Oscilloscopes.

1-2. FEATURES

- 100 Mc bandwidth at 100 mv/div sensitivity
- 10 mv/div sensitivity with 90 Mc bandwidth
- Solid state circuitry
- Cascading feature converts instrument from dual trace to a high-gain, single trace unit; 1 mv/div sensitivity with 30 Mc bandwidth nominal.

FEATURES (concluded)

- Front-panel GAIN ADJ control is provided for each channel to normalize gain between channels
- Polarity Inversion switch enables subtraction of two signals when operating in the Added mode
- Ground position on Input Selector switch provides ground reference on base line without necessity of grounding input of instrument
- Provides equivalent dual-beam scope operation when used with Fairchild Type 74-17A Automatic Display Time Base Plug-in unit

1-3. TECHNICAL SUMMARY (Specifications)

The electrical characteristics of the Type 79-02A Amplifier are listed in the Performance Specification which follows.

SPECIFICATIONS

Y AMPLIFIER

Bandwidth

Direct Coupled:

X1: DC to approximately
100 megacycles.

X10: DC to approximately
90 megacycles.

Capacitively Coupled:

X1 or X10: Low-frequency
cutoff is 16
cycles.

Rise Time:

X1: 3.8 nanoseconds or less.

X10: 4.2 nanoseconds or less.

NOTE: Rise time of Test Generator
should be 0.4 nsec or better.

Sensitivity

Cal X1: 100 millivolts/div.
to 20 volts/division
in 8 steps of 1, 2, and
5 sequence when VARIABLE
gain control is set to
CAL; accurate to within
+3% when set on any one
step.

Cal X10: 10 millivolts/division
to 2 volts/division in
12 and 5 sequence.

Uncal,
X1 or
X10: Continuously variable
from 10 millivolts/div.
to 50 volts/div. The
VARIABLE gain control
permits 2-1/2 to 1
continuous sensitivity
adjustments between the
attenuator steps and
extends the 20 volts/div.
range to 50 volts/div.

Output Range

Six divisions of vertical output
scan (D3 and D4 CRT plates) is
available. Overshoot and preswing
are each 3% at 4-division scan.

Input Impedance

1 megohm shunted by 14 pf.

Input Selector Switch

Channel 1 is provided with a
4-position lever switch which
permits selection of a-c or d-c
coupling, Channel 2 output or
ground. Channel 2 is provided
with a 3-position lever switch
providing selection of a-c or d-c
coupling and ground. The GND
position provides base line
reference and disconnects input
signal.

Polarity Inversion

Separate two-position rotary
switch for each channel provides
selection of either NORMAL or
INVERTed input signal.

Calibration

Calibrator signal (line frequency
square wave) is applied directly
to the input of the Y Amplifier
to standardize gain when VOLTS/
DIV switch is set to CAL.
(Cal: 4 divisions; valid only
in the X1 position.)

SPECIFICATIONS (Concluded)

Y AMPLIFIER

Signal Delay

A 185-nanosecond balanced distributed bifilar helical delay line is provided. This delay is sufficient to view baseline and the leading edge of a fast rise-time signal for internal triggering of the time base.

Internal Trigger

A two-position switch provides a trigger pick-off after switch stage (Ch 1 and Ch 2) or a trigger pick-off from Channel 2 only.

The internal trigger output signal is referenced to ground when the trace is positioned to screen center via factory adjustment of the Trig DC LEVEL control.

High Sensitivity Amplifier

An internal connection from Channel 2 output connector to Channel 1 input connector can provide a series connection of the Channel 1 and Channel 2 amplifiers. It should be noted that only when the channels are set up for X10 operation is the cascading feature useful.

Available sensitivity is 1 mv/div and bandwidth is dc to 25 Mc in this mode. 30 Mc nominal.

Operational Modes

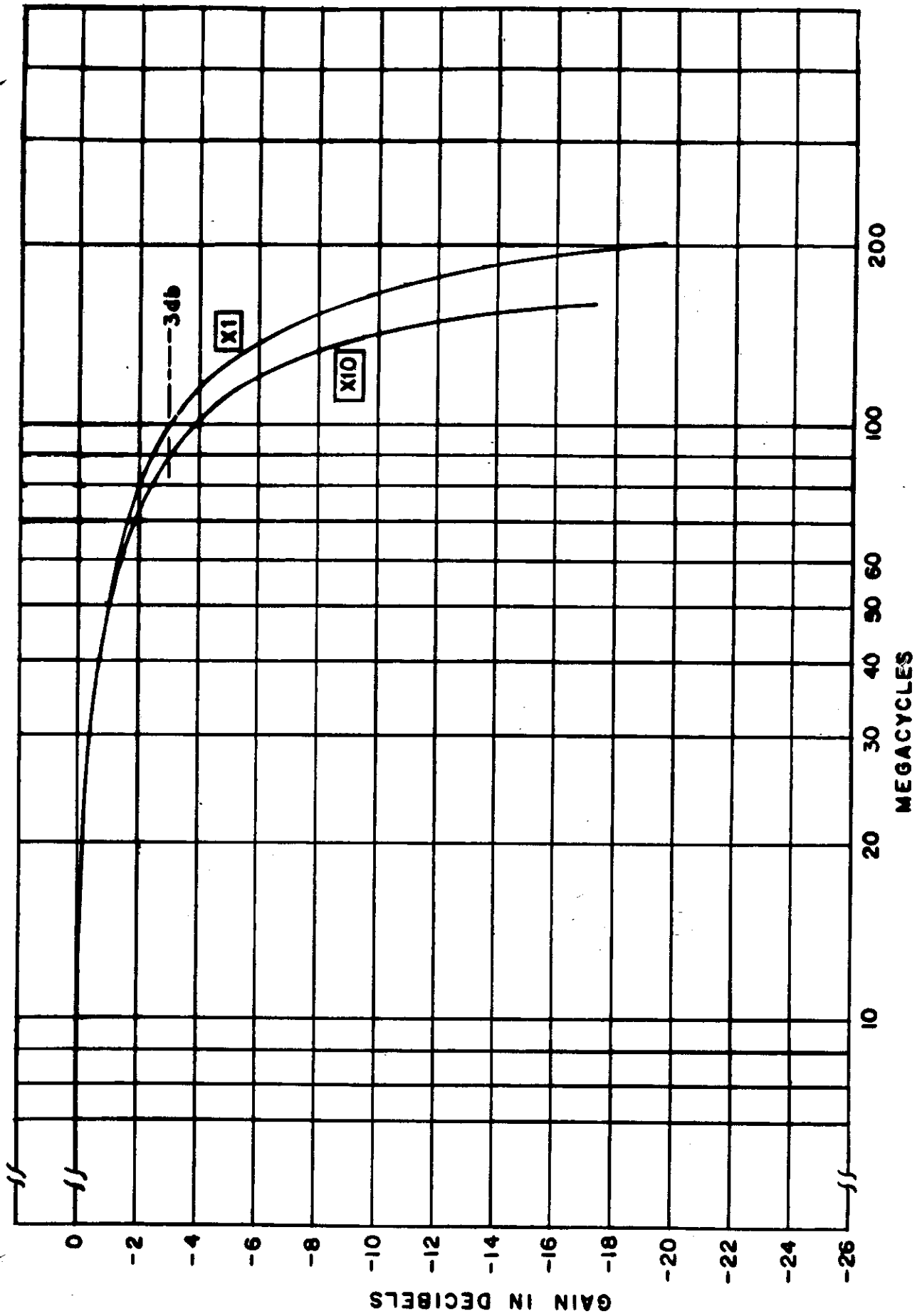
The following displays are available:

1. Ch 1 only
2. Ch 2 only
3. Ch 1 & Ch 2 switched alternately
4. Ch 1 & Ch 2 time shared (chopped)
5. Ch 1 & Ch 2 (Invert switch permits Ch 1 - Ch 2 or Ch 2 - Ch 1 presentation)
6. Cascaded operation.

In chopped operation, two chopping rates, 100 Kc and 1 Mc, are available and selected by an internal switch. Switching transients are automatically blanked.

Beam Finder

A spring-loaded push-button switch is provided to facilitate location of beam when it is positioned off screen.



TYPE 79-02A NOMINAL FREQUENCY RESPONSE CURVE

SECTION 2

OPERATING INSTRUCTIONS

2-1. FIRST TIME OPERATION (Figures 2-1 to 2-3)

The Type 79-02A Dual Trace Amplifier Plug-in is inserted in the Y cavity (left-hand side) and assume that the Type 74-03A Time Base Plug-in (other Fairchild X Plug-ins may be used) is inserted in the X cavity (right-hand side) of the H/F Series Main Frame Oscilloscopes. The H/F Series Oscilloscopes is provided with the Type 7062 CRT Termination Network to accommodate the Type 79-02A. In the instructions which follow, capital letters within the text indicate front-panel controls, connectors or settings.

Note: For proper performance, make certain the Type 79-02A is installed only in the Y cavity of the H/F Series Main Frame Oscilloscope.

The following illustrations are designed to aid the operator in becoming familiar with the oscilloscope:

- Figure 2-1. Function of Type 79-02A Dual Channel controls
- Figure 2-2. Function of Type 79-02A Input Channel Switching Facilities
- Figure 2-3. Type 79-02A Calibrator Display

The remaining paragraphs of this section are provided as a guide to extend the operator's skill in using the instrument.

2-2. APPLYING A SIGNAL

The signal (or signals) to be displayed is applied to either (or both) input connector on the front panel. To insure proper performance, the signal should be applied through a shielded cable, with the shield connected to the chassis of both the oscilloscope and the signal source.

The Fairchild Types 7994B and 7999B Accessory Probes are available for use with the Type 79-02A Amplifier.

2-3. DC BALANCE ADJUSTMENT

If the DC balance of the Type 79-02A Amplifier is not properly adjusted, the reference trace on the screen will be depositions when the VARIABLE control is rotated. To properly adjust the DC BAL front-panel screwdriver control for Channel 1, proceed as follows:

1. Set the MODE switch to CH 1 and the Input Selector switch to GND.
2. Set the VOLTS/DIV switch to 0.1 position and rotate the VARIABLE control to its minimum gain setting.
3. Adjust the Time Base Plug-in controls for automatic sweep to obtain a reference trace on the screen.

4. Adjust the POSITION control on each plug-in, to place the trace at center of screen (reference line).
5. Rotate the VARIABLE control right and left throughout its range observing the direction that the trace shifts vertically.
6. Adjust the front-panel DC BAL screwdriver control to bring the trace back to center of screen.

Note: Do not change the POSITION control settings.

7. Continue adjusting the DC BAL control while rotating the VARIABLE control back and forth, until there is minimum displacement of the trace when the VARIABLE control is rotated throughout its range.
8. Repeat preceding steps for Channel 2 using pertinent controls.

Note: If the adjustment range of the front-panel DC BAL control is insufficient, refer to Section 5, Maintenance and Recalibration, for the complete Coarse and Fine Balance adjustment procedure.

2-4. SETTING GAIN OF DUAL-TRACE AMPLIFIER

Whenever the Type 79-02A Amplifier is removed from the Main Frame and inserted in another, the front-panel screwdriver GAIN ADJ control must be reset. This procedure is necessary to compensate for difference in deflection plate sensitivities.

To properly normalize the gain between channels or between the Plug-in unit and the Main Frame, proceed as follows:

1. Set both Channel 1 and Channel 2 VOLTS/DIV switches to CAL and turn both VARIABLE controls to CAL (fully cw).
2. Push in both VARIABLE controls (X1 position).
3. Set MODE switch to CH 1 and TRIGGER switch to NORM.
4. Adjust the Sweep controls for auto sweep and line triggering.
5. Set MODE switch to ALT and adjust sweep rate for 2 milliseconds/division.
6. Adjust Channel 1 GAIN ADJ front-panel screwdriver control for 4 divisions of vertical deflection.
7. Position the traces one on top of the other.
8. Adjust Channel 2 GAIN ADJ control until only one trace may be observed (traces are superimposed).

VOLTS/DIV

One of two identical attenuators:

Calibrated X1 operation: from 100 mv/div to 20 volts/div

Calibrated X10 operations: from 10 mv/div to 2 volts/div. (In this mode, simply divide the knob setting by 10.)

NORM/INVERT

One of two identical switches: selects polarity of incoming signal. In NORM position, retains polarity of incoming signal; in INVERT position, reverses polarity of displayed waveform

POSITION

One of two identical controls: used to position the trace vertically

VARIABLE

One of two identical controls: provides a 1:2-1/2 variable adjustment permitting minimum sensitivity and overlap of the VOLTS/DIV setting. A detented stop position is provided in CAL setting. Increases amplifier gain by X10 when VARIABLE control is pulled out

GAIN ADJ

One of two identical screwdriver controls: normalizes inter-channel gain and the gain between Plug-in and Main Frame

INPUT

One of two identical BNC connectors: used to applying external signals to the associate channel amplifier via the MODE switch

DC BAL

One of two identical screwdriver controls: when properly adjusted minimizes deposition of the pattern when VARIABLE control is used



FIGURE 2-1. FUNCTION OF TYPE 79-02A DUAL CHANNEL CONTROLS

2-5. INPUT SELECTOR SWITCH

Each channel is provided with an Input Selector switch which provides the following common functions:

- AC or DC coupling of input signal
- Ground reference positions

Channel 1 Input Selector switch is provided with an additional position labeled CH 2. In this position, an internal connection from the output of Channel 2 amplifier is automatically connected in series with the input of Channel 1 amplifier. This technique converts the plug-in from its normal 100 Mc dual trace function to a high gain single trace amplifier with a 50 Mc bandwidth and a sensitivity of 1 millivolt/division.

The Input Selector switch permits choice of retaining the DC level of the input signal or blocking the dc component of the input signal by inserting a capacitor in series with the input. If it is desired to display both the ac and dc components of a signal, set this switch to DC. Thus, the position of the display at any instant is a function of the instantaneous signal voltage with respect to ground.

There are times when it is neither necessary nor desirable to display the dc component of the input waveform. A capacitor placed in series with the input connector will exclude the dc component while simultaneously permitting the ac component to be displayed. This is accomplished when the Input Selector switch is set to AC. The effect of the dc component is now excluded from the display.

It should be noted that when the Input Selector switch is set to the AC position, the lowest frequency limit (3 db) of the Amplifier is about 16 cycles. Therefore, some low-frequency distortion and loss of amplitude will occur if the pattern on display contains frequency components below the specified cut-offs. Use of a 10:1 Attenuator Probe brings the low frequency response to 1.6 cycles.

When using the dual-trace features of the Type 79-02A, you may desire to invert the displayed waveform. In the NORM position of the Polarity Inversion switch, the displayed waveform will have the same polarity as the applied signal. When the switch is set to INVERT, the displayed waveform will be inverted. In other words, a positive-going pulse will be displayed as a negative-going pulse.

INPUT SELECTOR

A four-position slide switch: enables selection of AC or DC coupling. Grounds amplifier input in GND position. In CH 2 position, connects Channel 2 output to input of Channel 1.

INPUT SELECTOR

A three-position slide switch: enables selection of AC or DC coupling. Grounds amplifier input in GND position.



TRIGGER

Switch: provides a choice of two internal trigger sources. Either Channel 2 signal or the composite signal driving the vertical deflection plates may be selected.

MODE

Switch: used to select the channels in the following manner:

1. CH 1 ONLY
2. CH 2 ONLY
3. CH 1 & CH 2 switched alternately
4. CH 1 & CH 2 time-shared (Chopped)
5. Added: algebraic sum of Channels 1 and 2

CH 2 OUT

BNC connector: used to make available CH 2 pre-amplifier output through a 5K-ohm isolating resistor.

FIGURE 2-2. FUNCTION OF TYPE 79-02A INPUT CHANNEL SWITCHING FACILITIES

To obtain the calibrator display, set the controls exactly as shown and perform the numbered steps in sequence.

Use the same procedure when difficulty is experienced in obtaining a display. This will eliminate "cockpit" troubles due to misalignment of controls.

Readjust INTENSITY, FOCUS and ASTIG controls for a sharp pattern. Readjust ⑥ to center the display

Set ASTIG, FOCUS and INTENSITY controls to center of range

Set POSITION controls to center of range

① Rotate clockwise to turn on the oscilloscope

Set to NORM ⑦

② Set outer knob (TIME/DIV) to 5 mSEC

Set to DC ⑧

③ Rotate inner knob (VARIABLE) clockwise to CAL until switch is actuated (click is heard). Note that UNCAL lamp is off

Set outer knob (VOLTS/DIV) to CAL ⑨

④ Set TRIGGERING switches to +, DC, LINE

Push in and rotate inner knob (VARIABLE) fully clockwise ⑩

Set inner knob (TRIGGER) to NORM ⑪

⑫ Set outer knob (MODE) to CH 1

⑤ Set outer knob (Sweep Mode Selector) to AUTO SWP

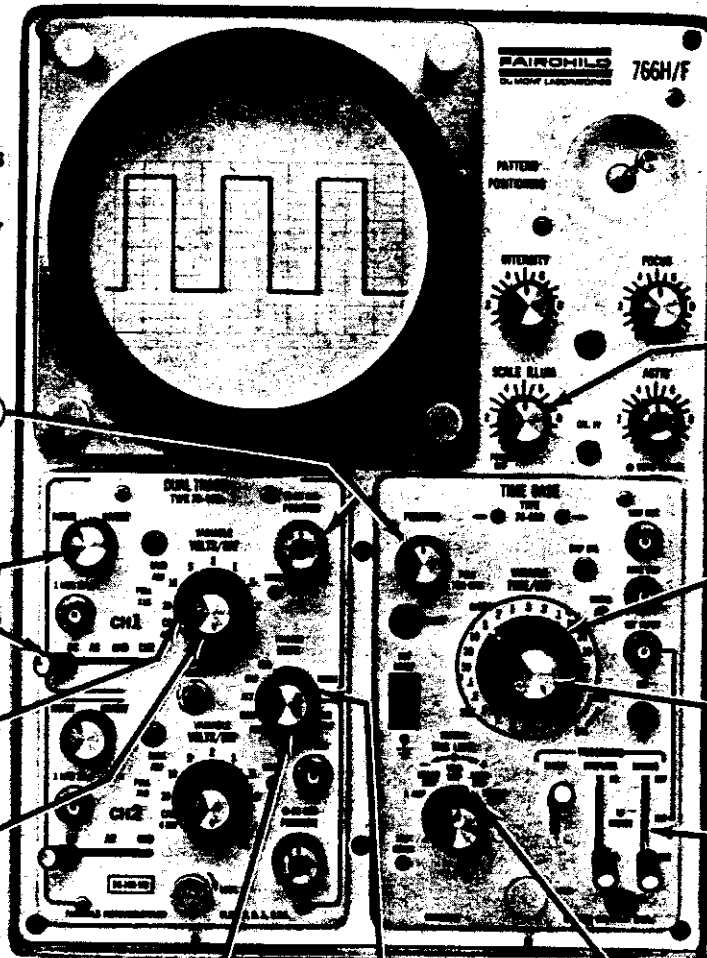


FIGURE 2-3. TYPE 79-02A CALIBRATOR DISPLAY

INPUT SELECTOR

A four-position slide switch: enables selection of AC or DC coupling. Grounds amplifier input in GND position. In CH 2 position, connects Channel 2 output to input of Channel 1



TRIGGER

Switch: provides a choice of two internal trigger sources. Either Channel 2 signal or the composite signal driving the vertical deflection plates may be selected

MODE

Switch: used to select the channels in the following manner:

1. CH 1 ONLY
2. CH 2 ONLY
3. CH 1 & CH 2 switched alternately
4. CH 1 & CH 2 time-shared (Chopped)
5. Added: algebraic sum of Channels 1 and 2

INPUT SELECTOR

A three-position slide switch: enables selection of AC or DC coupling. Grounds amplifier input in GND position

CH 2 OUT

BNC connector: used to make available CH 2 pre-amplifier output through a 5K-ohm isolating resistor

FIGURE 2-2. FUNCTION OF TYPE 79-02A INPUT CHANNEL SWITCHING FACILITIES

To obtain the calibrator display, set the controls exactly as shown and perform the numbered steps in sequence.

Use the same procedure when difficulty is experienced in obtaining a display. This will eliminate "cockpit" troubles due to misalignment of controls.

Readjust INTENSITY, FOCUS and ASTIG controls for a sharp pattern. Readjust ⑥ to center the display

Set ASTIG, FOCUS and INTENSITY controls to center of range

Set POSITION controls to center of range ⑥

Rotate clockwise to turn on the oscilloscope ①

Set to NORM ⑦

Set outer knob (TIME/DIV) to 5 mSEC ②

Set to DC ⑧

Rotate inner knob (VARIABLE) clockwise to CAL until switch is actuated (click is heard). Note that UNCAL lamp is off ③

Set outer knob (VOLTS/DIV) to CAL ⑨

Push in and rotate inner knob (VARIABLE) (TRIGGER) fully clockwise ⑩

Set TRIGGERING switches to +, DC, LINE ④

Set inner knob (TRIGGER) to NORM ⑪

Set outer knob (MODE) to CH 1 ⑫

Set outer knob (Sweep Mode Selector) to AUTO SWP ⑤

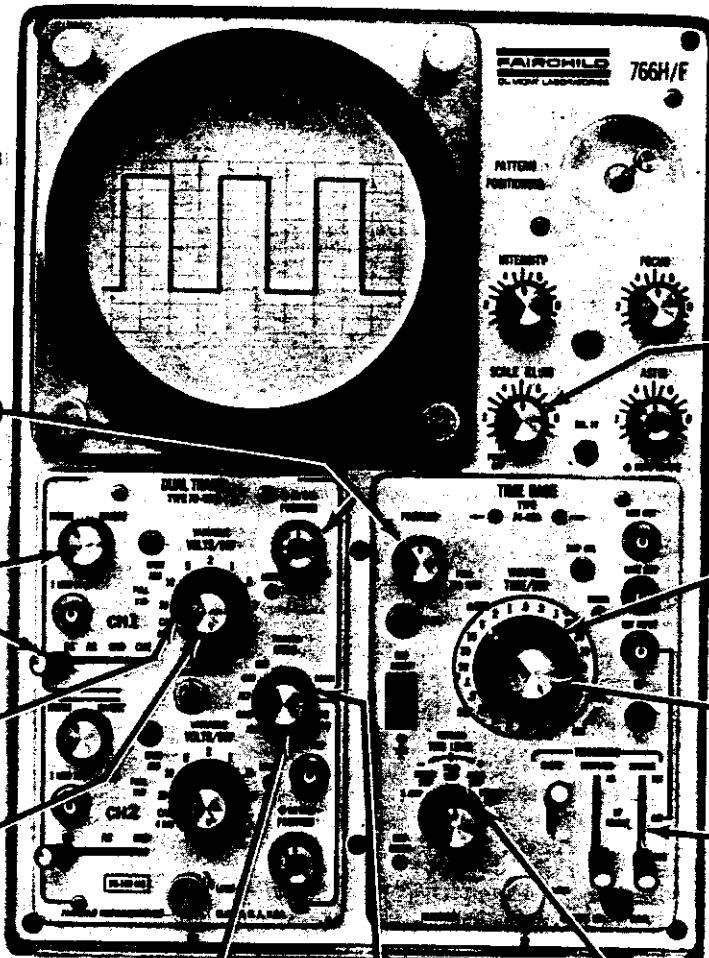


FIGURE 2-3. TYPE 79-02A CALIBRATOR DISPLAY

2-6. OBTAINING A DISPLAY

To use the Type 79-02A Amplifier to obtain a display, proceed as follows:

1. Signals to be observed are connected to the Type 79-02A Amplifier through the Channel 1 and/or Channel 2 BNC connector via shielded cable or an Attenuator Probe.
2. Establish a common ground between the oscilloscope chassis and the signal source.
3. To display a single trace with the Type 79-02A Amplifier, simply apply the signal to either Input connector and set the MODE switch to the corresponding channel.
4. To display two signals simultaneously, connect a signal to each Input connector and set the MODE switch to ALT or CHOP. The chopped position is used when it is desired to reduce the "flickering" of the display when observing input signal data at slow sweep speeds (below 1 millisecond/div). External triggering of the Time Base or CH 2 ONLY triggering is to be preferred in chopped position to prevent the sweep from triggering on the "chopping" signal. In general, the CHOP position is used with lower sweep rates and the ALT position with higher sweep rates.

Two chopping rates, 100 Kc and 1 Mc, are available, selected by an internal slide switch. Switching transients are automatically blanked.

5. To display the algebraic sum of two signals, connect a signal to each Input connector and set the MODE switch to ADDED (Ch + Ch 2).
6. To display the algebraic difference of two signals, apply a signal to each Input connector and set the MODE switch to ADDED. For Ch 1 minus Ch 2 presentation, set Channel 1 Polarity Inversion switch to NORM and Channel 2, Polarity Inversion switch to INVERT. For Ch 2 minus Ch 1 presentation, set Channel 1 Polarity Inversion switch to INVERT, Channel 2 Polarity Inversion switch to NORM.
8. Adjust the appropriate Time Base Plug-in controls to obtain a stable display of the pattern.
9. Set the VOLTS/DIV switch and POSITION control to obtain the desired size display positioned on screen.

NOTE: Whenever the Type 79-02A Amplifier is removed from the Main Frame and inserted in anchor, certain high-frequency adjustments must be taken to take advantage of the full possible bandwidth of the Type 79-02A Amplifier.

To make adjustments, proceed as follows:

1. Connect the Type 79-02A Amplifier into the test equipment system described in Figure 5-2 on page 5-12 of the Instruction Manual.
2. Follow the instructions outlined in paragraph 5-15 a,b, and c as described on pages 5-11 through 5-15 inclusive.

2-7. CABLING TECHNIQUES IN THE NANOSECOND REALM

a. INTRODUCTION

The purpose of this brief discussion is to point out the problems which may be encountered when one is trying to couple a signal from a source to a 100-megacycle oscilloscope over a transmission line.

If signal fidelity is to be maintained, cabling techniques and use of Passive Attenuator Probes which were satisfactory for microsecond rise-time measuring instruments, may, prove to be inadequate for application in the nanosecond realm. Since the oscilloscope is generally used as a remote monitoring device, it is necessary to transmit the signal that is to be observed some distance from the source to the load... the load being the vertical input of the oscilloscope. The two most common types of transmission lines employed in high-frequency real-time oscilloscopes are (1) the coaxial cable and (2) the high impedance passive probe.

The transmission line must be designed and connected so as to prevent ringing, reflections, and standing waves which would cause pulse deterioration. By insuring that the oscilloscope system is properly connected to the source, the operator is not only guaranteed optimum results, but time is conserved by obtaining the proper waveform the first time.

In the discussion to follow, the end of the transmission line to which power is applied is called the receiving or generator end; and the end at which power is received is called the receiving or load end.

b. EFFECT OF IMPROPER TERMINATION (Figure 2-4)

Let us first consider the 50-ohm coaxial cable as a transmission link between some 50-ohm signal source and an oscilloscope. Assume that we have a 50-ohm generator which develops a .4-nanosecond rise time pulse and that it is desired to view this pulse on the oscilloscope using the Fairchild Type 79-02A 100 Mc Dual Trace Amplifier Plug-In. We must then transmit this pulse from the generator to the oscilloscope without degrading the signal. Under these conditions, no mismatch exists at the source; however, at the load end of the coaxial which is connected directly to the oscilloscope input, the line sees one megohm shunted by 14 pf of capacity. Due to the mismatch at the oscilloscope, a reflected voltage is transmitted from the mismatch back to the generator where the energy will be dissipated in the 50-ohm load. See Figure 2-4.

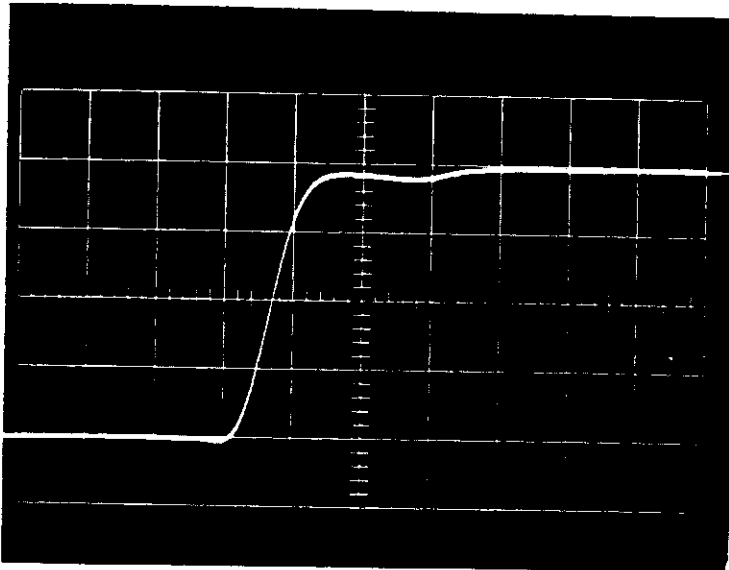


Figure 2-4.

.4-nanosecond rise time pulse from a 50-ohm source thru a 42-inch 50-ohm unterminated coax to the Type 79-02A Dual Trace 100 Mc Amplifier

c. EFFECT OF SOURCE AND LOAD TERMINATION (Figure 2-5)

Let us examine more closely the effects of mismatch on improper termination. When a mismatch occurs within the system, there will be a reflected voltage. This reflected voltage is a product of the input signal voltage and the coefficient of reflection which can be designated as the parameter (ρ). If the load impedance is much greater than the cable impedance, then $\rho \rightarrow 1$. If the load impedance approaches infinity, then the signal as viewed will be twice the output of the generator, and conversely if the load impedance is equal to zero, a short circuit exists and the signal output will be zero. When the transmission line at the load end sees a mismatch which is not a perfect open circuit, reflections occur causing signal deterioration. In order to obtain optimum response and pulse fidelity, it is necessary to terminate the load end of the line in its characteristic impedance. See Figure 2-5. The line is now terminated at both ends.

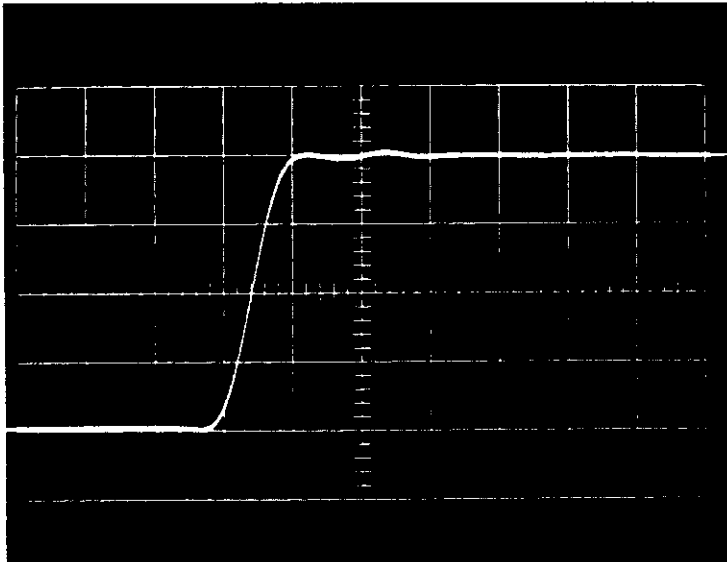


Figure 2-5.

.4-nanosecond rise time pulse from a 50-ohm source thru a 42-inch 50-ohm terminated coax to the Type 79-02A Dual Trace 100 Mc Amplifier

It can be seen that the reflection which was apparent in Figure 2-4 has been removed and the rise time has improved.

By terminating the load end of the transmission line, the reflection due to mismatch at the load end has been minimized and at the same time the bandwidth of the system has been improved.

d. EFFECT OF CABLE LENGTH ON PULSE RESPONSE (Figures 2-6 to 2-8)

Whenever the length of the unterminated cable is increased, the bandwidth of the system is reduced due to the increased cable capacity which the generator must drive. When both the sending and receiving ends of the transmission line are terminated in the characteristic impedance, the generator sees a resistive load, and therefore is no longer required to drive the line capacity. The reduction in signal amplitude is not paramount if the primary objective is the improvement to system response and pulse fidelity. See Figure 2-6.

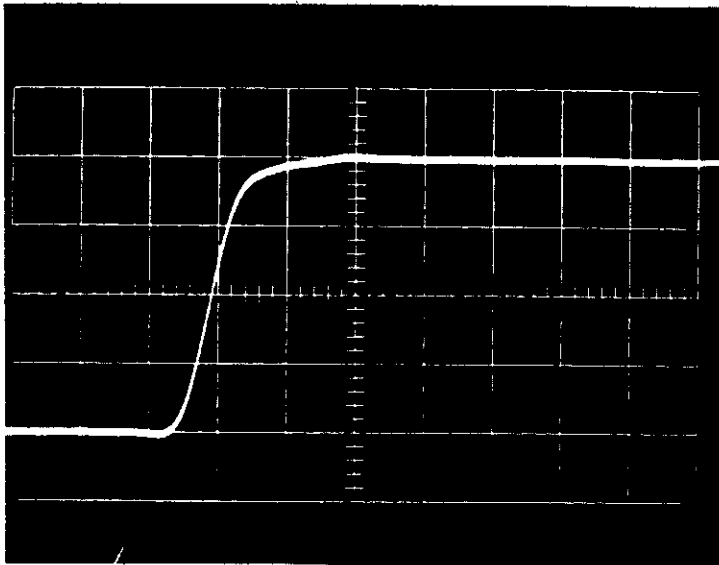


Figure 2-6.

.4-nanosecond rise time pulse from a 50-ohm source thru a 6-inch 50-ohm unterminated coax to the Type 79-02A dual trace 100 Mc Amplifier.

This shows an improvement over Figure 2-4 where a 42" unterminated cable was used. However the response and pulse fidelity is not of the quality shown in Figure 2-5 where a properly terminated line was used.

In the previous example, Figure 2-6, it was assumed that the generator end of the coax was properly terminated in the characteristic impedance of the line and the load end (scope input) was unterminated.

The pulse response will be adversely affected when both ends of the coaxial cable are not properly terminated. Reflections will occur due to the mismatching and the duration of the reflection will be determined by the length of cable between the points of mismatch.

In illustrative examples, Figures 2-7 and 2-8, a three-nanosecond pulse was coupled from a 50-ohm source into different lengths of unterminated 75-ohm coaxial cable to the Type 79-02A Amplifier. The positive overshoot is due to the mismatch at the load end (scope input) and the negative reflection is caused by the mismatch at the source or generator end. The duration of the reflection is longer in Figure 2-7 than in Figure 2-8 due to the longer length of cable used. The application of minimum loss matching pads in Figures 2-7 and 2-8 would have improved pulse fidelity, but at the expense of signal amplitude.

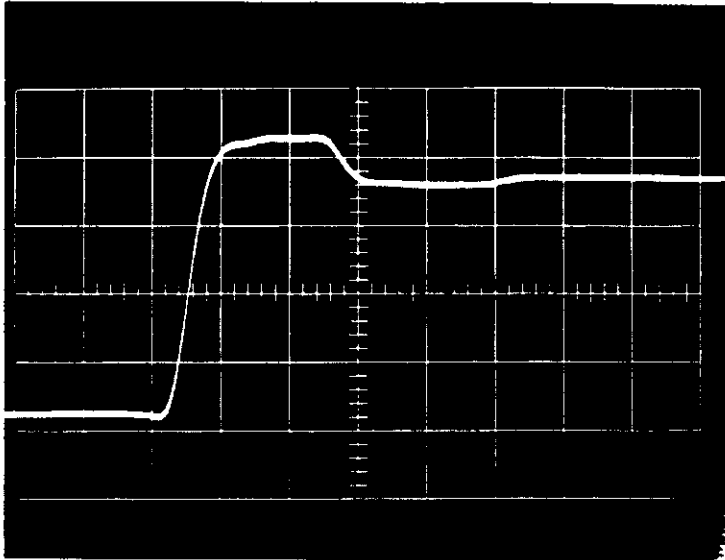
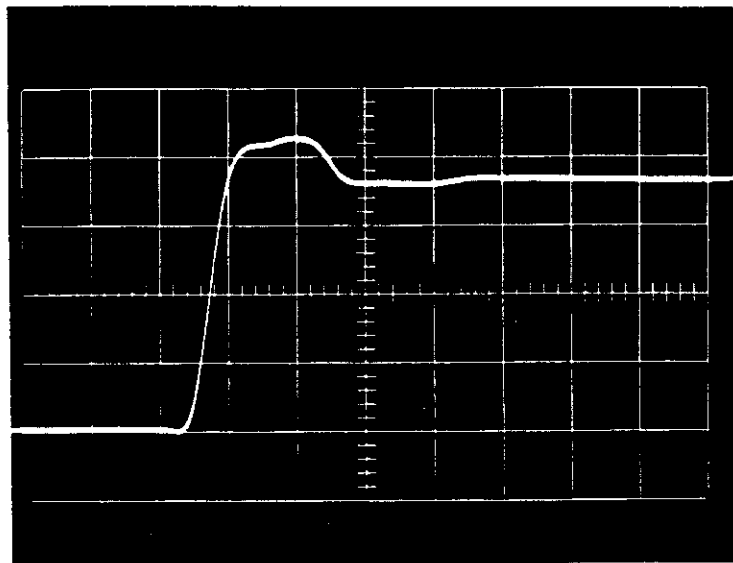


Figure 2-7.

.4-nanosecond pulse
from a 50-ohm source
into a 72-inch length
of 75-ohm cable to
the Type 79-02A
Dual Trace 100 Mc
Amplifier

Figure 2-8.

.4-nanosecond pulse
from a 50-ohm source
into a 42-inch length
of 75-ohm cable to
the Type 79-02A
Dual Trace 100 Mc
Amplifier



The use of coaxial cable will find its widest application in systems work where low impedance outputs are used. Quality coaxial cables are available in the range from 50 to 150 ohms.

In the case of circuits where impedances in the order of kilohms are found, standard coaxial cables are unsuitable for a transmission line because of their low impedance and capacitive loading effects. For these applications, a high impedance passive probe is recommended. Passive attenuator probes will generally reduce bandwidth and slow the display system rise time. Consider the effect of probe loading and response in your measurements. See paragraph entitled "Use of Probes."

e. SUMMARY OF CABLING TECHNIQUES

The ideas developed in the preceding paragraphs may be recapitulated as follows.

1. In broadband applications, it is necessary to terminate a coaxial cable with a resistance equal to its characteristic impedance. This is done to prevent standing waves or ringing (high-frequency damped oscillations).
2. To avoid erroneous results, the operator should simulate the actual operating conditions of the equipment being tested. For example, the equipment should work into a load impedance equal to that which it will see in actual use.
3. Consider the effect of loading upon the signal source due to the input impedance of the oscilloscope. The input impedance can be represented by a resistance shunted by a capacitance. The effective value of this impedance is indicated in the Specifications. However, the operator should be aware that even with a few feet of cable in the input circuit, the loading capacitance on the circuit under investigation might be greater than 100 pf.
4. There are cases when connecting the input of the oscilloscope to a signal source, the effect of loading the source is not negligible. To minimize this loading and therefore obtain a valid measurement, a probe may be used in the manner described in the paragraph entitled "Use of Probes."

5. Care must be exercised when applying a fast rise, high-frequency signal to the Input connector. It will be necessary to match and properly terminate the coaxial cable applying the signal to the oscilloscope or ringing on the rising and falling portion of the waveform will result.

f. CABLING FOR RACK-MOUNTING SYSTEMS

For rack-mounting systems, observe the following precautions if long, shielded cables are used.

1. It may be desirable to ground long shielded leads only at one end to avoid circulation currents. Even microamperes of extraneous currents in the shielded braid can cause unwanted distortions.
2. Use cable with insulation over the shielded braid so that the cable does not accidentally touch ground.
3. Use off-ground insulated bulkhead feed-thru connectors where applicable.
4. Do not pass cables near strong AC magnetic fields.
5. Long shielded input cables may also induce parasitic oscillations. It is suggested that a 100-ohm to 1000-ohm, 1/2 watt resistor be connected in series with the center conductor near or at the oscilloscope input terminals.
6. Use a resistance at least twice that required to just stop the parasitic oscillations. Too large a value may reduce the bandwidth of the system.

2-8. USE OF PROBES

a. INTRODUCTION

An attenuator probe reduces both the capacitive and resistive loading caused by the oscilloscope.

Simultaneously, while isolating the oscilloscope from the signal source, it reduces the effective sensitivity of the instrument. In other words, the displayed waveform will be reduced in amplitude by the attenuation factor of the probe.

When using the probe to sample signals from a tuned, matched, or otherwise critical circuit, capacitive loads may cause erroneous readings. In these cases it may be necessary to remove capacity and resistance from the circuit under observation. When the observations and adjustments are completed, capacitance and resistance precisely equal to that of the probe impedance, should be added to the circuit after the probe is removed from the circuit. This substitution will equalize loading and restore the operating characteristics of the circuit under observation to the same conditions as when probe measurements were made.

When using the attenuator probe to make amplitude measurements, multiply the observed amplitude of the display by the attenuation factor marked on the probe.

b. TYPE 7994B PROBE

As is the case where any probe is used with an oscilloscope, the over-all system bandwidth and response is reduced and there will be a certain degree of loading. The amount of loading introduced by the probe will be determined by the characteristics of the circuit under test and the input resistance and capacitance of the probe.

The Fairchild Type 7994B Probe is basically an unterminated high-frequency probe which has been designed to work with the Type 79-02A 100 Mc Amplifier Plug-in as a system. At low frequencies, the probe together with the input of the oscilloscope appears as a compensated divider. However, when using the probe to monitor nanosecond pulses, the reactive components and line losses become important factors.

Since the probe is used unterminated, the design must be such that no reflections or ringing will occur to cause

signal deterioration. The lead inductance of the center conductor at high frequencies becomes a critical factor in the probe design. Since the cable is unterminated and has inductance and capacitance, it is necessary that a resistance wire be used as a center conductor. This resistance is carefully selected so that the cable is critically damped. In the Fairchild Type 7994B Probe, there is a termination network located at the scope end of the probe. This network consists of reactive and resistive components and is used to adjust the response at high frequencies.

There is a limitation as to the length of cable that can be used in the probe without severely restricting the bandwidth of system, assuming that we desire to maintain the same input impedance in the probe. The Fairchild Type 7994B is a 3-1/2 foot probe with an input impedance of 10 megohms and 7 picofarads which will provide a 78 Mc system bandwidth when used with the Type 79-02A Dual Trace 100 Mc Amplifier.

c. EFFECT OF PROBE GROUND LEAD ON PULSE RESPONSE
(Figures 2-9 to 2-11)

The most common problem encountered when using a high-frequency probe is the introduction of high-frequency ringing due to the use of an excessively long ground lead. When using the Type 7994B Probe to monitor fast-rise pulses, a ground lead as short as possible should be employed. See Figures 2-9 to 2-11. Optimum pulse response is shown in Figure 2-11. The ringing observed in Figures 2-9 and 2-10 is due to excitation of a resonant circuit made up of the ground lead inductance of the probe input capacity.

It is obvious from the foregoing that the pulse response and bandwidth can be greatly exaggerated due to improper grounding of the probe. Correct use of the probe and an understanding of its capabilities and limitations will insure the display of true information on the oscilloscope.

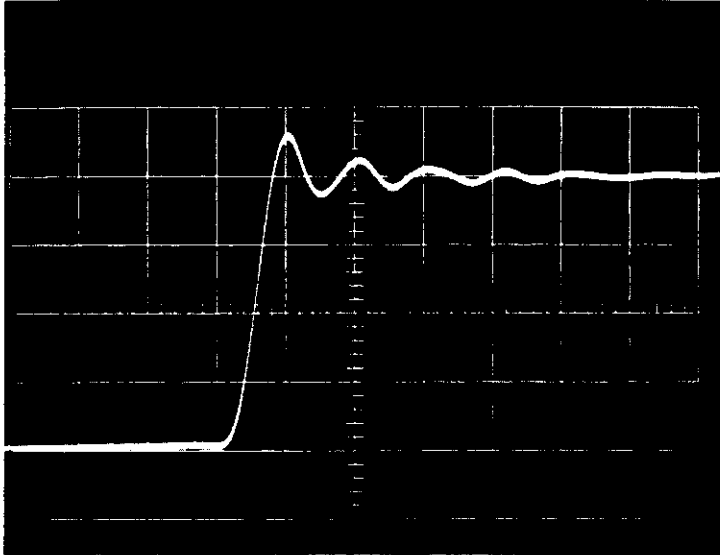


Figure 2-9.

Pulse response when using 6-inch ground lead on Type 7994B Probe

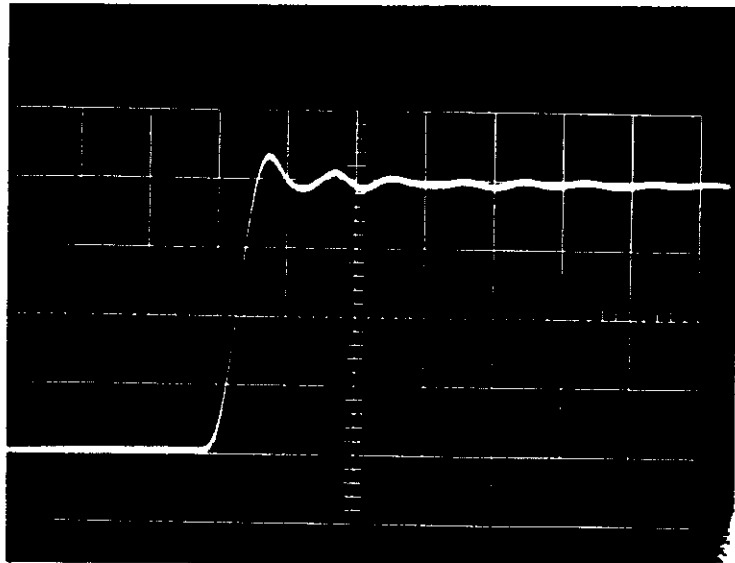


Figure 2-10.

Pulse response when using 3-inch ground lead on Type 7994B Probe

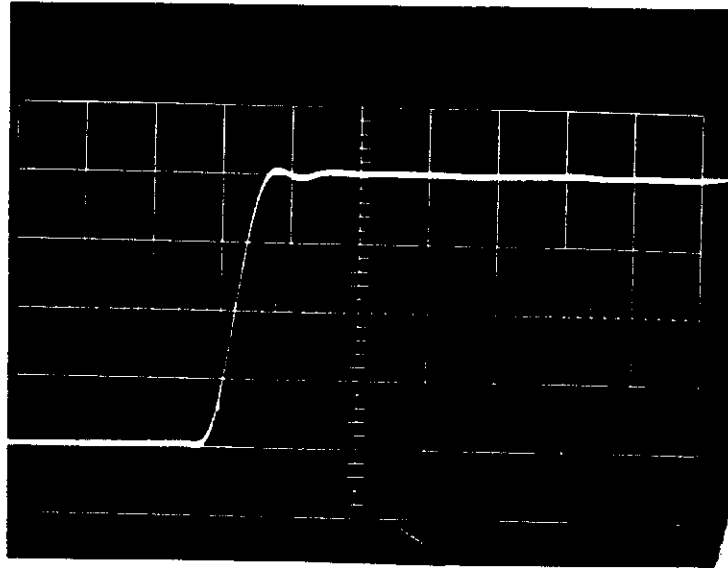


Figure 2-11. Pulse response using nose ground lead (an extremely short lead that connects directly to probe tip). Note that optimum pulse fidelity is achieved when using the nose ground on the Type 7994B Probe.

c. PROBE ADJUSTMENT

The Type 7994B Accessory Probe has an attenuation factor of 10 to 1. The maximum voltage that may be applied to this probe is 600 volts DC plus peak AC. Voltages in excess of this value (either DC volts or peak AC volts) may cause damage to components inside of the probe housing.

IMPORTANT: Before using the probe, always check its adjustment.

An adjustable capacitor in the probe compensates for variations in input capacitance from one unit to another. To insure accuracy in pulse and transient measurements, check the probe adjustment frequently. To check the probe, proceed as follows:

1. Connect the Probe to Input BNC connector on the Type 79-02A and apply the probe tip to the 1V CAL pin jack on the Main Frame. Set Input Selector switch to DC.
2. Adjust the oscilloscope to display several cycles of the calibrator waveform.
3. Adjust the variable capacitor in the body of the probe for a flat-top trace on the screen.
4. To preserve the waveform of the signal being displayed, clip the probe ground lead to the chassis of the equipment being tested. Select a short, clean, ground point near the probe input connection.

2-9. DUAL-TRACE OPERATION

Using the Type 79-02A Dual Trace Plug-in unit with the Main Frame, makes it possible to view two different time-shared vertical input signals displayed against one time base. The electronic switch will alternately accept either the Channel 1 or Channel 2 signal when the MODE switch is set to ALT. Each channel retains individual control of sensitivity, position, polarity, etc. Should the sweep rate be so low that the display has excessive flicker, the MODE switch may be set to CHOP position. The electronic switch will now chop the signals at either a 100Kc or 1Mc rate. Chopping rate is selected by an internal toggle switch. Switching transients will automatically be blanked for a clean, undistorted display.

The dual-trace display applications include comparisons of the input and output of amplifiers, multivibrators, shaping circuits, comparative phase and time delay measurements, etc.

Do not use normal internal triggering when in the chopped mode, since the sweep will trigger on the switching transients rather than on the signal. CHANNEL 2 ONLY triggering should be used.

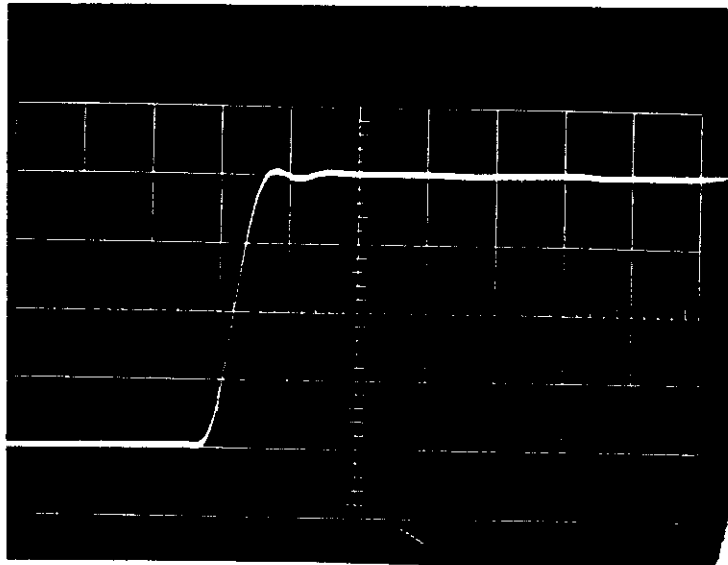


Figure 2-11. Pulse response using nose ground lead (an extremely short lead that connects directly to probe tip). Note that optimum pulse fidelity is achieved when using the nose ground on the Type 7994B Probe.

c. PROBE ADJUSTMENT

The Type 7994B Accessory Probe has an attenuation factor of 10 to 1. The maximum voltage that may be applied to this probe is 600 volts DC plus peak AC. Voltages in excess of this value (either DC volts or peak AC volts) may cause damage to components inside of the probe housing.

IMPORTANT: Before using the probe, always check its adjustment.

An adjustable capacitor in the probe compensates for variations in input capacitance from one unit to another. To insure accuracy in pulse and transient measurements, check the probe adjustment frequently. To check the probe, proceed as follows:

1. Connect the Probe to Input BNC connector on the Type 79-02A and apply the probe tip to the 1V CAL pin jack on the Main Frame. Set Input Selector switch to DC.
2. Adjust the oscilloscope to display several cycles of the calibrator waveform.
3. Adjust the variable capacitor in the body of the probe for a flat-top trace on the screen.
4. To preserve the waveform of the signal being displayed, clip the probe ground lead to the chassis of the equipment being tested. Select a short, clean, ground point near the probe input connection.

2-9. DUAL-TRACE OPERATION

Using the Type 79-02A Dual Trace Plug-in unit with the Main Frame, makes it possible to view two different time-shared vertical input signals displayed against one time base. The electronic switch will alternately accept either the Channel 1 or Channel 2 signal when the MODE switch is set to ALT. Each channel retains individual control of sensitivity, position, polarity, etc. Should the sweep rate be so low that the display has excessive flicker, the MODE switch may be set to CHOP position. The electronic switch will now chop the signals at either a 100Kc or 1Mc rate. Chopping rate is selected by an internal toggle switch. Switching transients will automatically be blanked for a clean, undistorted display.

The dual-trace display applications include comparisons of the input and output of amplifiers, multivibrators, shaping circuits, comparative phase and time delay measurements, etc.

Do not use normal internal triggering when in the chopped mode, since the sweep will trigger on the switching transients rather than on the signal. CHANNEL 2 ONLY triggering should be used.

2-10. DUAL TRACE TRIGGERING

a. INTRODUCTION

For simplicity, dual-trace triggering may be categorized as follows:

1. External triggering using alternate or chopped modes of operation.
2. Internal triggering (NORM or CH 2 ONLY) using the alternate mode.
3. Internal triggering (CH 2 ONLY) using the chopped mode.

b. EXTERNAL TRIG USING CHOP OR ALT MODES

For dual-trace operation, it is preferable to trigger the time base with an external signal which bears a fixed time relationship to the applied signal. One of the applied signals may normally be employed as the external triggering signal. When this technique is used, a stable display is more readily obtained, and the true time or phase relationship of the two signals is discernible.

In low frequency applications, one of the applied signals may be used as the external triggering signal. In general, useful stable displays may be obtained by this technique without excessively loading the signal source. However, in high-frequency applications, such a method for deriving the triggering signal loads down the signal source resulting in an unsatisfactory display. Therefore, a minimum-loading method must be used for obtaining the external trigger. For example, if the Fairchild Type 781A Time-Mark Generator is the signal source, use the TRIGGER OUT pulse from this generator to externally trigger the oscilloscope.

c. INTERNAL TRIG USING ALT MODE

Internal triggering of the time base may be used if the time or phase relationship between the two signals is not critical. In alternate mode of operation, the signal applied to the Type 79-02A internally triggers the Time Base Module, which in turn switches the channels at the completion of each sweep cycle during the retrace intervals.

Hence, it is important to set the Time Base TRIG LEVEL control to a point where the sweep can trigger on the signal applied to each channel. If one of the applied

signals possesses a smaller amplitude than the other, then the TRIG LEVEL control must be set for reliable triggering on the smaller amplitude signal.

Also, to avoid triggering on the change in dc positioning level between channels, set the Time Base Coupling switch to ACF or LF REJECT, when in the NORMAL trigger position.

As an alternative, the Type 79-02A may be set up for single channel internal triggering in the alternate mode by setting the TRIGGER switch to CH 2 ONLY.

d. INTERNAL TRIG USING CHOP MODE

For dual-trace chopped-mode operation, use CH 2 ONLY mode for reliable internal triggering. The advantages of internal triggering on CH 2 ONLY over the use of external sync trigger are:

- Increased sensitivity with effectiveness of using external trigger.
- Decreased loading.
- Minimum cabling to the oscilloscope.
- Two effective external trigger inputs.

2-11. SETTING UP AMPLIFIER FOR GREATER INPUT SENSITIVITY

The Type 79-02A Dual Trace Amplifier may be set up to provide an input sensitivity of 1 millivolt/division with an accompanying reduction in bandwidth. This is accomplished by setting the CH 1 INPUT SELECTOR switch in the CH 2 position. The output from Channel 2 pre-amplifier is now in series with the input of Channel 1 amplifier.

Next, apply the desired signal to Channel 2 Input connector. Set the TRIGGER switch to NORM and the MODE switch to CH 1. The maximum over-all input sensitivity will now be 1 millivolt/division. The front panel GAIN ADJ screwdriver control may require slight readjustment to achieve this sensitivity. Application of this technique for achieving greater sensitivity causes the system to have lower bandwidth and slower rise time. A nominal 30 Mc bandwidth and a rise time of 14 nanoseconds may be expected from cascaded amplifier operation.

2-12. VOLTAGE MEASUREMENTS

Note: When making voltage measurements, make sure there is a common ground between the oscilloscope and the signal source.

a. GENERAL

The Type 766H/F Family of Oscilloscopes may be used to measure the voltage of the input signal by using the calibrated VOLTS/DIV setting and observing the height of the display on the screen in graticule divisions.

When making voltage measurements, use full scale vertical deflection to insure maximum accuracy. Also, it is important to remember that the width of the trace may be an appreciable part of the over-all measurement.

This is particularly true when you are measuring signals of small amplitude or when stray signal pickup has broadened the trace. The operator should consistently make all measurements from one side of the trace. If the top side of the trace is used for one reading, it should be used for all subsequent readings.

b. MEASURING PEAK-TO-PEAK VOLTAGES (Figure 2-12)

The procedure employed for all voltage measurements is basically the same. The VARIABLE control must be set to CAL. The Specific examples that follow are intended to show the general procedure. These examples may be adapted to fit any particular application.

To measure the AC component of the signal on display, set the Input Selector switch to AC. In this position, only the AC components of the input signal are displayed on the screen. However, when the AC components of the input is of very low frequency, set the Input Selector switch to DC to prevent errors.

To make measurements, proceed as follows:

1. Using the calibrated scale, measure the vertical deflection in graticule divisions from the positive peak to the negative peak of the waveform.
2. Multiply the vertical dimension obtained in step 1 by the VOLTS/DIV switch setting to obtain the indicated voltage.
3. Multiply the indicated voltage obtained in step 2 by the attenuation factor of the probe, if one is used, to obtain the actual peak-to-peak voltage.

For example, suppose that you are using a 10:1 Attenuator Probe and the VOLTS/DIV switch is set to 0.1. Assume that the vertical distance between the peaks of the waveform measures 4 graticule divisions. Now, this graticule dimension of 4 is multiplied by the VOLTS/DIV setting of 0.1 to give 0.4 volt. Next, multiply this result by 10, if a 10:1 Attenuator Probe is used. This gives 4 volts as the peak-to-peak voltage of the display waveform.

Note: Always make sure that the VARIABLE control is set to CAL when making measurements.

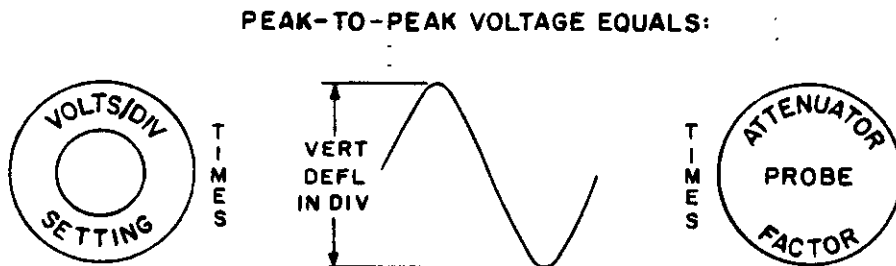


FIGURE 2-12. PEAK-TO-PEAK VOLTAGE MEASUREMENTS

c. MEASURING INSTANTANEOUS VOLTAGES WITH RESPECT TO A REFERENCE POTENTIAL (Figure 2-13)

The technique used for measuring instantaneous voltages with respect to a reference point, is virtually the same as that described for peak-to-peak voltage measurements. The difference is that now a reference point must be established on the screen of the oscilloscope. Since voltage measurements with respect to ground are the most common, the procedure which follows, establishes ground as the reference point. The same general technique may be used for instantaneous measurements with respect to any other potential, just so long as that potential is employed to establish the reference point.

To make measurements, proceed as follows:

1. Set the Input Selector switch to DC.
2. Adjust the appropriate Time Base Plug-in controls to obtain a reference trace.

3. To establish the reference point, touch the probe tip to the ground terminal on the oscilloscope (or to the desired source potential, if a point other than ground is used). Vertically position the trace to a convenient point on the screen. This point should be chosen so that it lies on one of the major horizontal scale divisions. The chosen horizontal scale line, which is now coincident with the trace, is the reference line from which all voltage measurements are to be made.
4. Disconnect the probe tip from ground and connect it to the signal source without disturbing the POSITION control.
5. Adjust the oscilloscope controls for a suitable and stable display.
6. Using the calibrated scale, measure the number of graticule divisions from the desired point on the waveform to the pre-established reference line set up in step 3.
7. Multiply the graticule dimension obtained in step 6 by the VOLTS/DIV switch setting to obtain the indicated voltage. Make sure that the VARIABLE control is set to CAL.
8. Multiply the indicated voltage obtained in step 7 by the attenuation factor of the probe used to obtain the actual instantaneous voltage.

For example, suppose that you are using a 10:1 Attenuator Probe and the VOLTS/DIV switch is set to 0.1. Assume that the vertical distance between the desired point on the waveform to the pre-established reference line is 4 graticule divisions. Now, multiply this vertical deflection of 4 graticule divisions by the VOLTS/DIV setting of 0.1 to give 0.4 volts. Next, multiply this result by 10, the attenuation factor of the probe. This shows that the instantaneous voltage with respect to ground to be 4 volts. Since the voltage point is above the reference line, the indicated polarity is positive.

INSTANTANEOUS VOLTAGE TO REFERENCE LINE EQUALS:

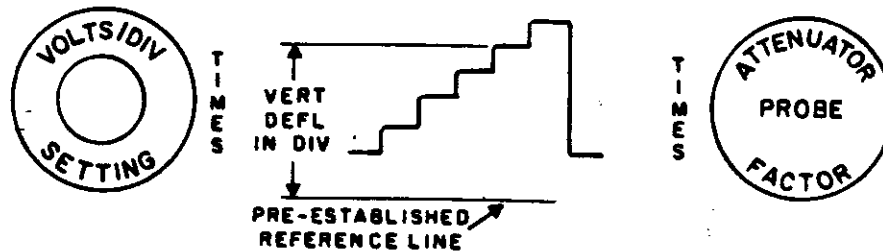


Figure 2-13. Instantaneous Voltage Measurement with Respect to a Reference Potential.

2-14 MEASURING SHORT RISE TIMES (Figure 2-14)

The response of an amplifier or other electronic device to a step function input signal is a measure of the ability of the device to pass signals without distortion. In general, the response of the device can be measured by comparing the rise time of the output signal with the rise time of the input signal. In the ideal case, the signal would be passed with zero change of rise time, indicating all signals would be passed without distortion. Further, if two devices yield identical rise times for the same step function input, they can be expected to provide similar responses to all types of waveforms.

The rise time is defined as the time between 10% and 90% of the amplitude.

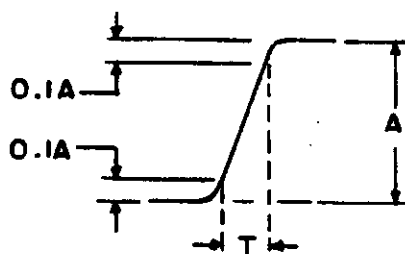


Figure 2-14.
Rise Time Sketch

To measure rise time, connect the circuit under investigation with a 50-ohm cable RG-8A/U, terminated with a 50-ohm pad to the input of the

oscilloscope. The rise time of the circuit is expressed in the form:

$$t_p = \sqrt{(t_o)^2 - (t_a)^2}$$

Where:

- t_p = actual pulse rise time
- t_o = observed rise time of pulse displayed on oscilloscope
- t_a = amplifier rise time

Once the amplifier rise time is known (see Specifications) the rise time of any pulse may be calculated.

The display of the pulse should be within the quality square of 6 divisions to avoid saturation of the output circuits and related distortion of the pulse response.

SECTION 3

FUNCTIONAL BLOCK DIAGRAMS

Functional Block Diagrams are provided as follows:

- Figure 3-1. Type 79-02A Input Circuit, Simplified Functional Block Diagram
- Figure 3-2. Type 79-02A Channels 1 & 2 Pre-Amplifiers, Simplified Functional Block Diagram
- Figure 3-3. Type 79-02A X10 Amplifiers, Functional Block Diagram
- Figure 3-4. Type 79-02A Electronic Switching Circuit, Functional Block Diagram
- Figure 3-5. Type 79-02A Y Deflection Amplifier, Functional Block Diagram
- Figure 3-6. Type 79-02A Trigger Amplifiers, Functional Block Diagram

Refer to Figure 5-1 in the Maintenance and Recalibration Section for the over-all system block diagram.

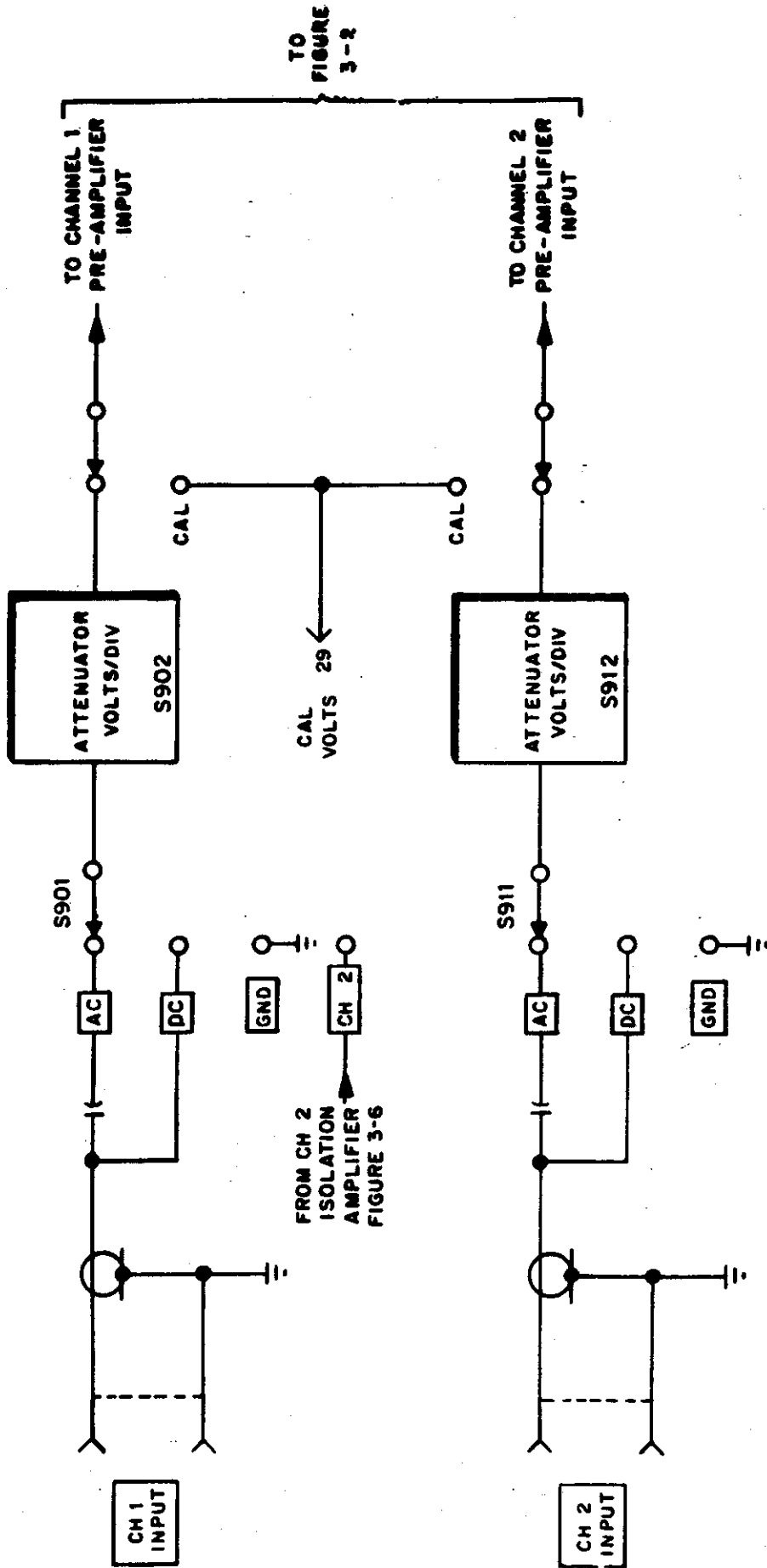


FIGURE 3-1. TYPE 79-02A INPUT CIRCUIT, SIMPLIFIED FUNCTIONAL BLOCK DIAGRAM

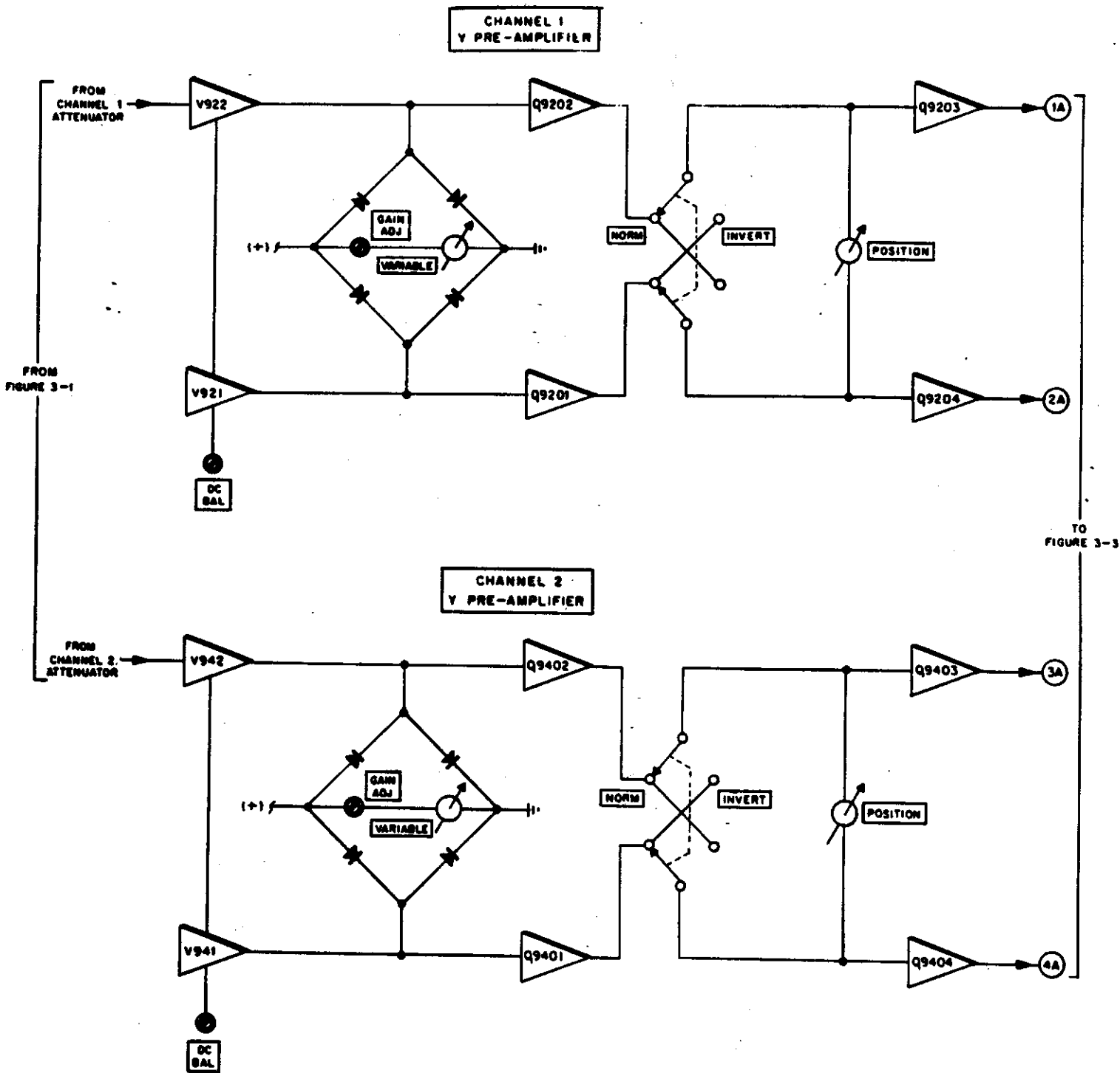


FIGURE 3-2. TYPE 79-02A CHANNELS 1 & 2 PRE-AMPLIFIERS, FUNCTIONAL BLOCK DIAGRAM

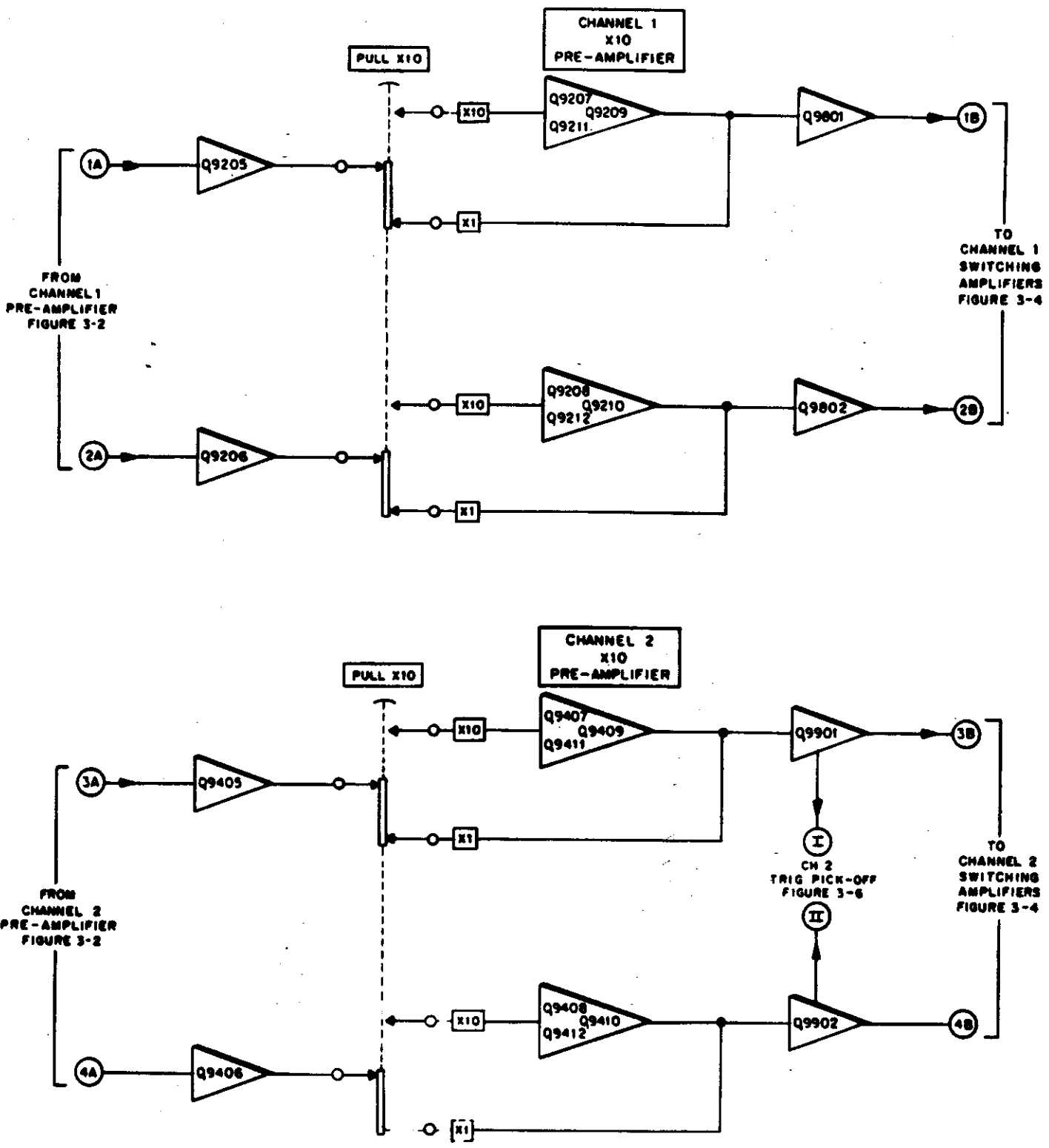


FIGURE 3-3. TYPE 79-02A X10 AMPLIFIERS, FUNCTIONAL BLOCK DIAGRAM

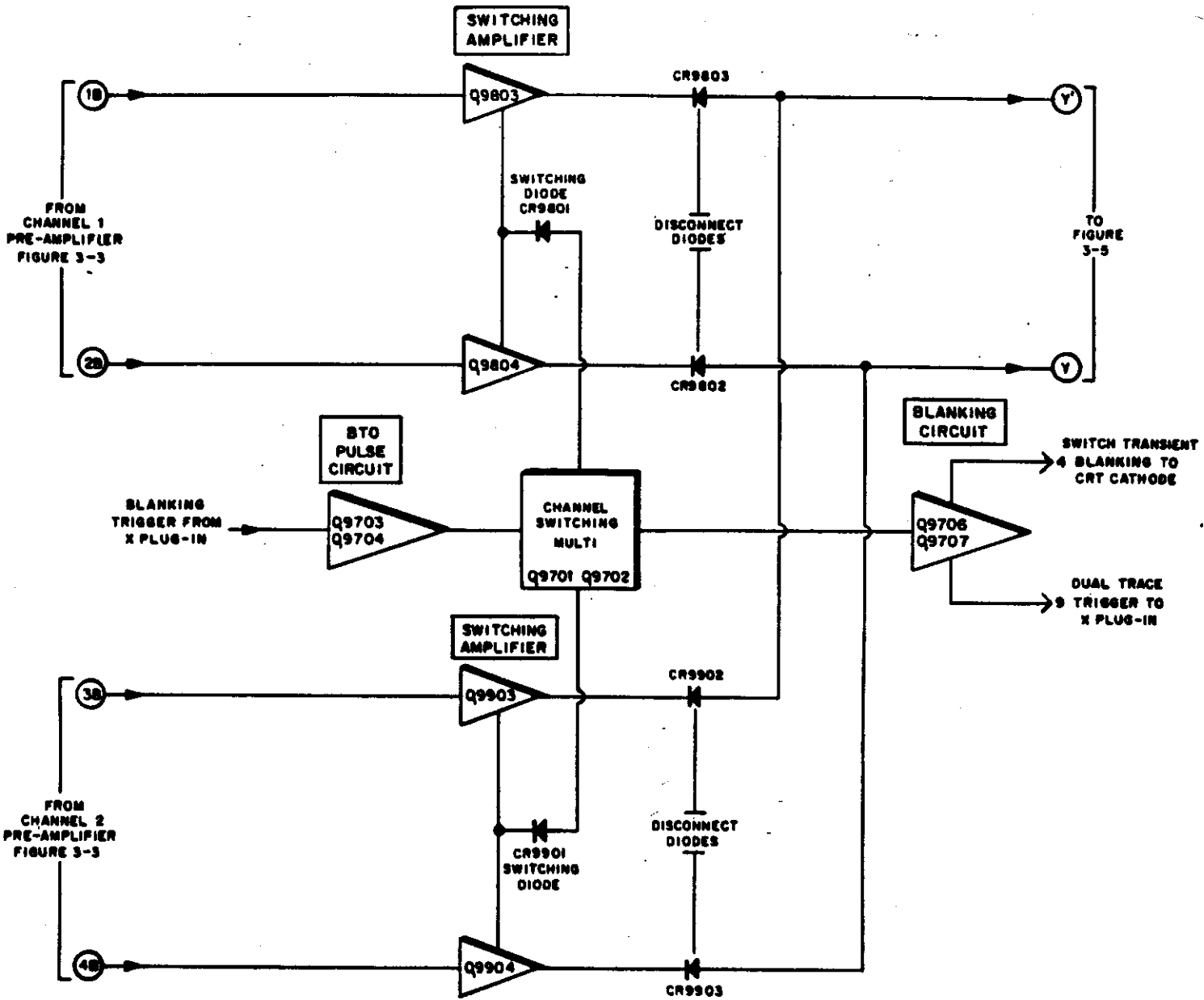
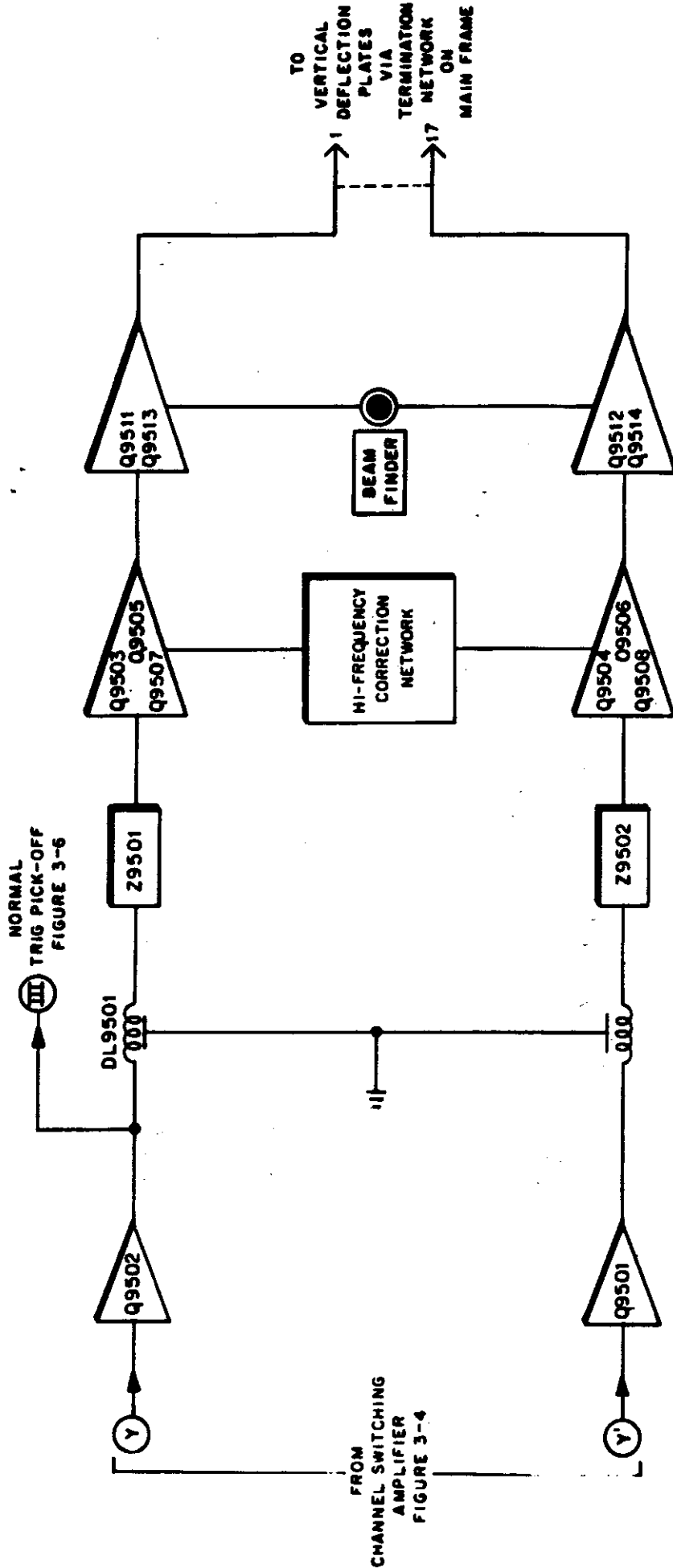


FIGURE 3-4. TYPE 79-02A ELECTRONIC SWITCHING CIRCUIT FUNCTIONAL BLOCK DIAGRAM

VERTICAL DEFLECTION AMPLIFIER



**FIGURE 3-5. TYPE 79-02A Y DEFLECTION AMPLIFIER
FUNCTIONAL BLOCK DIAGRAM**

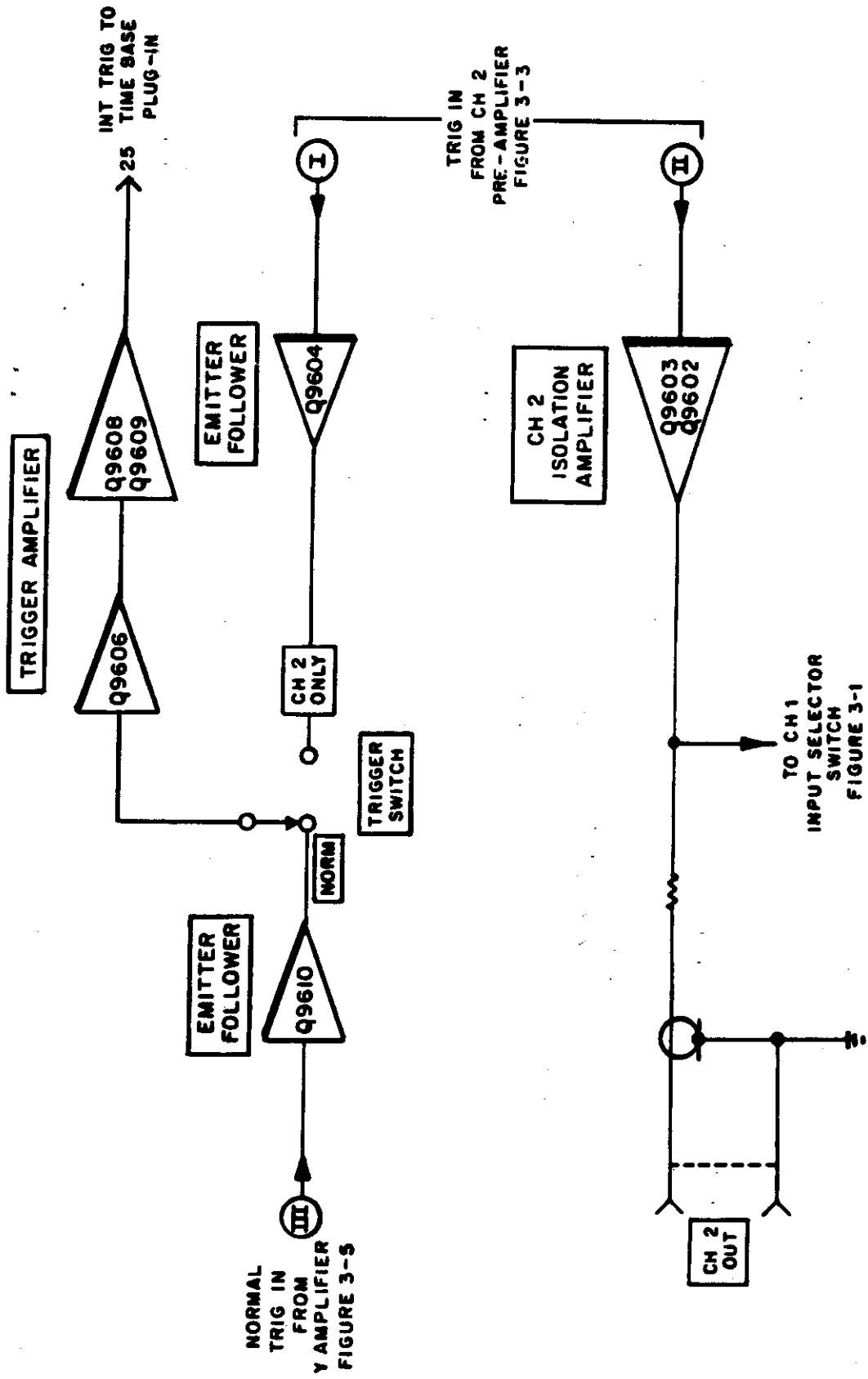


FIGURE 3-6. TYPE 79-02A TRIGGER AMPLIFIERS, FUNCTIONAL BLOCK DIAGRAM



SECTION 4

PERFORMANCE ASSURANCE TEST

4-1. MAINTENANCE CHECK TO ASSURE PERFORMANCE

The tests described in the paragraphs to follow should be performed by Instrument Test Departments and Maintenance Laboratories to certify proper performance. These tests are divided into sections for simplification and to assist those test groups where complete checking is not mandatory, or where all test equipment is not available. Refer to Section 5, paragraph 5-5, for list of test equipment required.

- All tests are performed with a representative Type 766H/F Series Main Frame Oscilloscope and a Time Base Plug-in. Both of the plug-in units must be normalized to the Main Frame before starting tests. This is accomplished by adjusting the front-panel screwdriver SWP CAL and GAIN ADJ control as described in the appropriate plug-in Instruction Manuals. Allow 30 to 60 minutes of warmup time before making any adjustments.

NOTE

If this Plug-in module is checked by a Receiving Inspection laboratory, the tests outlined below are recommended to certify performance. This instrument has been thoroughly tested and aged at the factory. Nevertheless, rough shipment, extreme environments, or long idle periods may necessitate minor adjustments of the controls. Hence, it is suggested that the certifying engineer try the recommended adjustments not only for recentering the controls, but also to ascertain their range and to familiarize himself with this precision instrument. If after performing all the tests outlined in the paragraphs to follow, the instrument will not perform to specification, the assistance of the local Fairchild Field Engineering representative should be requested.

4-2. CHECKING DC BALANCE ADJUSTMENT

1. Set the MODE switch to CH 1 and the Input Selector Switch to GND.
2. Set the VOLTS/DIV switch to 0.1 position and rotate the VARIABLE control to its minimum gain setting.
3. Set the Time Base Plug-in controls for automatic triggering to obtain a reference trace on the screen.
4. Adjust the POSITION control, on each plug-in, to center the trace on screen (reference line).
5. Rotate the VARIABLE control right and left throughout its range observing the direction the trace shifts vertically.
6. Adjust the front-panel DC BAL screwdriver control to bring the trace back to center of screen.

Note: DO NOT CHANGE THE POSITION CONTROL SETTINGS.

7. Continue adjusting the DC BAL control while rotating the VARIABLE control back and forth, until there is minimum displacement of the trace when the VARIABLE control is rotated throughout its range.
8. Repeat Channel 1 balance adjustments for Channel 2 using pertinent controls.

Note: If the adjustment range of the front-panel DC BAL control is insufficient, refer to Section 5, Maintenance and Recalibration, for the complete Coarse and Fine Balance adjustment procedure.

4-3. CHECKING SENSITIVITY OF CHANNELS 1 & 2

1. Set both Channel 1 and Channel 2 VOLTS/DIV switches to CAL and turn both VARIABLE controls to CAL (fully cw).
2. Push in both VARIABLE controls to set up the amplifier for X1 operation.
3. Set MODE switch to CH 1 and TRIGGER switch to NORM.

4. Adjust Time Base unit for LINE triggering and for a sweep rate of 10 msec/div and observe 6 cycles of calibrator waveform at 60-cycle line. (5 cycles for 50-cycle line.)
5. Set MODE switch to ALT.
6. Check range of Channel 1 GAIN ADJ front-panel screw-driver control. It should control the amplitude of the calibrator signal providing at least 4.1 cm of deflection peak-to-peak. Set Channel 1 GAIN ADJ control for 4 divisions of vertical deflection.
7. Position the trace one on top of the other.
8. Adjust Channel 2 GAIN ADJ control until only one trace may be observed (traces are superimposed).

4-4. CHECKING FAST RISE TIME OF CHANNELS 1 AND 2

1. Connect a Fairchild Type 791A Square-Wave Generator equipped with a Type 7911A Fast Rise Adapter, to the Type 79-02A. Connection should be through a 3-db pad and a 50-ohm cable, terminated in a 50-ohm pad with the Adapter connected to the oscilloscope.
2. Set both Channel 1 and Channel 2 VOLTS/DIV switches to 0.5 and turn both VARIABLE controls to CAL (fully cw).
3. Push in the VARIABLE control to the X1 position.
4. Set MODE switch to CH 1 and TRIGGER switch to NORM.
5. Set the SOURCE IMPEDANCE switch on the Square Wave Generator to 50Ω , OUTPUT AMPLITUDE control at maximum and FREQUENCY dial set to 1 Mc. Observe 4 divisions of positive rise on the oscilloscope.

Note: The overshoot, or preswing should be less than 0.25 division and ringing less than 0.1 division.

Rise time (10% to 90%) should be 3.8 nano-seconds or less. This includes the rise time of the Type 7911A Fast Rise Adapter.

4-5. CHECKING MODE SWITCH

1. Set MODE switch to CH 1 and operate Channel 1 POSITION control to check vertical displacement of the display.
2. Set MODE switch to CH 2 and operate Channel 2 POSITION control to check vertical displacement of the display.
3. Set MODE switch to ALT and operate both POSITION controls checking that they control their respective displays.
4. Set MODE switch to CHOP and operate both POSITION controls checking that they control their respective displays.
5. Set MODE switch to ADDED and operate either POSITION control checking that either one controls the display.

4-6. CHECKING CHOPPED OPERATION

1. Set the internal CHOP RATE switch (Figure 5-11) to 100 Kc on the Type 79-02A chassis and the front panel MODE switch to CHOP.
2. Adjust Time Base Plug-in for a sweep rate of 5 uSEC/DIV and INT Triggering.
3. Position both base lines on the screen.
4. Check that the total time for blanking and unblanking for each channel is less than 15 microseconds and that the switching transients are blanked.
5. Set the CHOP RATE switch to 1 Mc.
6. Adjust Time Base Plug-in for a sweep rate of 0.5 uSEC/DIV.
7. Check that the total time for blanking and unblanking for each channel is less than 1.5 microseconds and that the switching transients are blanked.

SECTION 5

MAINTENANCE AND RECALIBRATION

5-1. INTRODUCTION (Figure 5-1)

This section of the Instruction Manual contains service information and procedures for internal adjustments. Refer to Figure 5-1 for an over-all functional block diagram of the Type 79-02A system.

5-2. REMOVAL AND REPLACEMENT OF PARTS

If it is necessary to order a replacement component from the factory, always give the Type Number and Serial Number of the instrument. Before ordering parts for in-warranty replacement or purchasing them for out-of-warranty replacement, be sure to consult the Parts List in this manual. The Parts List gives the values, tolerances, ratings and the factory part number for all electrical components used in the instrument. This will help to expedite service.

Since your instrument left the factory, some of the parts may have been superseded by improved components. In such cases, the part numbers of these new components will not be listed in your Parts List. However, if you order a part from the factory, and it has been superseded by an improved component, the new part will be shipped in place of the part ordered.

It is the aim of Fairchild to make available the most reliable commercial oscilloscopes within the state of the art and to provide services which will help the user to rapidly restore any of our equipment to its specified performance. Your local Fairchild representative maintains a limited number of spare parts. Also, the factory may be asked to airship replacement parts on a rush basis.

5-3. SERVICING HINTS

General maintenance and trouble shooting information is given in the Type 766H/F Series Oscilloscope Instruction Manual. In the following discussion, it is assumed that you have already read that information and have definitely isolated a trouble in this Plug-in Module.

In trouble-shooting a Plug-in Unit, it becomes necessary to determine if the defect is in the plug-in or in the Main Frame of the oscilloscope. The quickest and easiest way of isolating the trouble is to substitute another plug-in unit and determine if the same trouble persists. If the trouble continues after substitution, it can be safely assumed that the defect is in the Main Frame.

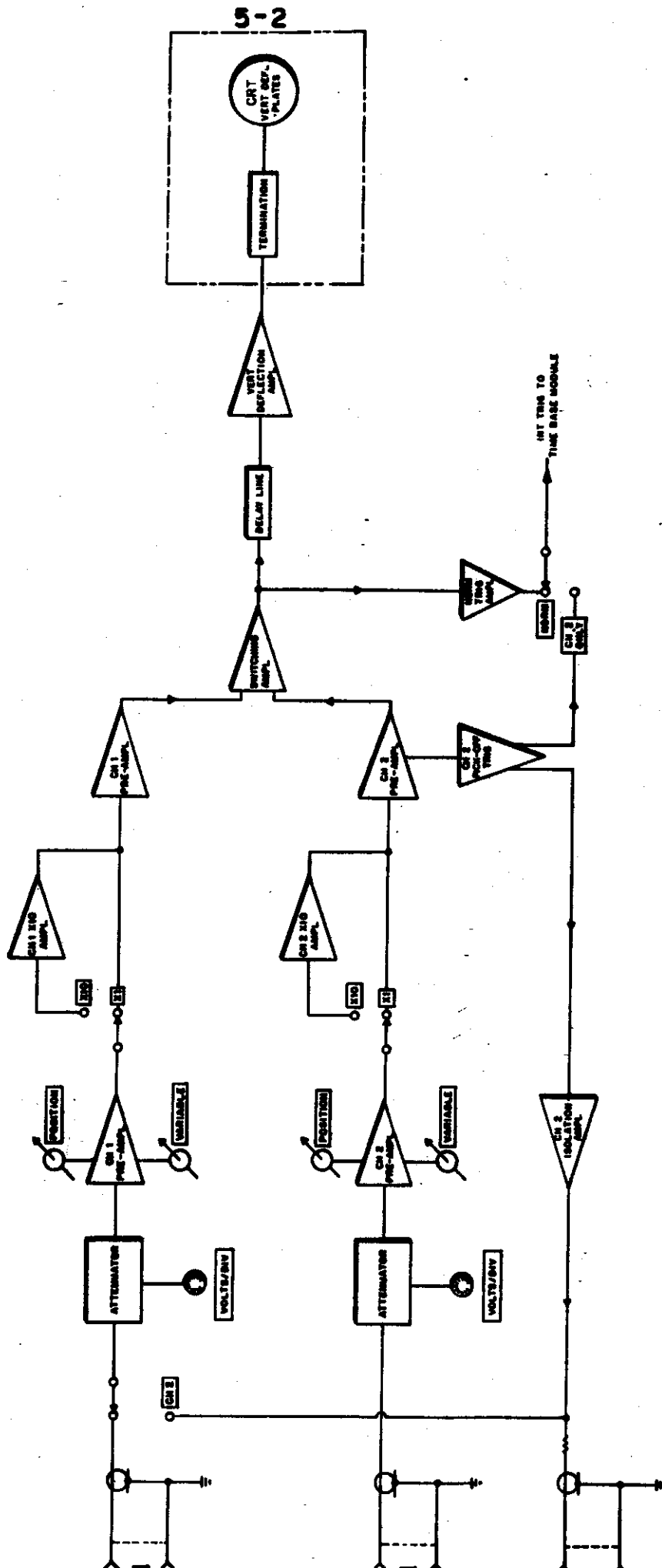


FIGURE 8-1 TYPE 79-02A OVER-ALL SYSTEM BLOCK DIAGRAM

There is no simple way of locating troubles. An understanding of the functions of the circuits is the best help. With an understanding of the circuit operation, it will be possible to make a good guess at the general source of troubles from the symptoms. As an aid in trouble shooting this unit, refer to the system block diagram in this Section and also to the schematics.

To keep electronic units operating at top performance, it is desirable to check the equipment at regular intervals. The period between checks will depend on the installation and the conditions of operation. For these regular checks, clean all dust and dirt from the unit using a light air blast or soft brush. However, to insure the reliability of measurements, we suggest that you recalibrate the Plug-in after each 500 hours of operation or every six months if used intermittently. Also, the calibration of a unit should always be fully checked and adjusted after the repair or replacement of any component in the unit. The complete adjustment procedure for this unit is given in this Section of the Instruction Manual.

In the event of improper performance of the Plug-in unit, the following suggestions are recommended:

1. The Type 4294 Extension Cable for remote operation of the plug-in from the oscilloscope is available as an accessory. This plug-in extender will be helpful for routing maintenance and recalibration. Do not use this extension for HF alignments; instead, remove the Main Frame side cover.
2. A Type 766H/F Test Oscilloscope is recommended for localizing troubles, especially when servicing a Type 79-02A inserted in a Type 766H/F Oscilloscope. To check waveforms, use a high-impedance probe while trouble shooting.
3. Maintain a high quality of workmanship. Use a clean bench and soldering iron; keep solder joints smooth and bright; do not overheat any component while soldering. Use heat sinks when soldering semiconductors. The use of a 30-watt iron such as a Hexacon Type 26S is recommended.
4. When using accessory probes or adapters, be sure the trouble is not originating in the accessory before suspecting the instrument itself.
5. Once the defective stage has been localized, the component or components causing the trouble can be located by tube and component substitution or by voltage measurement. Key voltage measurements are shown on the over-all schematics at the rear of this manual.
6. Electron tubes, semiconductors, and service adjustments are identified on photographs located in this Section of the manual.

5-4. GAINING ACCESS TO CHASSIS

Since the Plug-in is not contained in its own dust cover, most of the components are readily accessible when the plug-in is removed from the Main Frame. To gain access to the chassis, simply unscrew the knurled thumbscrew at center bottom of unit and pull it free of the Main Frame.

WARNING

WHEN THE PANELS OR PLUG-INS ARE REMOVED FROM THE INSTRUMENT FOR SERVICING, EXERCISE CAUTION WHILE THE POWER IS ON. The lower-voltage busses are potentially more dangerous than the cathode-ray tube potential because of the high current capabilities and large filter capacitors employed in these supplies. When you reach into the instrument with one hand while it is turned on, do not grasp the metal frame with the other hand. If possible, stand on an insulated floor and use insulated tools. It is advisable to ground the third lead in the power cord whenever the instrument is in use.

Note: Always use insulated tools while working or making adjustments on the unit when power is on. The transistors in this instrument may be damaged if over-voltaged by accidental grounding of one or more elements. Exercise caution and turn off power when making repairs.

5-5. TEST EQUIPMENT REQUIRED FOR SERVICE ADJUSTMENTS

a. INTRODUCTION

The adjustments outlined in the following paragraphs are based on the test procedure followed at the factory. All adjustments should be made at mid-line voltage, 115V/230V $\pm 2\%$.

To set up the Amplifier Plug-in unit for calibration, insert the Amplifier Plug-in and Time Base Plug-in into the Main Frame. The Time Base Plug-in module and Main Frame must be fully tested and certified units.

b. TEST EQUIPMENT REQUIRED (Equivalent may be substituted)

<u>Equipment</u>	<u>Description</u>
Oscilloscope	Fully certified and tested Type 766H/F Main Frame
X Plug-in	Type 74-03A Time Base
Volt-ohmmeter	Simpson Model 260; 20K ohms/volt sensitivity
Square Wave Generator	Fairchild Type 791A
Fast Rise Adapter	Fairchild Type 7911A
Square Wave Generator	Tektronix Type 105A
Capacitance Standardizer	Fairchild Type 7012A (1M, 14 pf)
Micromiker	Kaylab Model 402B
Extension Cable for Remote Operation of Plug-in	Fairchild Type 4294
Alignment Tools	Fairchild Type 7013 Tool Kit
50-ohm Termination	
93-ohm Termination	
50-ohm Cable	Fairchild Type 7082
Pads, Attenuator	GR 20 db (2); GR 3 db (1); GR 6 db (1)
Standard Amplitude Calibrator	Ballantine Type 420

Turn on the power and allow 30 minutes of warm up time.

5-6. GAS COMPENSATION ADJUSTMENTS R9201 (R9401)

Note: Channel 2 adjustments are designated by reference symbols in parenthesis.

Undesirable voltages are developed at the grids on V922 and (V942) due to leakage currents. These potentials are nulled by the proper adjustments of the GAS COMP potentiometers R9201 and (R9401). To adjust, proceed as follows:

1. Preset both Channel 1 and Channel 2 front-panel controls as indicated.

<u>Control</u>	<u>Settings</u>
VOLTS/DIV	0.1
VARIABLE	CAL X1 (fully cw, pushed in)
NORM-INVERT	NORM

2. Set up the Time Base controls for automatic triggering.
3. Adjust the GAS COMP potentiometer R9201 for no deposition of the trace while switching Channel 1 Input Selector slide switch from GND to AC.
4. Repeat step 3 for Channel 2 adjusting(R9401).

5-7. DC AND BRIDGE BAL ADJUSTMENT R9206 (R9406) AND R9220 (R9420)

If the dc balance of the Type 79-02A Amplifier is not properly adjusted, the reference trace on the screen will be deposited when the VARIABLE control is rotated. To properly adjust, proceed as follows:

1. Preset both Channel 1 and Channel 2 front-panel controls as indicated.

<u>Control</u>	<u>Settings</u>
Input Selector	GND
VOLTS/DIV	0.1
VARIABLE	CAL X1 (fully cw, pushed in)
NORM INVERT	NORM
GAIN ADJ	fully cw
DC BAL	centered

2. Set the MODE switch to Channel 1 and the TRIGGER switch to NORM.
3. Adjust Time Base controls for automatic Triggering to obtain a reference trace on the screen.

4. Adjust the POSITION controls to set reference trace to center of screen.
 5. Adjust the COARSE DC BAL internal control R9206 (R9406) for minimum depositioning of the trace while rotating Channel 1 VARIABLE control back and forth throughout its range.
 6. Set CH 1 VOLTS/DIV switch to CAL.
 7. Adjust the DIODE LEVEL control R9220 (R9420) for maximum amplitude of the calibrator signal.
 8. Reset the VOLTS/DIV switch to the 0.1 position.
 9. Readjust the COARSE DC BAL internal control while rotating the front panel VARIABLE control back and forth throughout its range. Continue adjusting until there is min depositioning of the trace when the VARIABLE control is rotated throughout its range.
 10. Pull the VARIABLE control out to the X10 setting and continue adjusting the COARSE DC BAL control until there is min depositioning of the trace when the VARIABLE control is rotated.
 11. Trim up the front panel DC BAL control.
- Note: Proper adjustment of the COARSE DC BAL control will leave the front panel DC BAL control set to center of its range.
12. Set the MODE switch to CH 2 and repeat balance procedure using pertinent Channel 2 controls shown in ().

5-8. INVERT BALANCE ADJUSTMENT R9231 (R9431)

The NORM-INVERT switch is properly adjusted when there is no depositioning of the trace while switching the Polarity switch from NORM to INVERT and vice versa. To properly adjust proceed as follows:

1. Set the Input Selector switch S901 (S911) to GND, VOLTS/DIV switch to 0.1 position and VARIABLE control pushed in for X1 operation.
2. Adjust the Time Base controls for automatic triggering.
3. Adjust the internal INVERT BAL control R9231 (R9431) until there is no depositioning of the trace when the front panel Polarity switch is operated back and forth from NORM to INVERT and vice versa.

4. Make a final check of the balance beyond the delay only if the CRT is changed.
 - a. Connect a voltmeter (Simpson or equivalent), set to the most sensitive range, between P9001, Pins 1 and 17.
 - b. Short the bases of Q9503 and Q9504 together.
 - c. Check meter for a reading of zero volts +1V, and that trace falls within +0.2 divisions of the vertical center of the CRT.

If it does not, either resistor R9517 or R9518, located in the emitters of Q9503 and Q9504 should be tailored by shunting with a much larger resistor.

5. Repeat this procedure for Channel 2 using pertinent controls shown in ().

5-9. X10 LEVEL ADJUSTMENT R9263 (R9463)

The X10 LEVEL internal control is properly adjusted when there is no depositioning of the trace while switching from X1 to X10 amplifier operation. To properly adjust proceed as follows:

1. Rotate the X10 CAL internal control R9254 (9454) fully counterclockwise for minimum gain.
2. Connect a voltmeter, Simpson or equivalent, set on the 50V scale across the collectors of transistors Q9211 and Q9212 (Q9411 and Q9412).
3. Adjust the CH 1 POSITION control for zero reading on the voltmeter.
4. Connect the voltmeter from either the collector of transistor Q9211 or Q9212 (Q9411 or Q9412) to ground and note meter reading.
5. Pull the CH 1 VARIABLE control out for X10 operation.
6. Adjust the internal X10 LEVEL control R9263 (R9463) for the same voltage reading obtained for X1 operation in Step 4.
7. Disconnect the voltmeter and push in CH 1 VARIABLE control.
8. Repeat this procedure for Channel 2 adjusting pertinent controls shown in ().

5-10. OUTPUT CURRENT ADJUSTMENT (R9545)

1. Set the MODE switch to CH 2 and the TRIGGER switch to NORM.
2. Connect a voltmeter, Simpson or equivalent, set on the 50V scale across the collectors of transistors Q9511 and 9514.
3. Adjust the CH 2 POSITION control for zero reading on the voltmeter.
4. Connect the voltmeter from collector of transistor Q9511 to the +100V buss.
5. Adjust OUTPUT CURRENT ADJ internal control R9545 for a meter reading of 15 volts.
6. Connect the voltmeter from collector of transistor Q9514 to the +100V buss and again adjust the OUTPUT CURRENT ADJ control for a meter reading of 15 volts.
7. Repeat Steps 4 through 6 until maximum balance of the output current is obtained.

5-11. GAIN ADJUSTMENTS R9227 (R9427)

Whenever the Type 79-02A Dual Trace Amplifier is removed from one Main Frame to another the front-panel GAIN ADJ screwdriver control must be reset. To properly normalize the gain between the plug-in and the Main Frame, proceed as follows:

1. Set CH 1 and CH 2 VOLTS/DIV switches fully counter-clockwise to CAL.
2. Push in and turn CH 1 and CH 2 VARIABLE controls and turn them fully clockwise to CAL position.
3. Set the MODE switch to CH 1 and the TRIGGER switch to NORM.
4. Set the Time Base controls for AUTO SWP and LINE triggering.
5. Set the MODE switch to ALT and adjust sweep rate for 2 milliseconds/division.
6. Adjust CH 1 GAIN ADJ control for 4 divisions of vertical deflection.
7. Position the traces one on top of the other.
8. Adjust CH 2 GAIN ADJ control until trace is superimposed on CH 1 trace.

5-12. X10 CAL ADJUSTMENT R9254 (R9454)

1. Set the following front-panel controls for CH 1 and CH 2 as indicated.

<u>Control</u>	<u>Settings</u>
VOLTS/DIV	0.1
VARIABLE	CAL (fully cw)
Input Selector	AC
TRIGGER	NORM

2. Set the MODE switch to CH 1.
3. Adjust the Time Base controls for automatic triggering.
4. Apply a 0.4 volt peak-to-peak signal from a Ballentine Type 420 Calibrator to CH 1 Input connector J9001. Observe 4 divisions of vertical deflection. If necessary adjust CH 1 VARIABLE control to obtain precisely 4 divisions of deflection.
5. Adjust the Calibrator for a 0.04 volt output.
6. Pull out the CH 1 VARIABLE control for X10 operation.
7. Adjust the X10 CAL internal control R9254 (R9454) for 4 divisions of deflection.
8. Set the MODE switch to CH 2 and repeat above procedure adjusting pertinent Channel 2 controls.

5-13. TRIGGER DC LEVEL ADJUSTMENT R9618, R9619

1. With no signal input, adjust the oscilloscope to obtain a trace centered on the screen.
2. Set TRIGGER switch to NORM and MODE switch to CH 1 position.
3. Connect a voltmeter from J9001-25 to ground.
4. Adjust NORM TRIG ADJ internal control R9618 for zero reading on the meter.
5. Set the TRIGGER switch to CH 2 ONLY position, MODE switch to CH 2 and center trace on screen using channel 2 POSITION control.
6. Adjust CH 2 TRIG ADJ internal control R9619 for zero reading on the meter.

5-14. CHANNEL 2 OUTPUT LEVEL ADJUSTMENT R9614

1. With no signal input, adjust the oscilloscope to obtain a trace centered on screen.
2. Set the TRIGGER switch to CH 2 ONLY and MODE switch to CH 2.
3. Connect a voltmeter from CH 2 OUT connector to ground.
4. Adjust CH 2 OUTPUT LEVEL ADJ internal control R9614 for zero reading on the meter.

5-15. HIGH FREQUENCY ADJUSTMENTS (Figures 5-2 to 5-4)

a. CHANNEL 1 AND 2 AMPLIFIERS (X1 Operation)

1. Connect the output from a Fairchild Type 791A Square Wave Generator through a 50-ohm cable and a Type 7911A Fast Rise Step Generator and BNC Tee terminated in 50-ohm to the CH 1 Input connector on the Type 79-02A plug-in. See Figure 5-2.
2. Set the SOURCE IMPEDANCE switch on the Type 791A to 50-ohms and the FREQUENCY control to 1 megacycle.
3. Preset the following CH 1 and CH 2 panels controls as indicated.

<u>Control</u>	<u>Settings</u>
VOLTS/DIV	0.1
VARIABLE	CAL X1 (fully cw, pushed in)
POLARITY	NORM
Input Selector	DC
MODE	CH 1
TRIGGER	NORM

4. Set the Time Base triggering controls for negative SLOPE, LF REJECT COUPLING, and INT SOURCE.
5. Adjust the output of the square wave generator to give 4 divisions of vertical deflection.

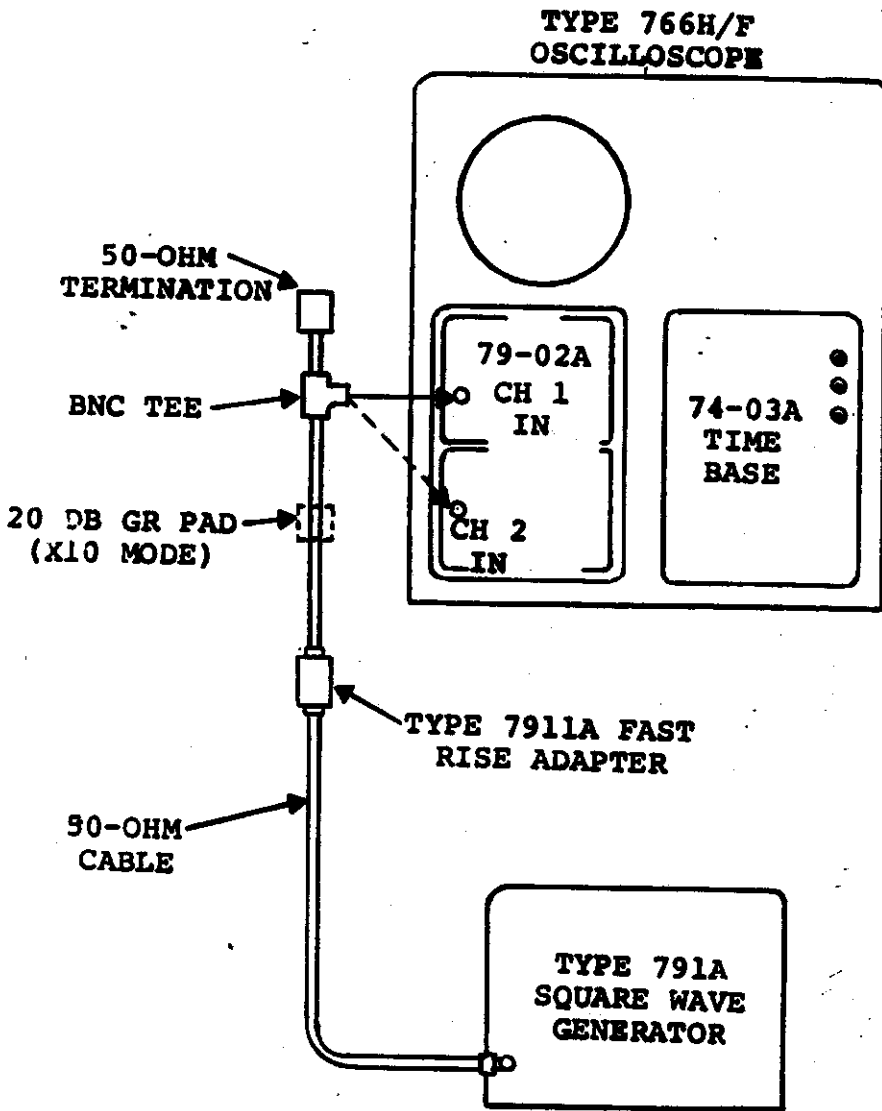


FIGURE 5-2. TEST SETUP FOR ADJUSTING HIGH FREQUENCY TRIMMERS

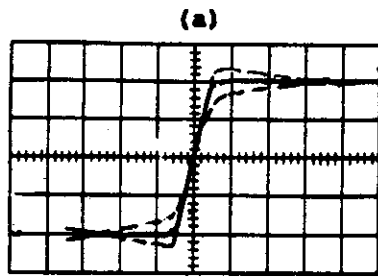
6. Adjust high-frequency trimmer C9804, the RC combination R9807 and C9806 and trimmers C9508, C9212 and C9512 for optimum flatness of the square wave. Capacitor C9804 and the RC combination R9806 and C9806 are adjusted for the long time constants, C9508 and C9212 for the overshoot and C9512 to smooth out the waveshape after initial over and undershoot. See Figures 5-3a and 5-3b for typical waveshapes and Figure 5-4 for location of high-frequency adjustment.

Note: Adjusting trimmer capacitor C9508 will create two peaks, one of which will give a cleaner top but slower rise time. Backing off from this setting will bring down the peak and speed the rise time until a point is reached where the peak again begins to rise and have a hint of a ring. This is the proper setting.

b. DELAY LINE TERMINATION R9511, C9501

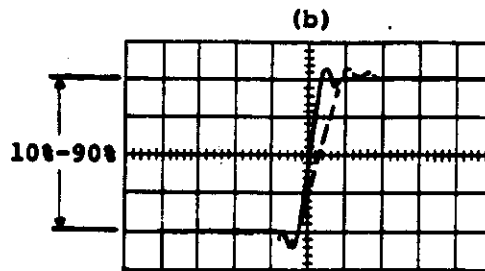
When the preceding adjustments in paragraph 5-15a have been made, a small step and bump may be noticed about 0.4 microseconds from the start of the pulse. The step may appear either above or below the top of the pulse after the termination bump and is due to misalignment of the delay line termination. To align the step and minimize the bump use the same test setup procedure described in paragraph 5-15a and proceed as follows:

1. Adjust the DELAY LINE ADJ control R9511 to reduce step until the trace is in line on each side of the termination bump. See Figure 5-3c.
2. Adjust the delay line trimmer capacitor C9501 to minimize termination bump. See Figure 5-3d.
3. Set the VOLTS/DIV switch to CAL and check gain calibration. Trim up with GAIN ADJ control if necessary.
4. Reset Channel 1 VOLTS/DIV switch to 0.1.
5. Readjust Channel 1 high-frequency trimmer C9804, the RC combination R9807 and C9806, and trimmer C9212 for optimum flatness of the square wave.
6. Disconnect the square wave generator from Channel 1 and connect it to the Channel 2 Input connector. See Figure 5-2.
7. Set MODE switch to Channel 2.
8. Adjust Channel 2 high-frequency trimmer C9904, the RC combination R9907 and C9906 and trimmer C9412 for optimum flatness of the square wave.



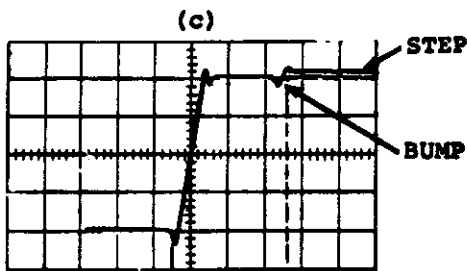
TIME CONSTANT ADJ

C9804 (C9904)
C9806, R9807
(C9906, R9907)



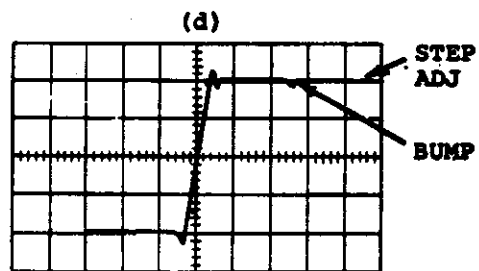
OVER & UNDERSHOOT ADJ

C9508
C9212 (C9412)
C9512

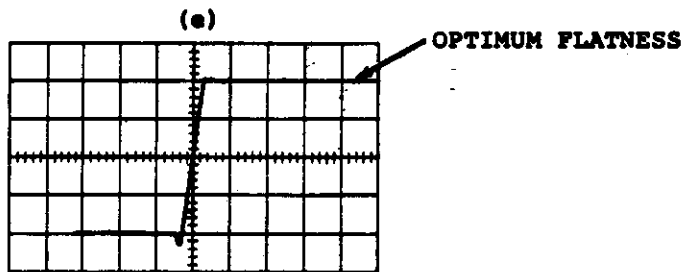


0.4
uSEC

STEP ADJ
R9511



DELAY LINE TERMINATION ADJ
C9501



CORRECTLY ADJUSTED
WAVEFORM

FIGURE 5-3. APPEARANCE OF WAVEFORM WHEN MAKING HIGH FREQUENCY ADJUSTMENTS

Note: Do not readjust trimmer capacitors C9508 and C9512 unless absolutely necessary. If re-adjustment is necessary, work back and forth between channels until the best compromise is reached. See Figure 5-3e.

c. CHANNELS 1 AND 2 AMPLIFIERS (X10 Operation)
C9210 (C9410), C9213 (C9413), C9214 (C9414)

Trimmer capacitors specified above are provided to improve the amplifier performance in the X10 range. To align the X10 amplifier proceed as follows:

1. Referring to the test setup shown in Figure 5-2, insert a 20 db General Radio pad between the output of the Type 7911A Generator and to CH 1 Input connector.
2. Pull out CH 1 VARIABLE knob for X10 operation, and set MODE switch to CH 1.
3. Adjust trimmer capacitor C9210 (C9410), C9213 (C9413), C9214 (C9414) for optimum flatness of the square wave.

Note: Trimmers C9213 (C9413) should be aligned in the same manner as C9508. See reference paragraph 5-15a, step 6 and the relevant note.

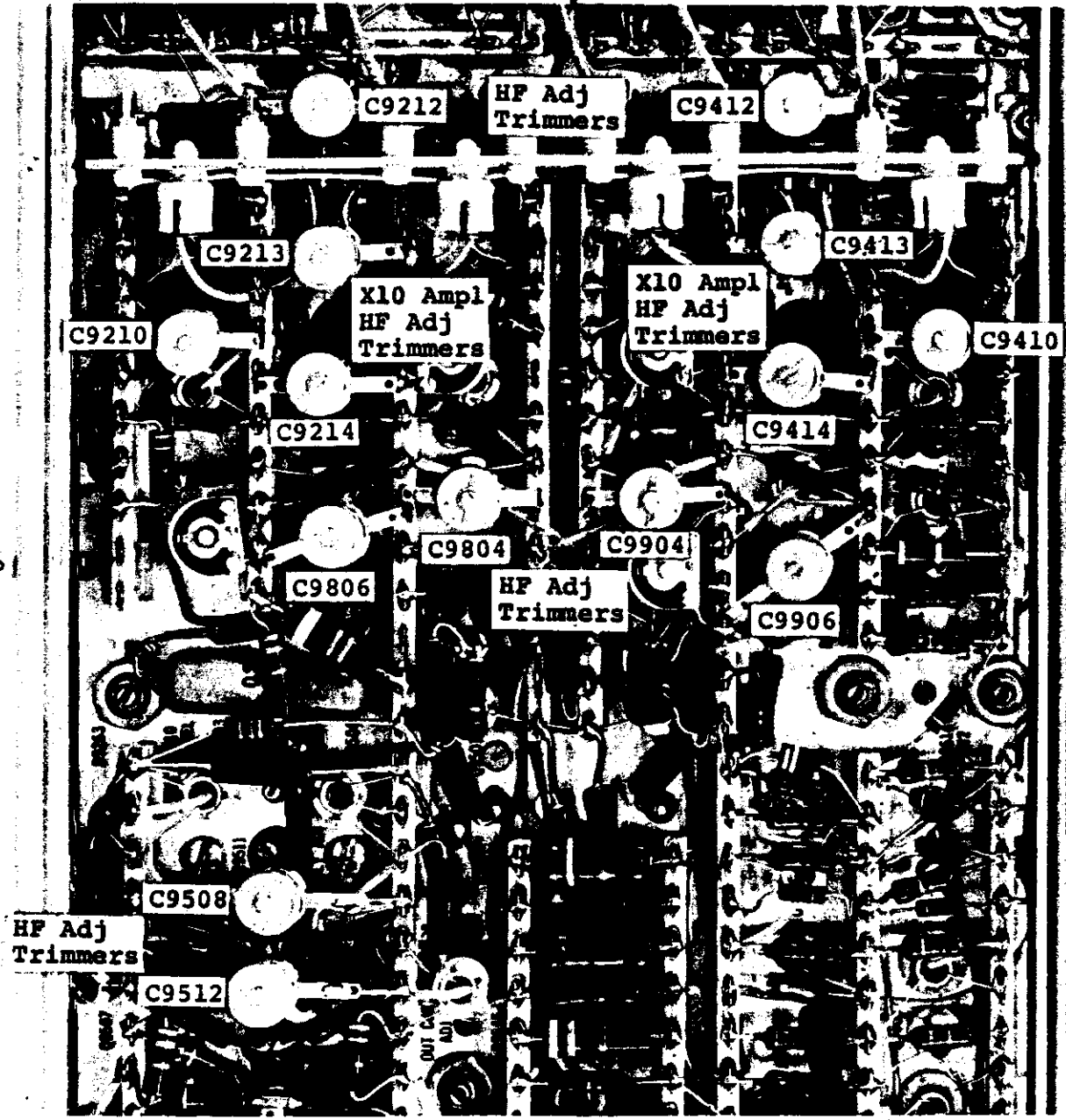
4. Check the rise time of the displayed waveshape at the 10% to 90% points. It should measure less than 3.8 nanoseconds in X1 mode and less than 4.2 nanoseconds in the X10 mode. The permissible overshoot and undershoot should be less than 0.15 divisions out of 4 divisions. The termination bump should be less than one trace width in amplitude.
5. Switch the generator to Channel 2 Input and set MODE switch to Channel 2. Repeat this procedure for Channel 2 using pertinent controls shown in ().

FRONT

CHANNEL 1

CHANNEL 2

TOP



REAR

FIGURE 5-4. LEFT SIDE VIEW SHOWING HF TRIMMERS

5-16. INPUT CAPACITANCE STANDARDIZATION AND ATTENUATOR ADJUSTMENT
(Figures 5-5 to 5-7)

The attenuators are factory aligned and should not be touched unless there is positive indication that they require adjustment. If adjustment is necessary, follow the steps as outlined making reference to Table 5-1. Reference symbols in () pertain to Channel 2.

The input capacitance standardization and attenuator adjustments are interdependent; therefore, both tests must be performed in the same procedure. The need for readjustment is normally indicated by distortion of fast-rising waveforms on one or more of the most sensitive ranges of this plug-in unit.

Standardization of the input capacitance of this Y plug-in unit requires the use of a 14-picofarad Capacitance Standardizer. To properly adjust the input capacitance and the attenuators of this plug-in unit, proceed as follows:

1. Connect a Capacitance Meter directly to Channel 1 Input BNC connector on the Type 79-02A Plug-in.
2. Set the VOLTS/DIV switch to 0.1 and the Input Selector switch to DC and the VARIABLE gain control fully ccw.
3. Adjust input capacity trimmer C9202 (C9402) for a meter reading of 14 pf; then disconnect meter.
4. Connect a Type 7012A Capacitance Standardizer to Channel 1 Input BNC on the Type 79-02A plug-in.
5. Apply the output from a Fairchild Type 791A Square Wave Generator through a RG-8A/U 50-ohm cable, through the Capacitance Standardizer to the Input BNC connector or the Type 79-02A. See hook-up shown in solid lines in Figure 5-5.
6. Set the Square Wave Generator to 5Kc and adjust the Time Base controls for a display of several cycles.
7. Adjust the Type 7012A Capacitance Standardizer for best flat top. See Figure 5-6 for proper waveshape and Figure 5-7 for location of trimmers.
8. Disconnect the Capacitance Standardizer from the test setup.

Note: Do not readjust the setting of the Standardizer, it will be used later in this procedure.

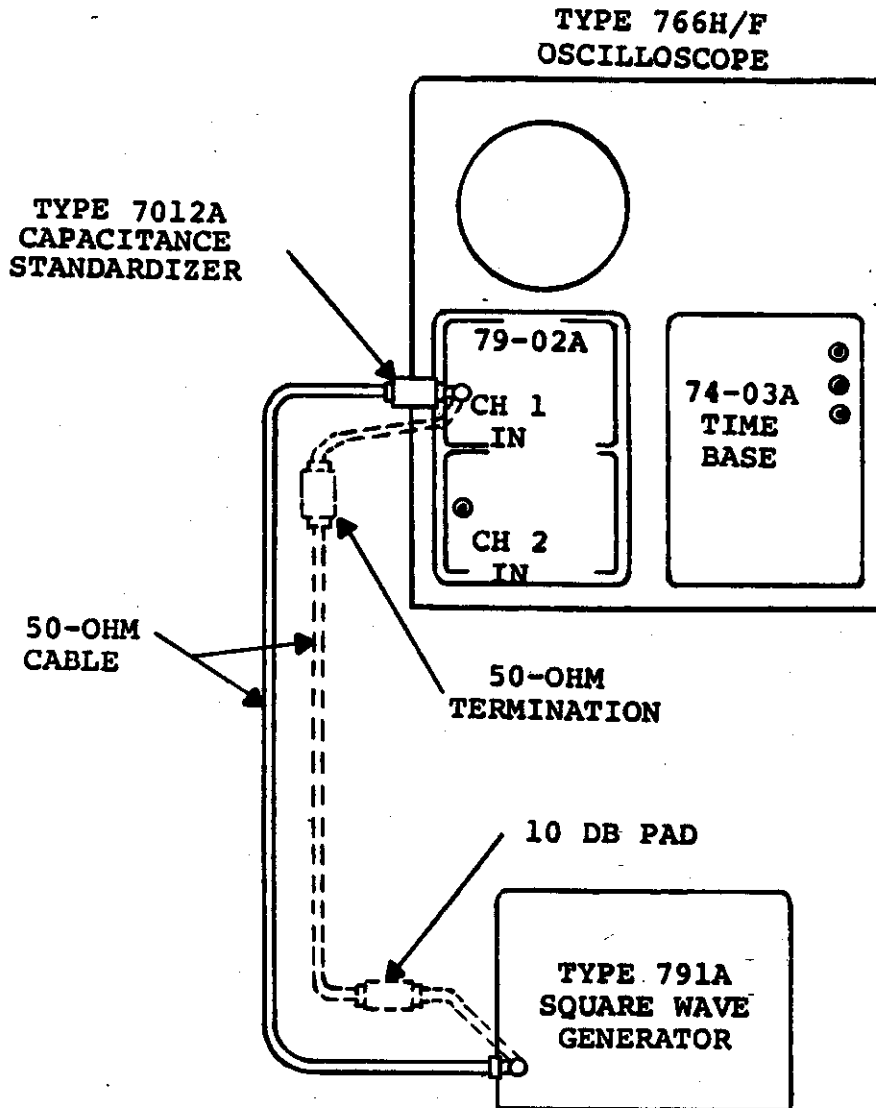
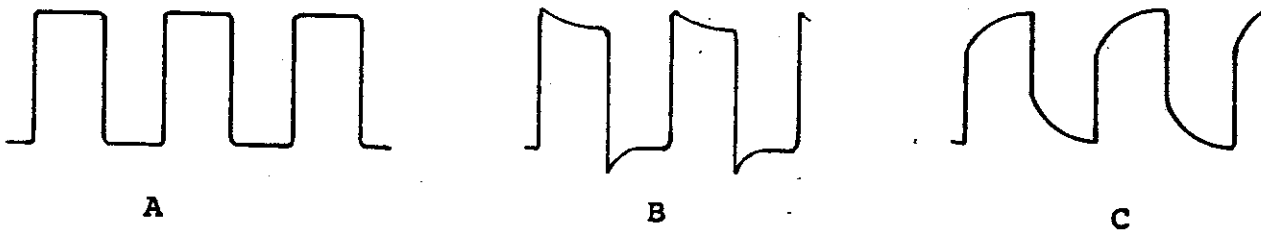


FIGURE 5-5. TEST SETUP FOR ADJUSTING INPUT CAPACITANCE AND VOLTS/DIV TRIMMERS

9. Apply the 5 Kc generator output through a General Radio 10 db pad and through a 50-ohm cable terminated in 50-ohms to the CH 1 Input connector on the Type 79-02A. See hook-up shown in dotted lines in Figure 5-5.
10. Set the VOLTS/DIV switch to 0.2 and the VARIABLE gain control to CAL. Adjust the generator to obtain 5 divisions of vertical deflection of the square wave pattern.
11. Adjust the attenuator frequency compensation trimmers indicated in Table 5-1 for maximum flatness of the positive peaks of the square wave.



A: Proper Adjustment
B, C: Improper Adjustment

FIGURE 5-6. STANDARDIZING THE INPUT CAPACITANCE

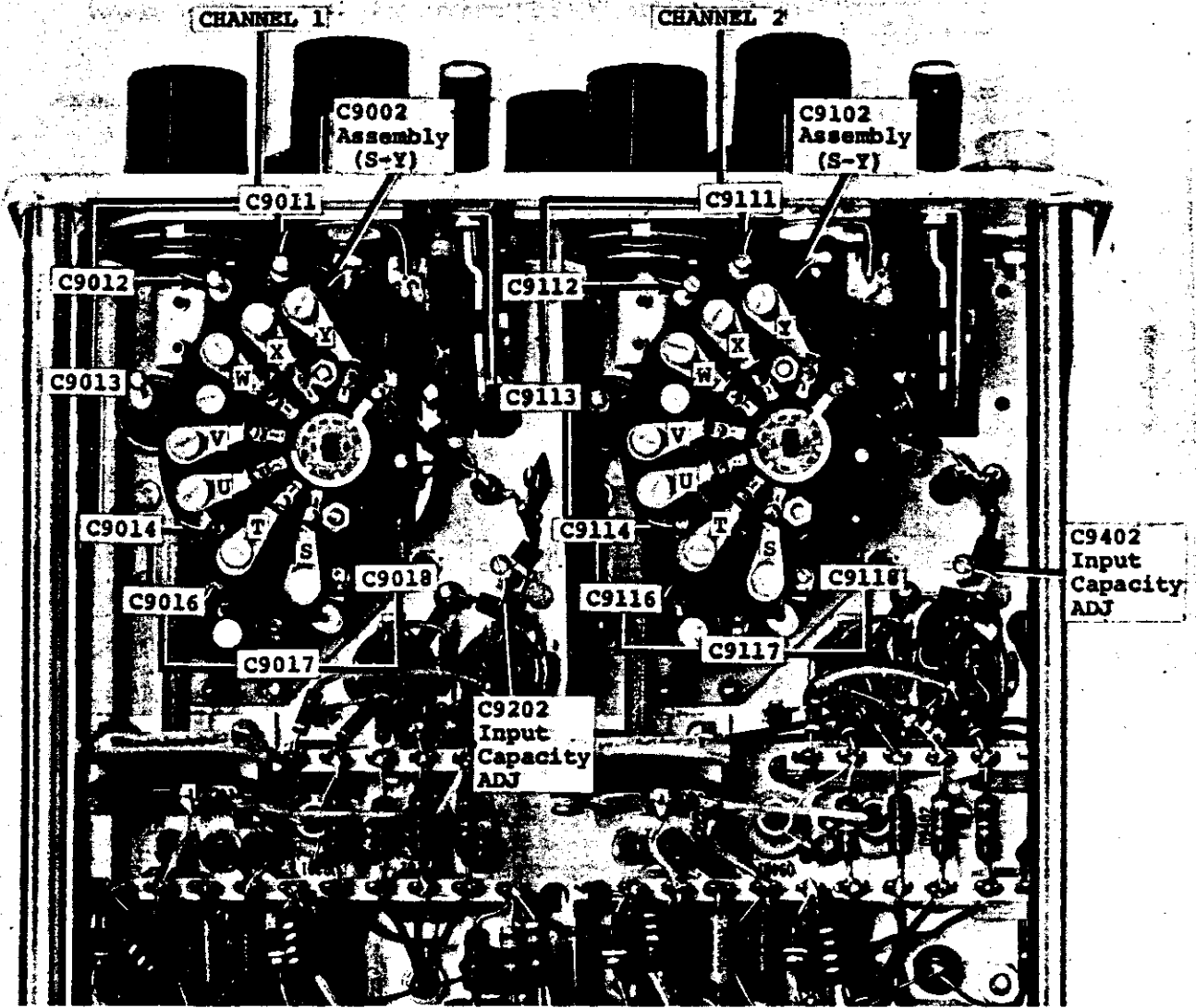


FIGURE 5-7. LEFT SIDE VIEW SHOWING CHANNEL 1 AND CHANNEL 2 ATTENUATOR ADJUSTMENTS

TABLE 5-1

ATTENUATOR COMPENSATION TRIMMERS

<u>VOLTS/DIV Setting</u>	<u>Trimmers</u>	<u>Location</u>
0.2	C9018 (C9118)	Figure 5-7
0.5	C9017 (C9117)	Figure 5-7
1.0	C9016 (C9116)	Figure 5-7
2.0	C9014 (C9114)	Figure 5-7
5.0	C9013 (C9113)	Figure 5-7
10	C9012 (C9112)*	Figure 5-7
20	C9011 (C9111)*	

*Note: If trimmers for the 10 and 20 VOLTS/DIV settings do not have sufficient range, dress resistors R9200 (R9400) 27 ohm and R9003 (R9103) 10 ohm away from each other.

() denotes CH 2.

Disconnect the 10 db pad and attenuator from the setup and reconnect the capacitance standardizer. See hook-up shown in solid lines in Figure 5-5. Continue adjustments given below:

<u>VOLTS/DIV Setting</u>	<u>Trimmers</u>	<u>Location (Figure 5-7)</u>
0.2	C9002 (C9102)	S
0.5	C9002 (C9102)	T
1	C9002 (C9102)	U
2	C9002 (C9102)	V
5	C9002 (C9102)	W
10	C9002 (C9102)	X
20	C9002 (C9102)	Y

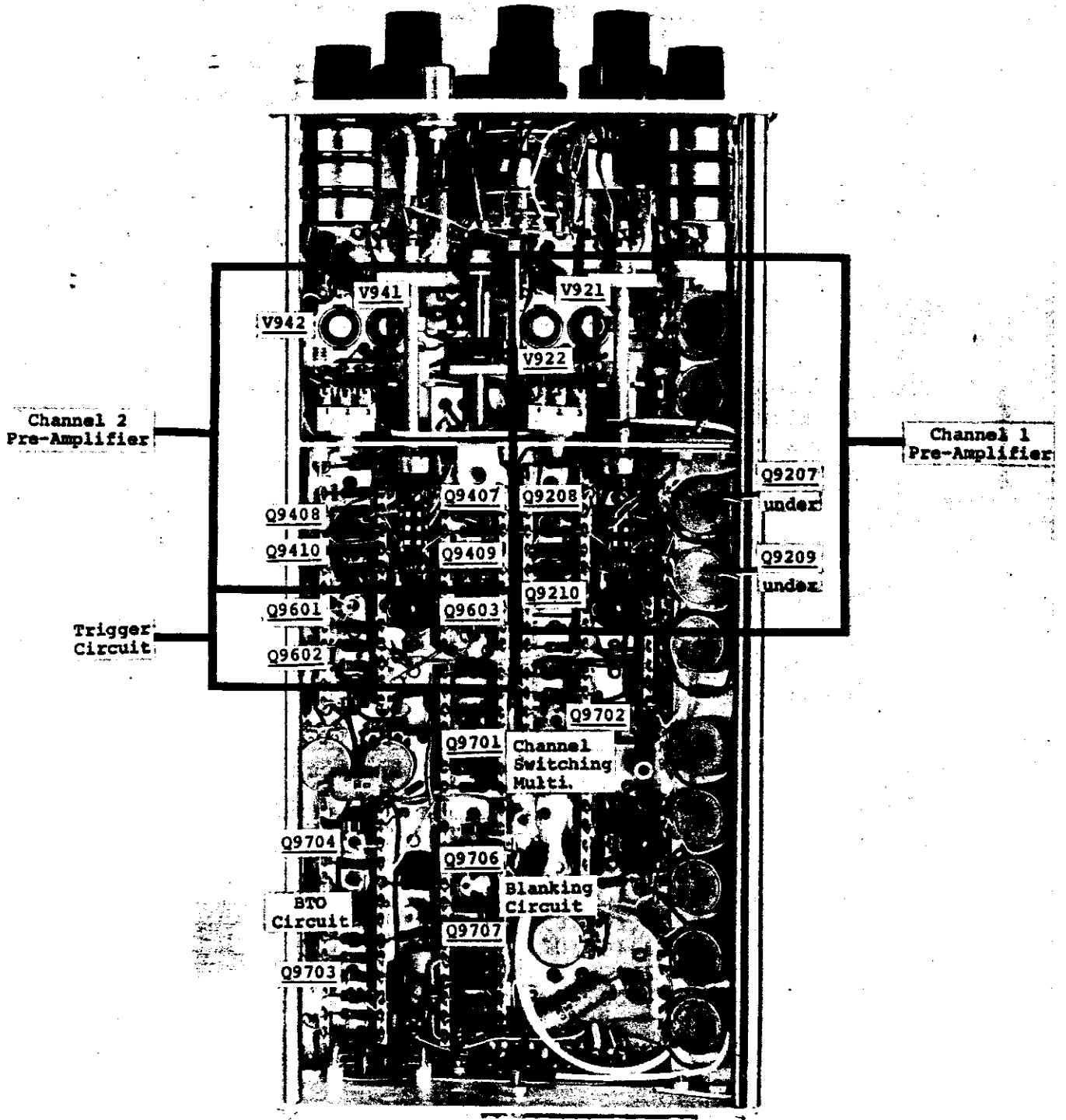


FIGURE 5-8. RIGHT SIDE VIEW SHOWING NUVISTORS AND TRANSISTORS

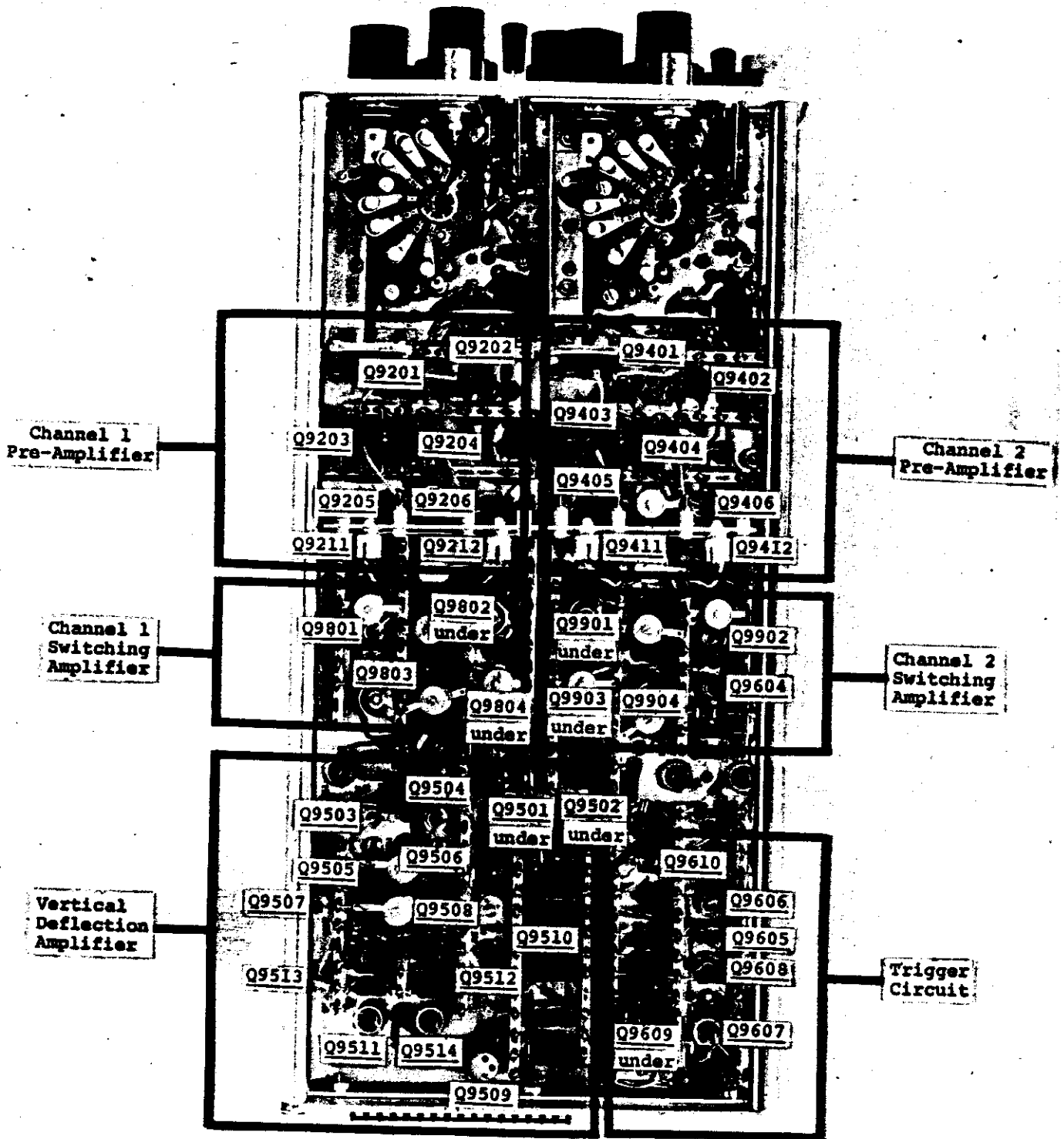
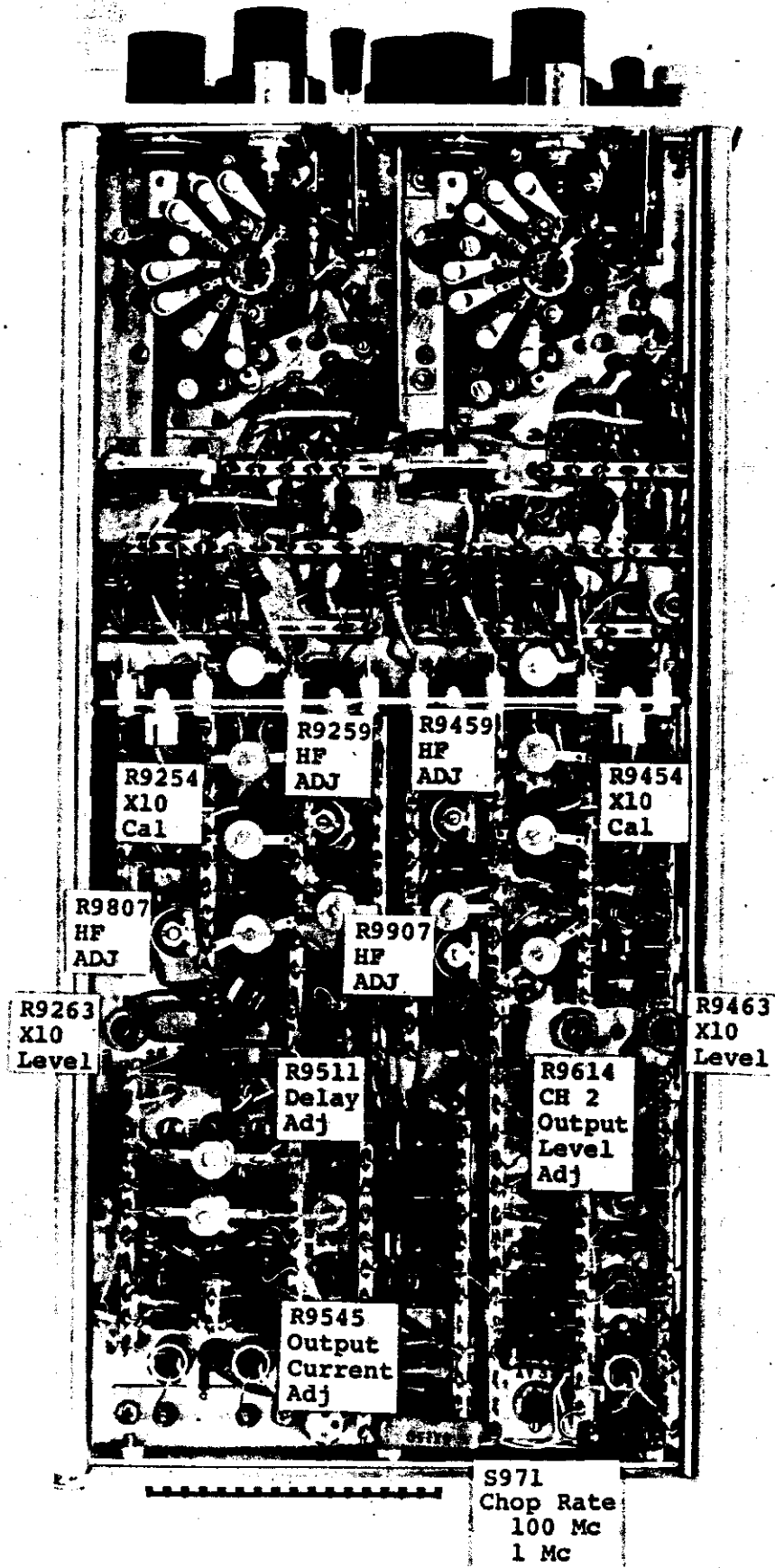


FIGURE 5-9. LEFT SIDE VIEW SHOWING TRANSISTORS



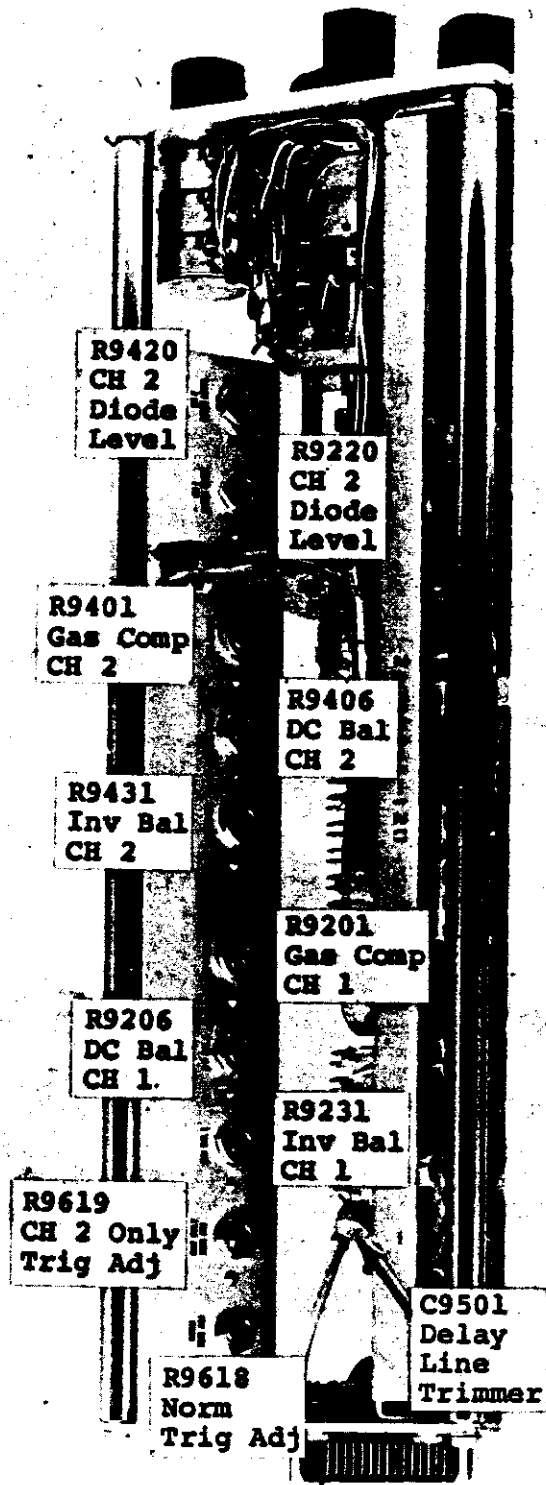
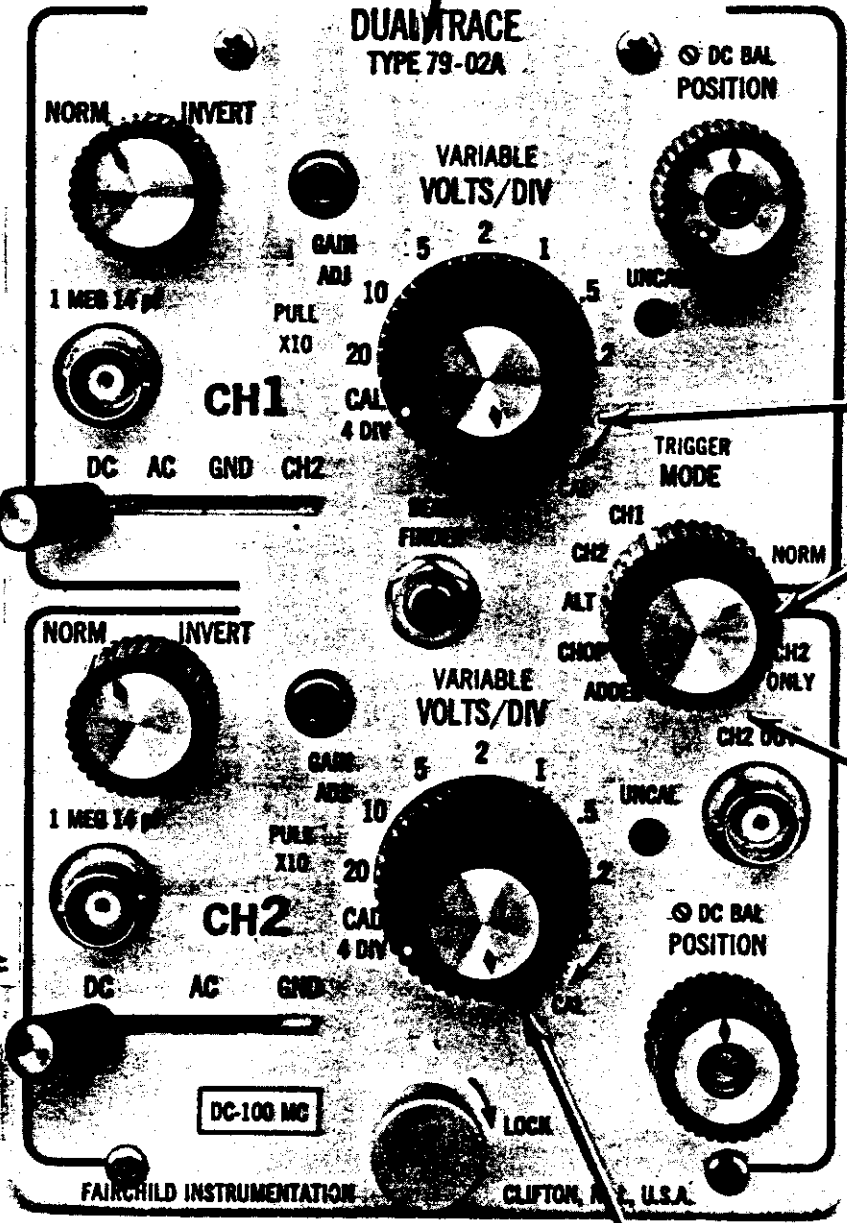


FIGURE 5-11. TOP VIEW SHOWING DELAY LINE TRIMMER AND POT ADJUSTMENTS.

PANEL:
Front
3201 3771



KNOB: (2)
Norm/Invert
4501 2022

KNOB: (2)
Position
4501 2024

KNOB: (2)
Volts/Div
4500 8945

BUSHING: (2)
4301 3581

KNOB:
Mode
4501 2035

CONNECTOR: (3)
BNC
Input & CH 2 Out

KNOB:
Trigger Mode
4501 2091

KNOB: (2)
Lever
4501 2202

KNOB:
Fastener
4501 0431

KNOB: (2)
Variable
4501 2021

FIGURE 6-1. FRONT PANEL REPLACEABLE PARTS

SECTION 6

ELECTRICAL PARTS LIST AND SCHEMATIC

<u>Symbol</u>	<u>Part Number</u>	<u>Description</u>	<u>Vendor</u>	
			<u>Code</u>	<u>Type</u>
CAPACITORS				
Notes:				
1. All capacitors are fixed, ceramic and 500V unless otherwise specified; pf denotes picofarads.				
2. GMV denotes Guaranteed Minimum Value.				
C9001	0327 2390	plastic, 0.0047 uf, <u>+10%</u> , 600V	GDE	663UW
C9002	3506 7032 3005 7832 3005 7842 3005 7852 6091 1731	assembly consisting of: plate, cap, adjust spring contact spring contact spring contact sc MSPH 4-40 x 1/4		
C9011 to C9013 C9014	0327 3920 0319 1071	variable, 0.2-1.5 pf, 600V variable, plastic, 0.65-3.5 pf	ERC ABD	570-000
C9016 to C9018	0319 1071	variable, plastic, 0.65-3.5 pf	ABD	
C9019	0313 9750	mica, 250 pf, <u>+10%</u>	ERC	654-006
C9021	0326 3060	mica, 130 pf, <u>+10%</u>	ERC	654-006
C9022	0313 9720	mica, 50 pf, <u>+10%</u>	ERC	654-006
C9023	0327 4020	10 pf	ERC	301
C9024	0327 4010	8.2 pf	ERC	301
C9101	0327 2390	plastic, 0.0047 uf, <u>+10%</u> , 600V	GDE	663UW
C9102	3506 7032 3005 7832 3005 7842 3005 7852 6091 1731	assembly consisting of: plate, cap, adjust spring contact spring contact spring contact sc, MSPH, 4-40 x 1/4		
C9111 to C9113 C9114	0327 3920 0319 1071	variable, 0.2-1.5 pf, 600V variable, plastic, 0.65-3.5 pf	ERC ABD	570-000
C9116 to C9118	0319 1071	variable, plastic, 0.65-3.5 pf	ABD	
C9119	0313 9750	mica, 250 pf, <u>+10%</u>	ERC	654-006
9121	0326 3060	mica, 130 pf, <u>+10%</u>	ERC	654-006
C9122	0313 9720	mica, 50 pf, <u>+10%</u>	ERC	654-006

<u>Symbol</u>	<u>Part Number</u>	<u>Description</u>	<u>Vendor</u>	
			<u>Code</u>	<u>Type</u>
<u>CAPACITORS (Continued)</u>				
C9123	0327 4020	10 pf	ERC	301
C9124	0327 4010	8.2 pf	ERC	301
C9201	0310 1270	1000 pf, 1000V	RMC	B
C9202	0327 3920	variable, 0.2-1.5 pf, 600V	ERC	570-000
C9203	0319 1060	0.01 uf, 150V	CPG	DDM
C9204	0319 0450	1000 pf	SPG	505C1A1
C9205	0316 7180	3.9 pf	ERC	NPO331
C9206	0319 1060	0.01 uf, 150V	CPC	DDM
C9207	0316 7180	3.9 pf	ERC	NPO331
C9208	0319 0450	1000 pf	SPG	505C1A1
C9210	0326 9490	variable, 2-8 pf, 200V	ERC	538
C9211	0319 0450	1000 pf	SPG	505C1A1
C9212	0326 9490	variable, 2-8 pf, 200V	ERC	538
C9213 to C9214	0326 9480	variable, 9-35 pf, 100V	ERC	538
C9215	0316 7240	6.8 pf	ERC	NPO331
C9216	0326 4520	1000 pf, GMV	ERC	831
C9217 to C9218	0319 0450	1000 pf	SPG	505C1A1
C9219	0316 7410	22 pf, <u>+5%</u>	ERC	NPO331
C9221 to C9223	0326 7880	plastic, 0.22 uf, <u>+10%</u> , 200V	AMX	C296AB
C9224	0319 2420	composition, 1.5 pf, <u>+5%</u>	STC	GA
C9226	0319 2420	composition, 1.5 pf, <u>+5%</u>	STC	GA
C9281	0326 4550	2000 pf, GMV	ERC	841
C9301	0326 4520	1000 pf, GMV	ERC	831
C9302	0326 7860	plastic, 0.1 uf, <u>+10%</u> , 200V	AMX	C296AB
C9303 to C9304	0326 4520	1000 pf, GMV	ERC	831
C9306 to C9307	0326 4520	1000 pf, GMV	ERC	831
C9308	0326 7880	plastic, 0.22 uf, <u>+10%</u> , 200V	AMX	C296AB
C9401	0310 1270	1000 pf, 1000V	RMC	B
C9402	0327 3920	variable, 0.2-1.5 pf, 600V	ERC	570-000

<u>Symbol</u>	<u>Part No.</u>	<u>Description</u>	<u>Vendor</u>	
			<u>Code</u>	<u>Type</u>
<u>CAPACITORS (Cont.)</u>				
C9403	0319 1060	0.01 μ f, 150V	CPC	DDM
C9404	0319 0450	1000 pf	SPG	505C1A1
C9405	0316 7180	3.9 pf	ERC	NPO331
C9406	0319 1060	0.01 μ f, 150V	CPC	DDM
C9407	0316 7180	3.9 pf	ERC	NPO331
C9408	0319 0450	1000 pf	SPG	505C1A1
C				
C9410	0326 9490	Variable, 2-8 pf, 200V	ERC	538
C9411	0319 0450	1000 pf	ERC	538
C9412	0326 9490	Variable, 2-8 pf, 200V	ERC	538
C9413 to C9414	0326 9480	Variable, 9-35 pf, 100V	ERC	538
C9415	0316 7240	6.8 pf	ERC	NPO331
C9416	0326 4520	1000 pf, GMV	ERC	831
C9417 to C9418	0319 0450	1000 pf	SPG	505C1A1
C9419	0316 7410	22 pf, \pm 5%	ERC	NPO331
C9424	0319 2420	Composition, 1.5 pf, \pm 5%	STC	GA
C9426	0319 2420	Composition, 1.5 pf, \pm 5%	STC	GA
C9481	0326 4550	2000 pf, GMV	ERC	841
C9500	0316 7110	2.2 pf	ERC	NPO331
C9501	0326 9490	Variable, 2-8 pf, 200V	ERC	538
C9502 to C9503	0316 7290	1.5 pf	ERC	NPO331
C9504	0319 0450	1000 pf	SPG	50C1A1
C9505	0316 7110	2.2 pf	ERC	NPO331
C9506	0326 4500	470 pf	ERC	831
C9507	0319 0450	1000 pf	SPG	505C1A1
C9508	0326 9480	Variable, 9-35 pf, 100V	ERC	538
C9509	0319 0450	1000 pf	SPG	505C1A1
C9510	0319 1050	0.2 μ f, 150V	CRL	DDM
C9511	0319 0450	1000 pf	SPG	505C1A1

<u>Symbol</u>	<u>Part Number</u>	<u>Description</u>	<u>Vendor</u>	
			<u>Code</u>	<u>Type</u>
<u>CAPACITORS (Continued)</u>				
C9512	0326 9490	variable, 2-8 pf, 200V	ERC	538
C9513	0319 1060	0.01 uf, 150V	CPC	DDM
C9514 to C9515	0319 0450	1000 pf	SPG	505C1A1
C9516	0316 7460	33 pf, +5%	ERC	
C9517	0317 3310	100 pf, +10%	CPC	
C9518	0319 2380	composition, 0.68 pf, +5%	STC	GA
C9519	0326 4520	1000 pf, GMV	ERC	831
C9600	0316 0350	47 pf, +5%	EIA	
C9601	0316 7410	22 pf, +5%	ERC	NPO331
C9602	0319 1050	0.02 uf, 150V	CPC	DDM
C9603	0316 7410	22 pf, +5%	ERC	NPO331
C9604	0317 4010	750 pf, +10%	EIA	
C9605 to C9606	0326 4520	1000 pf, GMV	ERC	831
C9607	0319 1050	0.02 uf, 150V	CPC	DDM
C9608	0326 4520	1000 pf, GMV	ERC	831
C9609	0326 8520	680 pf, +10%, 1000V	RMC	JF
C9610	0316 0360	51 pf, +5%	EIA	
C9611	0316 7350	12 pf, +5%	ERC	NPO331
C9612	0319 1050	0.02 uf, 150V	CPC	DDM
C9613	0326 4550	2000 pf, GMV	ERC	831
C9614	0313 3850	composition, 1.5 pf, +10%	STC	GA
C9615*	0315 2100	10 pf, +10%	ERC	NPO331
C9616	0316 7390	18 pf, +5%	ERC	NPO331
C9617	0316 7450	30 pf, +5%	ERC	NPO331
C9700	0316 0360	51 pf, +5%	EIA	
C9701	0315 1530	33 pf	ERC	NPO338
C9702	0316 7410	22 pf	ERC	NPO331
C9703	0326 4520	1000 pf, GMV	ERC	831
C9704	0316 7410	22 pf	ERC	NPO331
C9705	0326 7860	plastic, 0.1 uf, 200V	AMX	C296AB
C9706	0315 1530	33 pf	ERC	NPO338
C9707 to C9708	0319 1060	0.01 uf, 150V	CPC	DDM
C9709	0326 7860	plastic, 0.1 uf, +10%, 200V	AMX	C206AB
C9710	0319 1060	0.01 uf, 150V	CPC	DDM
C9711	0317 3310	100 pf, +10%	CPC	
C9712	0326 7860	plastic, 0.1 uf, 200V	AMX	C296AB
C9713	0327 4580	3000 pf	ERC	
C9714	0317 3820	220 pf, +10%	EIA	
C9715	0319 1060	0.01 uf, 150V	CPC	DDM

*TEST OPTION

<u>Symbol</u>	<u>Part No.</u>	<u>Description</u>	<u>Vendor</u>	
			<u>Code</u>	<u>Type</u>
<u>CAPACITORS (Cont.)</u>				
C9716	0316 7280	10 pf	ERC	NPO331
C9717	0319 1050	0.02 μ f, 150V	CPC	DDM
C9718	0319 1060	0.01 μ f, 150V	CPC	DDM
C9719	0326 7860	Plastic, 0.1 μ f, 200V	AMX	C296AB
C9721	0326 4520	1000 pf, GMV	ERC	831
C9801	0316 7410	22 pf, +5%	ERC	NOP331
C9802	0319 0450	1000 pf	SPG	505C1A1
C9804	0326 9490	Variable, 2-8 pf, 200V	ERC	538
C9805	0319 2420*	Composition, 1.5 pf, \pm 5%	STC	GA
C9805	0319 2480*	Composition, 2.7 pf, \pm 5%	STC	GA
C9806	0326 9490	Variable, 2-8 pf, 200V	ERC	538
C9901	0316 7410	22 pf, \pm 5%	ERC	NPO331
C9902	0319 0450	1000 pf	SPG	505C1A1
C9904	0326 9490	Variable, 2-8 pf, 200V	ERC	538
C9905	0319 2420*	Composition, 1.5 pf, \pm 5%	STC	GA
C9905	0319 2480	Composition, 2.7 pf, \pm 5%	STC	GA
C9906	0326 9490	Variable, 2-8 pf, 200V	ERC	538
C9907	0313 3580**	Composition, 2 pf, +5%	JEF	JM5/32

SEMI-CONDUCTORS

CR9221	2600 6910	Diode, FD841	FCI	
CR9222 & CR9223	2600 3041	Diode, IN830 (CR9222 & CR9223 Matched Pair)	ABD	
CR9224 & CR9225	2600 3041	Diode, IN830 (CR9224 & CR9225 Matched Pair)	ABD	
CR9421	2600 6910	Diode, FD841	FCI	
CR9422 & CR9423	2600 3041	Diode, IN830 (CR9422 & CR9423 Matched Pair)	ABD	
CR9424 & CR9425	2600 3041	Diode, IN830 (CR9424 & CR9425 Matched Pair)	ABD	

*Selected by Test Dept.
**Test Option

<u>Symbol</u>	<u>Part Number</u>	<u>Description</u>	<u>Vendor</u>	
			<u>Code</u>	<u>Type</u>
<u>SEMI-CONDUCTORS (Concluded)</u>				
CR9501	2600 6990	diode, 1N752	HOF	
CR9601 to CR9604	2600 6910	diode, FD841	FCI	
CR9605	2600 8910	diode, 1N756A	FCI	
CR9700 to CR9706	2600 6910	diode, FD841	FCI	
CR9801 to CR9803	2600 6910	diode, FD841	FCI	
CR9901 to CR9903	2600 6910	diode, FD841	FCI	
<u>DELAY LINE</u>				
DL9501	8800 2401	delay line	ABD	
<u>LAMPS</u>				
DS9201	1200 3960	glow neon (UNCAL)	GE	NE2
DS9401	1200 3960	glow neon (UNCAL)	GE	NE2
<u>HYBRID COILS</u>				
HY9000 to HY9002	2110 1560	bead ferroxcube	FER	
HY9003 to HY9004	2110 1590	bead ferroxcube	FER	
HY9005 to HY9010	2110 1560	bead ferroxcube	FER	
HY9100 to HY9102	2110 1560	bead ferroxcube	FER	
HY9105	2110 1560	bead ferroxcube	FER	
HY9200 to HY9204	2110 1560	bead ferroxcube	FER	
HY9206 to HY9209	2110 1560	bead ferroxcube	FER	
HY9211 to HY9212	2110 1560	bead ferroxcube	FER	
HY9301 to HY9302	2110 1560	bead ferroxcube	FER	
HY9303 to HY9304	2110 1590	bead ferroxcube	FER	
HY9306	2110 1590	bead ferroxcube	FER	
HY9400 to HY9404	2110 1560	bead ferroxcube	FER	
HY9407 to HY9409	2110 1560	bead ferroxcube	FER	
HY9411 to HY9412	2110 1560	bead ferroxcube	FER	
HY9413 to HY9414	2110 1590	bead ferroxcube	FER	
HY9416 to HY9419	2110 1590	bead ferroxcube	FER	
HY9511 to HY9512	2110 1590	bead ferroxcube	FER	
HY9501 to HY9505	2110 1560	bead ferroxcube	FER	
HY9506 to HY9509	2110 1590	bead ferroxcube	FER	
HY9600	2110 1590	bead ferroxcube	FER	

<u>Symbol</u>	<u>Part Number</u>	<u>Description</u>	<u>Vendor</u>	
			<u>Code</u>	<u>Type</u>
<u>HYBRID COILS (Concluded)</u>				
HY9601 to HY9604	2110 1560	bead ferroxcube	FER	
HY9606 to HY9607	2110 1590	bead ferroxcube	FER	
HY9701 to HY9703	2110 1560	bead ferroxcube	FER	
<u>ELECTRICAL CONNECTORS</u>				
J9001	0904 4541	connector, MODIFIED (CH 1)	CAN	
J9101	0904 4541	connector, MODIFIED (CH 2)	CAN	
J9601	0905 9940	receptacle, BNC, rf, female, 1 contact (CH 2 OUT)	CAN	
P9001	0905 7340	plug, general purpose, male, 32 contacts	APH	26 159 32
<u>COILS</u>				
L9701	2110 1820	RF, F, 39 UH +5%	SWW	43901
<u>TRANSISTORS</u>				
Q9201 to Q9204	2600 3084 2600 7700	DU#12A (Selected) DU#12A	FI	
Q9205 to Q9208	2600 3071 2600 8190	DU#14A (Selected) DU#14A	FI	
Q9209 to Q9210	2600 3084 2600 7700	DU#12A (Selected) DU#12A	FI	
Q9211 to Q9212	2600 8690 2600 8680	DU#30 alternate, 2N2894	FCI	
Q9401 to Q9404	2600 3084 2600 7700	DU#12A (Selected) DU#12A	FI	
Q9405 to Q9408	2600 3071 2600 8190	DU#14A (Selected) DU#14A	FI	
Q9409 to Q9410	2600 3084 2600 7700	DU#12A (Selected) DU#12A	FI	
Q9411 to Q9412	2600 8690 2600 8680	DU#30 alternate, 2N2894	FCI	
Q9501 to Q9508	2600 3071 2600 8190	DU#14A (Selected) DU#14A	FI	

<u>Symbol</u>	<u>Part Number</u>	<u>Description</u>	<u>Vendor</u>	
			<u>Code</u>	<u>Type</u>
TRANSISTORS (Continued)				
Q9509	2600 7270 2600 7250	DU#6A alternate, 2N1893	FCI	
Q9510	2600 8500	2N2218	FCI	
Q9511	2600 2791	2N2218	ABD	
Q9512 to Q9513	2600 8400 2600 8390	DU#28 alternate, 2N3013	FCI	
Q9514	2600 2791	2N2218	ABD	
Q9601	2600 7070 2600 7050	DU#2A alternate, 2N915	FCI	
Q9602	2600 8580 2600 8560	DU#37A alternate, 2N3072	FCI	
Q9603 to Q9605	2600 3071 2600 8190	DU#14A (Selected) DU#14A	FI	
Q9606	2600 7420 2600 7400	DU#9A alternate, 2N869	FCI	
Q9607	2600 7460 2600 7450	DU#10 alternate, 2N1711	FCI	
Q9608	2600 7420 2600 7400	DU#9A alternate, 2N869	FCI	
Q9609 to Q9610	2600 3071 2600 8190	DU#14A (Selected) DU#14A	FI	
Q9701 to Q9702	2600 3071 2600 8190	DU#14A (Selected) DU#14A	FI	
Q9703	2600 7070 2600 7050	DU#2A alternate, 2N915	FCI	
Q9704	2600 3071 2600 8190	DU#14A (Selected) DU#14A	FI	
Q9706	2600 8570 2600 8560	DU#37 alternate, 2N3072	FCI	

<u>Symbol</u>	<u>Part Number</u>	<u>Description</u>	<u>Vendor</u>	
			<u>Code</u>	<u>Type</u>
<u>TRANSISTORS (Concluded)</u>				
Q9707	2600 7070 2600 7050	DU#2A alternate, 2N915	FCI	
Q9801 to Q9804	2600 3071 2600 8190	DU#14A (Selected) DU#14A	FI	
Q9901 to Q9904	2600 3071 2600 8190	DU#14A (Selected) DU#14A	FI	

RESISTORS

Note: All resistors are fixed, film, +5%, and 1/2W. Values are in ohms unless otherwise specified. K = thousand, M = million.

R9001	0235 4460	composition, 220, 1/4W	ALB	CB
R9003	0235 4140	composition, 10, 1/4W	ALB	CB
R9004	0235 4340	composition, 68, 1/4W	ALB	CB
R9006	0236 7840	178K, +1%	CGW	NS20
R9007	0236 7940	226K, +1%	CGW	NS20
R9008	0237 5660	995K, +1%, 1/8W	TEX	CD1/8R
R9009	0237 5540	5.03K, +1%, 1/8W	TEX	CD1/8R
R9011	0237 5650	990K, +1%, 1/8W	TEX	CD1/8R
R9012	0237 5550	10.1K, +1%, 1/8W	TEX	CD1/8R
R9013	0237 5640	980K, +1%, 1/8W	TEX	CD1/8R
R9014	0237 5560	20.4K, +1%, 1/8W	TEX	CD1/8R
R9016	0237 5630	950K, +1%, 1/8W	TEX	CD1/8R
R9017	0237 5570	52.6K, +1%, 1/8W	TEX	CD1/8R
R9018	0237 5620	900K, +1%, 1/8W	TEX	CD1/8R
R9019	0237 5580	111K, +1%, 1/8W	TEX	CD1/8R
R9021	0237 5610	800K, +1%, 1/8W	TEX	CD1/8R
R9022	0237 5590	250K, +1%, 1/8W	TEX	CD1/8R
R9023	0237 5600	500K, +1%, 1/8W	TEX	CD1/8R
R9024	0237 5670	1M, +1%, 1/8W	TEX	CD1/8R
R9101	0235 4460	composition, 220, 1/4W	ALB	CB
R9102	0234 8010	150	CGW	C20
R9103	0235 4140	composition, 10, 1/4W	ALB	CB

<u>Symbol</u>	<u>Part No.</u>	<u>Description</u>	<u>Vendor</u>	
			<u>Code</u>	<u>Type</u>
<u>RESISTORS (Cont.)</u>				
R9104	0235 4340	Composition, 68, 1/4W	ALB	CB
R9106	0236 7840	178K, $\pm 1\%$	CGW	NS20
R9107	0236 7940	226K, $\pm 1\%$	CGW	NS20
R9108	0237 5660	995K, $\pm 1\%$, 1/8W	TEX	CD1/8R
R9109	0237 5540	5.03K, $\pm 1\%$, 1/8W	TEX	CD1/8R
R9111	0237 5650	990K, $\pm 1\%$, 1/8W	TEX	CD1/8R
R9112	0237 5550	10.1K, $\pm 1\%$, 1/8W	TEX	CD1/8R
R9113	0237 5640	980K, $\pm 1\%$, 1/8W	TEX	CD1/8R
R9114	0237 5560	20.4K, $\pm 1\%$, 1/8W	TEX	CD1/8R
R9116	0237 5630	950K, $\pm 1\%$, 1/8W	TEX	CD1/8R
R9117	0237 5570	52.6K, $\pm 1\%$, 1/8W	TEX	CD1/8R
R9118	0237 5620	900K, $\pm 1\%$, 1/8W	TEX	CD1/8R
R9119	0237 5580	111K, $\pm 1\%$, 1/8W	TEX	CD1/8R
R9121	0237 5610	800K, $\pm 1\%$, 1/8W	TEX	CD1/8R
R9122	0237 5590	250K, $\pm 1\%$, 1/8W	TEX	CD1/8R
R9123	0237 5600	500K, $\pm 1\%$, 1/8W	TEX	CD1/8R
R9124	0237 5670	1M, $\pm 1\%$, 1/8W	TEX	CD1/8R
R9200	0235 4240	Composition, 27, 1/4W	ALB	CB
R9201	0107 5960	Variable, composition, 100K, $\pm 20\%$ (GAS COMP)	CTS	65
R9202	0234 8690	100K	CGW	C20
R9203	0237 5670	1M, $\pm 1\%$, 1/8W	TEX	CD1/8R
R9204	0234 7970	100,	CGW	C20
R9206	0107 5960	Variable, composition, 1/4W 100K, $\pm 20\%$ (COARSE DC BAL)	CTS	65
R9207	0107 2952	Variable, 100K/ 100K/ 100K, $\pm 20\%$, (DC BAL/POSITION)	ABD	
R9208	0235 5180	Composition, 240K, 1/4W	ALB	CB
R9209	0203 1170	Composition, 750K,	ALB	EB
R9211	0203 1300	Composition, 2.7M	ALB	EB
R9212	0234 8520	20K,	CGW	C20
R9213	0235 4300	Composition, 47, 1/4W	ALB	CB

<u>Symbol</u>	<u>Part No.</u>	<u>Description</u>	<u>Vendor</u>	
			<u>Code</u>	<u>Type</u>
<u>RESISTORS (Cont.)</u>				
R9214	0203 0100	Composition, 27	ALB	EB
R9216	0235 4380	Composition, 100, 1/4W	ALB	CB
R9217	0235 2350	3.9K, $\pm 2\%$, 1W	CGW	C32
R9218	0235 4300	Composition, 47, 1/4W	ALB	CB
R9219	0235 4240	Composition, 27, 1/4W	ALB	CB
R9226	0234 8340	3.6K	CGW	C20
R9221	0235 4240	Composition, 27, 1/4W	ALB	CB
R9222	0235 4300	Composition, 47, 1/4W	ALB	CB
R9223 & R9224	0235 0670	3K, $\pm 2\%$	CGW	C20
R9225	0235 0730	5.1K, $\pm 2\%$	CGW	C20
R9220	0107 5930	Variable, composition, 3K, $\pm 20\%$ (BRIDGE BAL)	CTS	65
R9227	0109 3620	Variable, composition, 5K, $\pm 20\%$, 1/4W (GAIN ADJ)	CTS	200
R9228	0107 3041	Variable, composition, 10K, $\pm 20\%$, 1/8W (VARIABLE)	ABD	
R9229	0234 8730	150K	CGW	C20
R9230	0234 8560	30K	CGW	C20
R9231	0107 5950	Variable, composition, 50K, $\pm 20\%$, (BAL INVERT)	CTS	65
R9232	0236 5490	634, $\pm 1\%$	CGW	NS20
R9233	0234 8560	30K,	CGW	C20
R9234	0236 5490	634, $\pm 1\%$	CGW	NS20
R9235	0235 4300	Composition, 47, 1/4W	ALB	CB
R9236 & R9237	0236 4890	150, $\pm 1\%$	CGW	NS20
R9238	0234 8040	200,	CGW	C20
R9239	0237 8550	1.33K, $\pm 1\%$, 1W	IRC	CES
R9240	0235 4300	Composition, 47, 1/4W	ALB	CB
R9241	0203 0120	Composition, 33	ALB	EB
R9242 & R9243	0234 8150	560,	CGW	C20
R9244	0234 8450	10K,	CGW	C20
R9246	0234 8450	10K,	CGW	C20
R9247 & R9248	0235 0840	15K, $\pm 2\%$	CGW	C20
R9249	0235 0480	470, $\pm 2\%$	CGW	C20
R9251	0235 0480	470, $\pm 2\%$	CGW	C20

<u>Symbol</u>	<u>Part No.</u>	<u>Description</u>	<u>Vendor</u>	
			<u>Code</u>	<u>Type</u>
<u>RESISTORS (Cont.)</u>				
R9252 & R9253 R9254	0236 6400 0107 2658	5.62K, $\pm 1\%$ Variable, 250, $\pm 20\%$, 1/4W (X10 CAL CH 1)	CGW ABD	NS20 NS20
R9256 & R9257 R9258 R9259	0236 6500 0236 6400 0109 3970	7.15K, $\pm 1\%$ 5.62K, $\pm 1\%$ Variable, composition, 500, 1/10W (HF ADJ)	CGW CGW CRL	NS20 NS20 601-1
R9261 R9262 R9263	0236 6400 0203 0120 0107 5920	5.62K, $\pm 1\%$ Composition, 33, Variable, composition, 1K, $\pm 20\%$ (X10 LEVEL CH 1)	CGW ALB CTS	NS20 EB 65
R9264 R9265 R9266 & R9267 R9268 & R9269 R9270 R9271 R9272 R9273 & R9274	0234 9040 0234 8440 0236 5490 0236 5330 0234 8440 0236 5330 0234 7920 0236 4340	910, 1W 9.1K 634, $\pm 1\%$ 432, $\pm 1\%$ 9.1K 432, $\pm 1\%$ 62 40.2, $\pm 1\%$	CGW CGW CGW CGW CGW CGW CGW CGW	C32 C20 NS20 NS20 C20 NS20 C20 NS20
R9280 R9281 R9282 & R9283 R9284 R9285 R9286 R9287 R9288 R9289	0236 6560 0236 6840 0235 4140 0234 8540 0234 8570 0234 8570 0234 8570 0234 8540	8.25K, $\pm 1\%$ 16.2K, $\pm 1\%$ Composition, 10, 1/4W 24K Test Option 33K Test Option 33K 24K	CGW CGW ALB CGW CGW CGW CGW CGW	NS20 NS20 CB C20 C20 C20 C20 C20
R9291 R9292 R9293 & R9294 R9295	0234 8340 0234 8480 0211 8640 0203 1530	3.6K 13K Wirewound, 4.7 Composition, 10, $\pm 10\%$	CGW CGW IRC ALB	C20 C20 BW1/2 EB
R9301 & R9302 R9303 R9304 R9306	0237 0740 0203 0000 0234 8260 0203 0000	430, 2W Composition, 10 1.6K Composition, 10	CGW ALB CGW ALB	C42S EB C20 EB

<u>Symbol</u>	<u>Part No.</u>	<u>Description</u>	<u>Vendor</u>	
			<u>Code</u>	<u>Type</u>
<u>RESISTORS (Cont.)</u>				
R9400	0235 4240	Composition, 27, 1/4W	ALB	CB
R9401	0107 5960	Variable, composition, 100K, $\pm 20\%$ (GAS COMP)	CTS	65
R9402	0234 8690	100K	CGW	C20
R9403	0237 5670	1M, $\pm 1\%$, 1/8W	TEX	CD1/8R
R9404	0234 7970	100	CGW	C20
R9406	0107 5960	Variable, composition, 100K, $\pm 20\%$, 1/4W (COARSE DC BAL)	CTS	65
R9407	0107 2952	Variable, 100K/100K/100K, $\pm 20\%$ (DC BAL/POSITION)	ABD	
R9408	0235 5180	240K, 1/4W	ALB	CB
R9409	0203 1170	Composition, 750K	ALB	CB
R9411	0203 1300	Composition, 2.7M	ALB	EB
R9412	0234 8520	20K	CGW	C20
R9413	0235 4300	Composition, 47, 1/4W	ALB	AB
R9414	0203 0100	Composition, 27	ALB	EB
R9416	0235 4380	Composition, 100, 1/4W	ALB	CB
R9417	0235 2350	3.9K, $\pm 2\%$, 1W	CGW	C32
R9418	0235 4300	Composition, 47, 1/4W	ALB	CB
R9419	0235 4240	Composition, 27, 1/4W	ALB	CB
R9426	0234 8340	3.6K	CGW	C20
R9421	0235 4240	Composition, 27, 1/4W	ALB	CB
R9422	0235 4300	Composition, 47, 1/4W	ALB	CB
R9423 & R9424	0235 0670	3K, $\pm 2\%$	CGW	C20
R9425	0235 0730	5.1K, $\pm 2\%$	CGW	C20
R9420	0107 5930	Variable, composition, 3K, $\pm 20\%$ (BRIDGE BAL)	CTS	65
R9427	0109 3620	Variable, composition, 75K, $\pm 20\%$, 1/4W (GAIN ADJ)	CTS	200
R9428	0107 3041	Variable, composition, 10K, $\pm 20\%$, 1/8W (VARIABLE)	ABD	
R9429	0234 8730	150K	CGW	C20
R9430	0234 8560	30K	CGW	C20
R9431	0107 5950	Variable, composition, 50K, $\pm 20\%$ (INVERT BAL)	CTS	65
R9432	0236 5490	634, $\pm 1\%$	CGW	NS20

Symbol	Part No.	Description	Vendor	
			Code	Type
<u>RESISTORS (Cont.)</u>				
R9433	0234 8560	30K	CGW	C20
R9434	0236 5490	634, $\pm 1\%$	CGW	NS20
R9435	0235 4300	Composition, 47, 1/4W	ALB	CB
R9436 & R9437	0236 4890	150, $\pm 1\%$	CGW	NS20
R9438	0234 8040	200	CGW	C20
R9439	0237 8550	1.33K, $\pm 1\%$, 1W	IRC	CES
R9440	0235 4300	Composition, 47, 1/4W	ALB	CB
R9441	0203 0120	Composition, 33	ALB	EB
R9442 & R9443	0234 8150	560	CGW	C20
R9444	0234 8450	10K	CGW	C20
R9446	0234 8450	10K	CGW	C20
R9447 & R9448	0235 0840	15K, $\pm 2\%$	CGW	C20
R9449	0235 0480	470, $\pm 2\%$	CGW	C20
R9451	0235 0480	470, $\pm 2\%$	CGW	C20
R9452 & R9453	0236 6400	5.62K, $\pm 1\%$	CGW	NS20
R9454	0107 2658	Variable, 250, $\pm 20\%$, 1/4W (X10 CAL CH 2)	ABD	
R9456 & R9457	0236 6500	7.15K, $\pm 1\%$	CGW	NS20
R9458	0236 6400	5.62K, $\pm 1\%$	CGW	NS20
R9459	0109 3970	Variable, composition, 500, 1/10W (HF ADJ)	CRL	601-1
R9461	0236 6400	5.62K, $\pm 1\%$	CGW	NS20
R9462	0203 0120	Composition, 33	ALB	EB
R9463	0107 5920	Variable, composition, 1K, $\pm 20\%$ (X10 LEVEL CH 2)	CTS	65
R9464	0234 9040	910, 1W	CGW	C32
R9465	0234 8440	9.1K	CGW	C20
R9466 & R9467	0236 5490	634, $\pm 1\%$	CGW	NS20
R9468 & R9469	0236 5330	432, $\pm 1\%$	CGW	NS20
R9470	0234 8440	9.1K	CGW	C20
R9471	0236 5330	432, $\pm 1\%$	CGW	NS20
R9472	0234 7920	62	CGW	C20
R9473 & R9474	0236 4340	40,2, $\pm 1\%$	CGW	NS20
R9480	0236 6560	8.25K, $\pm 1\%$	CGW	NS20
R9481	0236 6840	16.2K, $\pm 1\%$	CGW	NS20
R9482 & R9483	0235 4140	Composition, 10, 1/4W	ALB	CB
R9484	0234 8540	24K	CGW	C20
R9485		Test Option		
R9486	0234 8570	33K	CGW	C20
R9487		Test Option		
R9488	0234 8570	33K	CGW	C20

<u>Symbol</u>	<u>Part Number</u>	<u>Description</u>	<u>Vendor</u>	
			<u>Code</u>	<u>Type</u>
RESISTORS (Continued)				
R9489	0234 8540	24K	CGW	C20
R9491	0234 8340	3.6K	CGW	C20
R9492	9234 8480	13K	CGW	C20
R9501	0236 5490	634, +1%	CGW	NS20
R9502 & R9503	0237 8690	1.87K, +1%, 1W	CGW	C6
R9504	0236 5490	634, +1%	CGW	NS20
R9505	0235 4920	composition, 20K, 1/4W	ALB	CB
R9506 & R9507	0236 4260	33.2, +1%	CGW	NS20
R9508	0234 8530	22K	CGW	C20
R9509	0234 8170	680	CGW	C20
R9511	0107 3241	variable, composition, 5K, +20%, 1/4W (DELAY LINE ADJ)	ABD	
R9512	0234 8170	680	CGW	C20
R9513 & R9514	0236 4760	110, +1%	CGW	NS20
R9515	0203 0090	composition, 24	ALB	EB
R9516	0203 0110	composition, 30	ALB	EB
R9517 & R9518	0237 9050	4.42K, +1%, 1W	CGW	C6
R9519	0236 5280	383, +1%	CGW	NS20
R9520	0236 4360	42.2, +1%	CGW	NS20
R9521	0203 0120	composition, 33	ALB	EB
R9522	0236 5490	634, +1%	CGW	NS20
R9523	0236 4890	150, +1%	CGW	NS20
R9524	0236 5490	634, +1%	CGW	NS20
R9525	0236 4360	42.2, +1%	CGW	NS20
R9526 & R9527	0236 5140	274, +1%	CGW	NS20
R9528	0237 0730	390, 2W	CGW	C42S
R9529	0235 0670	3K, +2%	CGW	C20
R9530	0237 0760	510, +2%, 2W	CGW	C42S
R9531	0235 0580	1.2K, +2%	CGW	C20
R9532	0234 9180	3.6K, 1W	CGW	C32
R9533 & R9534	0234 8080	300	CGW	C20
R9535	0203 3080	composition, 22, 1W	ALB	GB
R9536	0222 4690	wirewound, 150, 5W	WDL	X
R9537	0234 8520	20K	CGW	C20

<u>Symbol</u>	<u>Part Number</u>	<u>Description</u>	<u>Vendor</u>	
			<u>Code</u>	<u>Type</u>
RESISTORS (Continued)				
R9538 & R9539	0235 2350	3.9K, <u>+2%</u> , 1W	CGW	C32
R9540	0234 7910	56	CGW	C20
R9541	0203 3150	composition, 43, 1W	ALB	GB
R9542	0234 8750	56, 1W	CGW	C32
R9543	0235 4140	composition, 10, 1/4W	ALB	CB
R9544	0203 0120	composition, 33	ALB	EB
R9545	0107 5910	variable, composition, 500, <u>+20%</u> , (OUTPUT CURR.ADJ)	CTS	65
R9546	0234 8250	1.5K	CGW	C20
R9547	0203 0120	composition, 33	ALB	EB
R9548	0235 4140	composition, 10, 1/4W	ALB	CB
R9549	0234 8370	4.7K	CGW	C20
R9551 to R9554	0235 0300	82, <u>+2%</u>	CGW	C20
R9600	0234 8200	910	CGW	C20
R9601	0234 8380	5.1K	CGW	C20
R9602	0236 4690	93.1, <u>+1%</u>	CGW	NS20
R9603 & R9604	0203 1610	composition, 47, <u>+10%</u>	ALB	EB
R9605	0234 7970	100	CGW	C20
R9606	0234 7920	62	CGW	C20
R9607	0237 7180	49.9, 1W, <u>+1%</u>	CGW	C20
R9608	0234 8310	2.7K	CGW	C20
R9609	0234 8360	4.3K	CGW	C20
R9610	0234 8270	1.8K	CGW	C20
R9611	0234 8420	7.5K	CGW	C20
R9612	0234 8460	11K	CGW	C20
R9613	0234 8200	910	CGW	C20
R9614	0107 5910	variable, composition, 500, <u>+20%</u> (CH 2 OUTPUT LEVEL)	CTS	65
R9615	0234 8290	2.2K	CGW	C20
R9616	0234 8360	4.3K	CGW	C20
R9617	0234 8530	22K	CGW	C20
R9618	0107 5910	variable, composition, 500, <u>+20%</u> (NORMAL TRIG ADJ)	CTS	65
R9619	0107 5910	variable, composition, 500, <u>+20%</u> (CH 2 ONLY TRIG ADJ)	CTS	65
R9620	0234 8190	820	CTS	65
R9621*	0234 8140	510	CGW	C20
R9622	0234 8450	10K	CGW	C20
R9623	0234 8410	6.8K	CGW	C20
R9624	0234 8210	1K	CGW	C20
R9625	0235 4440	composition, 180, 1/4W	ALB	CB

<u>Symbol</u>	<u>Part No.</u>	<u>Description</u>	<u>Vendor</u>	
			<u>Code</u>	<u>Type</u>
<u>RESISTORS (Cont.)</u>				
R9626	0234 8020	160	CGW	C20
R9627	0234 8450	10K	CGW	C20
R9628	0234 8280	2K	CGW	C20
R9629	0234 7990	120	CGW	C20
R9630	0234 8140	510	CGW	C20
R9631	0234 8460	11K	CGW	C20
R9632	0203 0150	Composition, 43	ALB	EB
R9633	0234 8140	510	CGW	C20
R9634	0234 8270	Composition, 1.8K	CGW	C20
R9636	0237 0770	560, 2W	CGW	C42S
R9637	0234 8450	10K	CGW	C20
R9638	0234 8430	8.2K	CGW	C20
R9639	0234 8460	11K	CGW	C20
R9641	0234 8450	10K	CGW	C20
R9642	0236 5670	976, $\pm 2\%$	CGW	NS20
R9643	0236 5420	536, $\pm 2\%$	CGW	NS20
R9644	0237 0940	3K, 2W	CGW	C42S
R9646	0234 8040	200	CGW	C20
R9700	0236 7200	38.3K, $\pm 1\%$,	CGW	NS20
R9701	0234 8320	3K	CGW	C20
R9702	0234 9030	820, 1W	CGW	C32
R9703	0203 1170	Composition, 750K	ALB	EB
R9704	0234 8450	10K	CGW	C20
R9705	0234 8210	1K	CGW	C20
R9706	0234 8400	6.2K	CGW	C20
R9707	0234 8490	15K	CGW	C20
R9708 & R9709	0234 8450	10K	CGW	C20
R9710	0234 8400	6.2K	CGW	C20
R9711	0234 8660	75K	CGW	C20
R9712	0234 9030	820, 1W	CGW	C32
R9713	0234 8320	3K	CGW	C20
R9714	0203 0060	Composition, 18	ALB	EB
R9715	0236 6980	22.6K, $\pm 1\%$	CGW	NS20
R9716	0235 0540	820, $\pm 2\%$	CGW	C20
R9717	0236 6260	4.02K, $\pm 1\%$	CGW	NS20

<u>Symbol</u>	<u>Part Number</u>	<u>Description</u>	<u>Vendor</u>	
			<u>Code</u>	<u>Type</u>
<u>RESISTORS (Continued)</u>				
R9718	0236 6920	19.6K, <u>+1%</u>	CGW	NS20
R9719	0234 7970	100	CGW	C20
R9720	0236 6720	12.1K, <u>+1%</u>	CGW	NS20
R9721	0235 0830	13K, <u>+2%</u>	CGW	C20
R9722	0235 0610	1.6K, <u>+2%</u>	CGW	C20
R9723	0234 8520	20K	CGW	C20
R9724	0234 8270	1.8K	CGW	C20
R9726	0234 8290	2.2K	CGW	C20
R9727	0234 8310	2.7K	CGW	C20
R9728	0234 7910	56	CGW	C20
R9729	0234 7950	82	CGW	C20
R9731	0203 1600	composition, 39	ALB	EB
R9732	0234 8590	39K	CGW	C20
R9733	0234 8440	9.1K	CGW	C20
R9734	0234 8270	1.8K	CGW	C20
R9735	0203 0160	composition, 47	ALB	EB
R9736	0234 9070	1.2K, 1W	CGW	C32
R9737	0203 1610	composition, 47, <u>+10%</u>	ALB	EB
R9738	0236 6060	2.49K, <u>+1%</u>	CGW	NS20
R9739	0236 7020	24.9K, <u>+1%</u>	CGW	NS20
R9741	0234 8260	1.6K	CGW	C20
R9742	0234 8340	3.6K	CGW	C20
R9743	0236 6860	16.9K, <u>+1%</u>	CGW	NS20
R9744	0236 6570	8.45K, <u>+1%</u>	CGW	NS20
R9746	0203 0070	composition, 20	ALB	EB
R9801 & R9802	0234 8130	470	CGW	C20
R9803	0203 0120	composition, 33	ALB	EB
R9804	0234 8360	4.3K	CGW	C20
R9806	0234 8360	4.3K	CGW	C20
R9807	0109 3600	var., composition, 1K, .1W	CRL	601-1
R9808	0234 8330	3.3K	CGW	C20
R9809	0236 5010	200, <u>+1%</u>	CGW	NS20
R9811	0236 5010	200, <u>+1%</u>	CGW	NS20
R9812	0237 8990	3.83K, <u>+1%</u> , 1W	CGW	V6
R9813 & R9814	0236 3090	200K	CGW	C20

<u>Symbol</u>	<u>Part No.</u>	<u>Description</u>	<u>Vendor Code</u>	<u>Type</u>
<u>RESISTORS (Cont.)</u>				
R9816	0234 8520	20K	CGW	C20
R9817	0236 6710	11.8K, $\pm 1\%$	CGW	NS20
R9818	0236 6760	13.3K, $\pm 1\%$	CGW	NS20
R9901 & R9902	0234 8130	470	CGW	C20
R9903	0203 0120	Composition, 33	ALB	EB
R9904	0234 8360	4.3K	CGW	C20
R9905*	0235 4720	Composition, 3K, 1/4W	ALB	CB
R9906	0234 8360	4.3K	CGW	C20
R9907	0109 3600	Variable, composition, 1K	CRL	601-1
R9908	0234 8330	3.3K	CGW	C20
R9909	0236 5010	200, $\pm 1\%$	CGW	NS20
R9911	0236 5010	200, $\pm 1\%$	CGW	NS20
R9912	0237 8990	3.83K, $\pm 1\%$, 1W	CGW	C6
R9913 & R9914	0236 3090	200K	CGW	C20

SWITCHES

S901	0501 7461	Lever, 1 section, 4 positions (INPUT SEL CH 1)	ABD	
S902	0501 7433	Rotary, 3 sections, 9 positions (VOLTS/DIV)	ABD	
S911	0501 7451	Lever, 1 section, 3 positions (INPUT SEL CH 2)	ABD	
S912	0501 7433	Rotary, 3 sections, 9 positions (VOLTS/DIV)	ABD	
S920	0107 3041	Part of R9228		
S921	0501 7621	(VARIABLE, GAIN CH 1) Switch Section, Rotary (NORM CH 1)	ABD	

<u>Symbol</u>	<u>Part No.</u>	<u>Description</u>	<u>Vendor</u>	
			<u>Code</u>	<u>Type</u>
<u>SWITCHES (Cont.)</u>				
S922A & S922B	0503 2390	Slide, DPDT (PULL X10 CH 1)	COW	126
S940	0107 3041	Part of R9428	ABD	
S941	0501 7621	Switch Section, Rotary (NORM CH 2)	ABD	
S942A & S942B	0503 2390	Slide, DPDT (PULL X10 CH 2)	COW	126
S950	0503 2550	Push, SPST (BEAM FINDER)	GRY	32
S960	0501 7442	Rotary, 2 sections 2/5 positions (TRIG MODE)	ABD	
S970		Part of S960 (MODE)		
S971	0503 2490	Toggle, SPST (CHOP RATE)	ALCO	MST105D

TRANSFORMER

T9701	2001 4841	BTO	ABD	
-------	-----------	-----	-----	--

ELECTRON TUBES

V921 & V922	2501 4060	8056	RCA	NUVISTOR
V941 & V942	2501 4060	8056	RCA	NUVISTOR

NETWORKS

Z9201 & Z9202	8800 2426	Peaking	ABD	
Z9401 & Z9402	8800 2426	Peaking	ABD	
Z9501 & Z9502	8800 2422	Peaking	ABD	
Z9503	8800 2424	Peaking	ABD	
Z2050	8700 1871	Termination CRT	FCIC	7062

LIST OF RECOMMENDED VENDORS

CODE	NAME	CODE	NAME
ABD	Du Mont Laboratories	HP	Hewlett-Packard Company
AER	Aerovox Corporation	IRC	International Resistance Company
AHM	Arrow-Hart & Hegeman Electric Company	IRP	International Rectifier Corporation
ALB	Allen-Bradley Company	ITT	International Telephone and Telegraph Corporation
ALC	Allied Control	JEF	Jeffers Electronics, Inc.
ALCO	Alco Electronic Products	JHN	E. F. Johnson Company
ALD	Alden Products Company	JWM	J. W. Miller Company
AMA	Amaton Electronic Hardware	KUL	Kulka Electric Mfg. Co. Inc.
AMP	Amp Inc.	KXM	Klixon Metals and Control Corporation
AMR	Amperite Company, Inc.	LED	Ledex Inc.
AMX	Amperex Electronics Products, Inc.	LEE	Leecraft Mfg. Company
APC	American Phenolic Corporation	LIN	Line Electric
APH	Amphenol Electronics Corporation	LFI	Littlefuse, Inc.
ARC	Arco Electronics Inc. (Elmenco)	MAL	P. R. Mallory & Company, Inc.
AST	Astron Corporation	MCR	Micro Switch (Division of Minneapolis-Honeywell Regulator Co.)
AUT	Automatic Metal Products Corporation	MIC	Micamold Electronics Mfg. Corporation
BNS	Bourns Inc.	MIL	Miller Electric Company
BUR	Burndy Engrg. Company	MOV	M-O Valve Company Ltd.
BUS	Bussmann Mfg. Company	MOT	Motorola Semiconductor Products, Inc.
CAN	Cannon Electric Company	MUC	Mucon Corporation
CBS	CBS-Hytron Division of CBS	MUL	Mullard Limited
CDE	Cornell-Dubilier Electric Corporation	MUT	The Muter Company
CGW	Corning Glass Works	NYT	New York Transformer Company, Inc.
CH	Cutler-Hammer, Inc.	OAK	Oak Mfg. Company
CHC	Chester Cable Corporation	PHC	Philca Corporation
CHM	Chatham Electronics	PHI	Philips Electronic Tube Division
CIN	Cinch Manufacturing Company	PLS	Plastoid Corporation
CLS	Clarostat Mfg. Co., Inc.	POT	Potter & Brumfield, Inc.
COC	Continental Carbon (Division of Wirt Company)	PRC	Precision Resistor Co., Inc.
COW	Continental-Wirt Electronics Corporation	PYR	Pyramid Electric Company
CPC	C. P. Clara & Company	RCA	Radio Corporation of America
CRL	Centralab, Division of Globe-Union, Inc.	RMC	Radio Materials Corporation
CST	Chicago Standard Transformer Corporation	ROY	Royal Electric Corporation, Inc.
CTC	Cambridge Thermionic Corporation	RTN	Rotron Mfg. Company
CTS	Chicago Telephone Supply Corporation	SIG	Signalite Inc.
DAG	Dage Electric Company, Inc.	SIL	Silicon Transistor Corporation
DAL	Dale Products, Inc.	SLT	Sealctro Corporation
DIC	Dialight Corporation	SOL	Solitron Devices, Inc.
DRK	Drake Mfg. Company	SPG	Sprague Electric Company
EBY	Hugh H. Eby, Inc.	STC	Stackpole Carbon Company
EDL	Edal Industries	STW	Standard Winding Company
EIA	Any manufacturer meeting EIA standards	SUM	Summit Coil Company
ELC	Electra Manufacturing Company	SWT	Switchcraft Inc.
ELD	Eldema Corporation	SWW	Stanwyck Winding Company
ELM	Elmenco	SYL	Sylvania Electric Products, Inc.
EMC	Electro Motive Mfg. Company	SYN	Syntronic Instruments, Inc.
EMW	Elmwood Sensors, Inc.	TEC	Transistor Electronics Corporation
ERC	Erie Technological Products, Inc.	TEX	Texas Instruments, Inc.
ESX	Essex Electronics	THC	Thermal Control, Inc.
FCI	Fairchild Camera and Instrument Corporation	TOR	Torrington Mfg. Company
FER	Ferroxcube Corporation of America	TRS	Tresco, Inc.
GDE	Good-All Electric Mfg. Company	TRU	Tru-Ohm Products
GE	General Electric Company	TUG	Tung-Sol Electric Inc.
GEN	General Instrument Corporation	UCN	Ucinite Company
GEP	General Products Corporation	UTC	United Transformer Company
GRC	General Radio Company	VIC	The Victoreen Instrument Company
GRY	Grayhill, Inc.	WDE	Wood Electric Corporation
GUD	The Gudeman Company	WDL	Ward Leonard Electric Company
HAM	The Hammarlund Manufacturing Co. Inc.	WES	Weston Electrical Instrument Corporation
HON	Honeywell	WYN	Welwyn International Inc.
HOP	Hopkins Engineering Company		

INSTRUMENT WARRANTY AND SERVICE NOTICE

WARRANTY

The Scientific Instrument Department warrants that each new Cathode-ray Oscilloscope, Automotive Test Equipment, and other Electronic or Electrical Test or Measuring Equipment (hereinafter referred to as "Instrument") manufactured or sold by it, is free from defects in material or workmanship under normal use and service for a period of one year from the date of its sale to the first purchaser for use. If, upon examination by Fairchild, the Instrument is determined to be defective in workmanship or material, Fairchild will, subject to the conditions set forth below, either repair the defective part or replace it with a new part. Fairchild shall not be liable for any delay or failure to furnish a replacement part resulting directly or indirectly from governmental restriction, priority allocation or any other governmental regulatory order or action, nor shall Fairchild be liable for damages by reason of the failure of the Instrument to perform properly or for any consequential damages. This warranty does not apply to any Instrument that has been subject to negligence, accident, misuse or improper installation, operation or that in any way has been tampered with, altered or repaired by any person other than an authorized Fairchild service organization or an employee thereof, or to any Instrument whose serial number has been altered, defaced or removed, or to any Instrument purchased within, and thereafter removed beyond, the continental limits of the United States. This warranty shall be void unless registration is promptly effected as provided herein. This warranty is in lieu of all other warranties, expressed or implied, and no one is authorized to assume any liability on behalf of Fairchild or impose any obligation upon it in connection with the sale of any Instrument, other than as stated above.

REGISTERING THE WARRANTY

To register this warranty, the enclosed warranty registration card must be properly filled out and mailed to the Instrument Service Department immediately upon receipt of the equipment. Complete information is necessary. BOTH THE TYPE NUMBER AND THE SERIAL NUMBER OF THE INSTRUMENT MUST BE GIVEN ON THIS CARD. Instruments must be examined immediately upon receipt, since claims for damage in transit will not be honored by the carrier unless prompt action is taken.

CHANGES IN SPECIFICATIONS

The right is reserved to change the published specifications of equipment at any time and to furnish merchandise in accordance with current specifications without incurring any liability to modify equipment previously sold, or to supply new equipment in accordance with earlier specifications excepting under the classification of special apparatus.

SERVICE

To insure service under our warranty, the enclosed warranty service card must be properly filled out and returned to the factory. In all cases where service or adjustment is requested, please contact the factory or an authorized depot, giving complete information concerning the nature of the failure and describing the manner in which the equipment was used when failure occurred. THE TYPE NUMBER AND SERIAL NUMBER of the equipment must also be given. In this way, much time can be saved and unnecessary inconvenience often avoided. When writing to the factory in this respect, address:

FAIRCHILD
Instrumentation
Scientific Instrument Dept.
750 Bloomfield Avenue, Clifton, New Jersey

The Instrument Service Department will then send the customer the written procedure for disposition and shipping instructions. All equipment should be packed and shipped in accordance with this procedure; and identification tags should be attached to each tube or instrument.

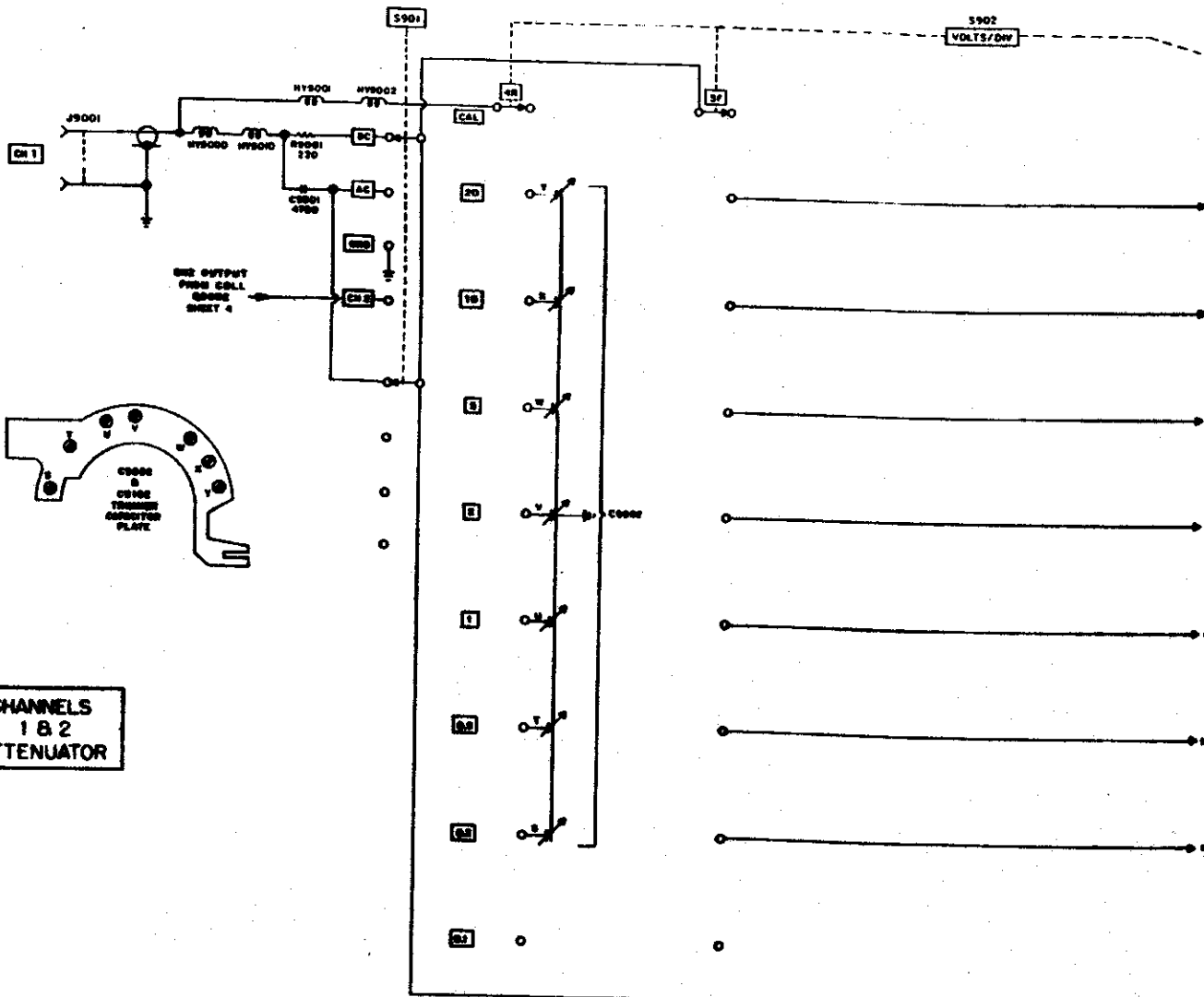
REPLACEMENT PARTS

If it is necessary to order a replacement component from the factory, always give the Type number and Serial number of the Instrument. Before ordering parts for in-warranty replacement or purchasing them for out-of-warranty replacement, be sure to consult the Parts List in the Instruction Manual. The Parts List gives the values, tolerances, ratings, and Fairchild part number for all electrical components used in the Instrument. This will help to expedite service.

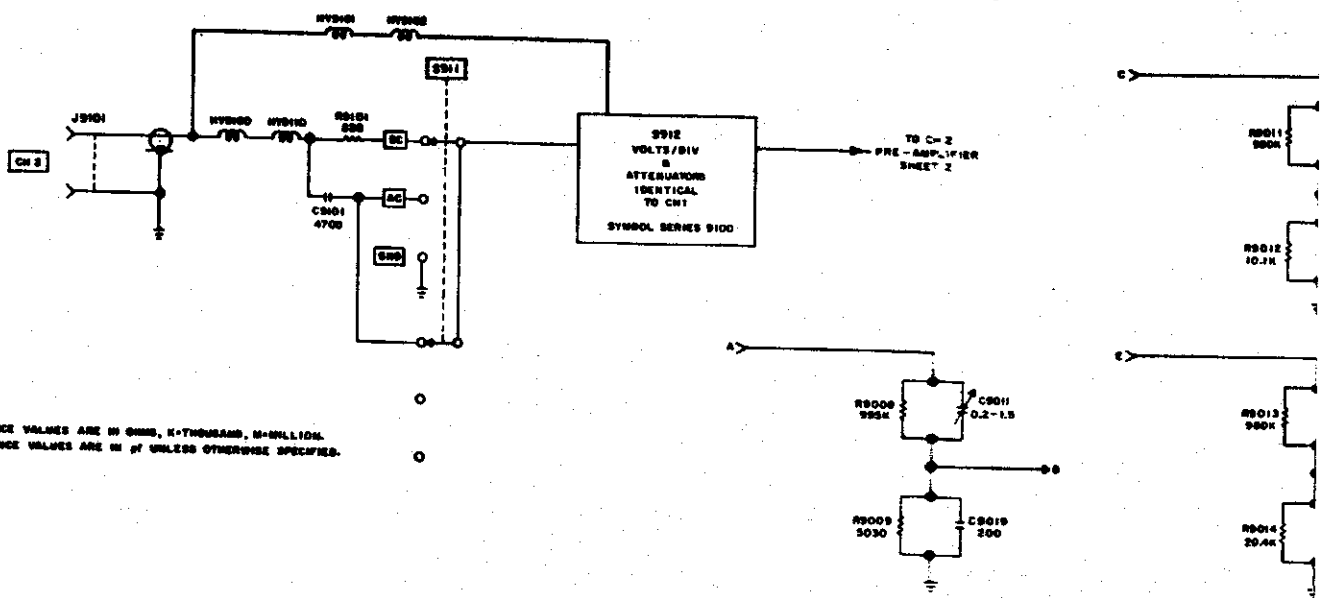
PATENT NOTICE

Manufactured under one or more U. S. Patents owned or controlled by Fairchild Camera and Instrument Corporation, 750 Bloomfield Avenue, Clifton, New Jersey, U.S.A. Patent Numbers supplied upon request.

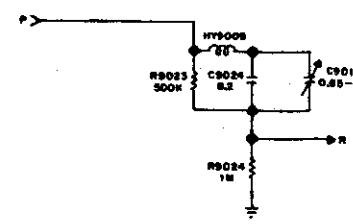
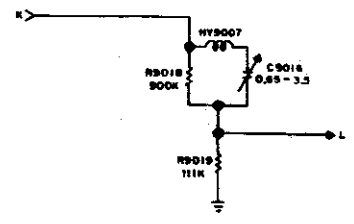
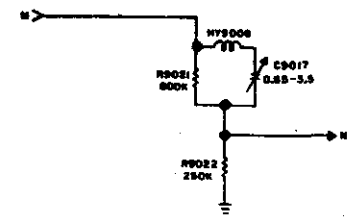
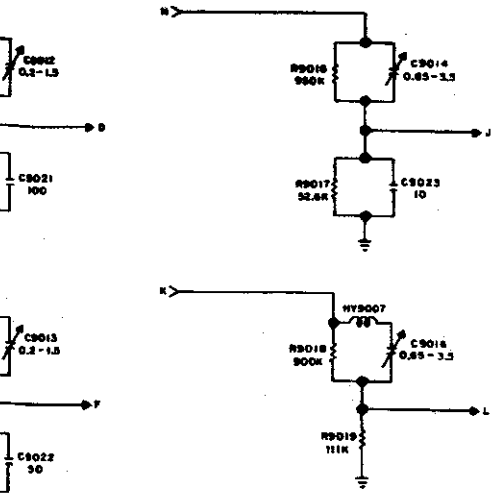
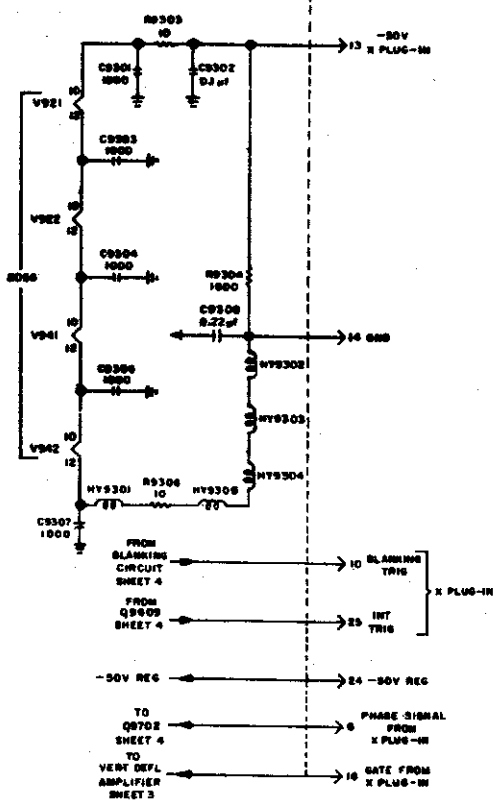
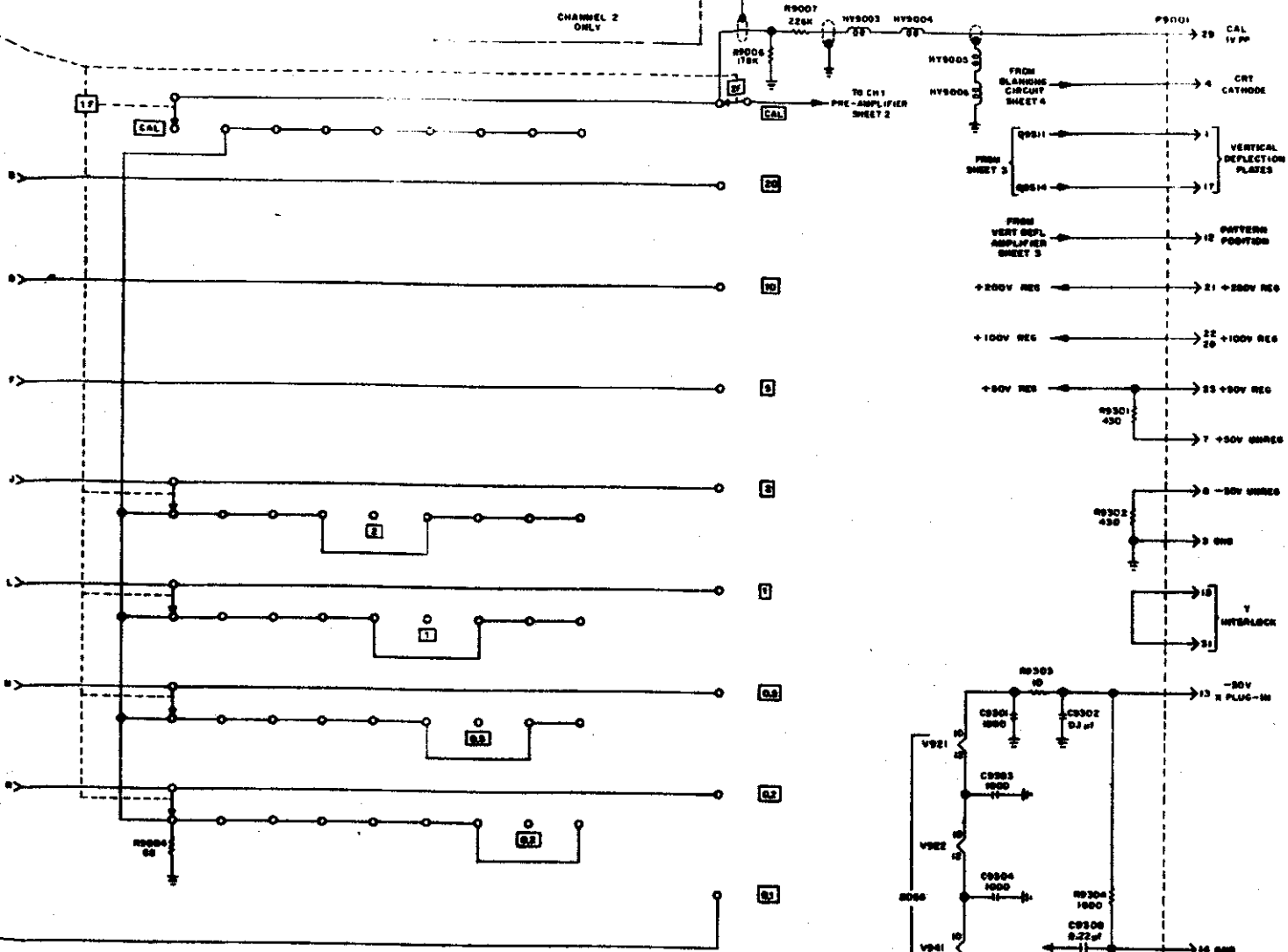
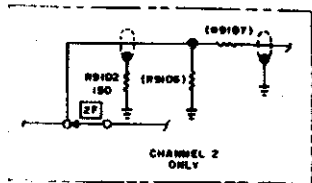
WARRANTY REGISTRATION
NO STAMP REQUIRED
IMPORTANT - MAIL THIS CARD
30 DAYS AFTER RECEIPT
SEE INSTRUCTIONS



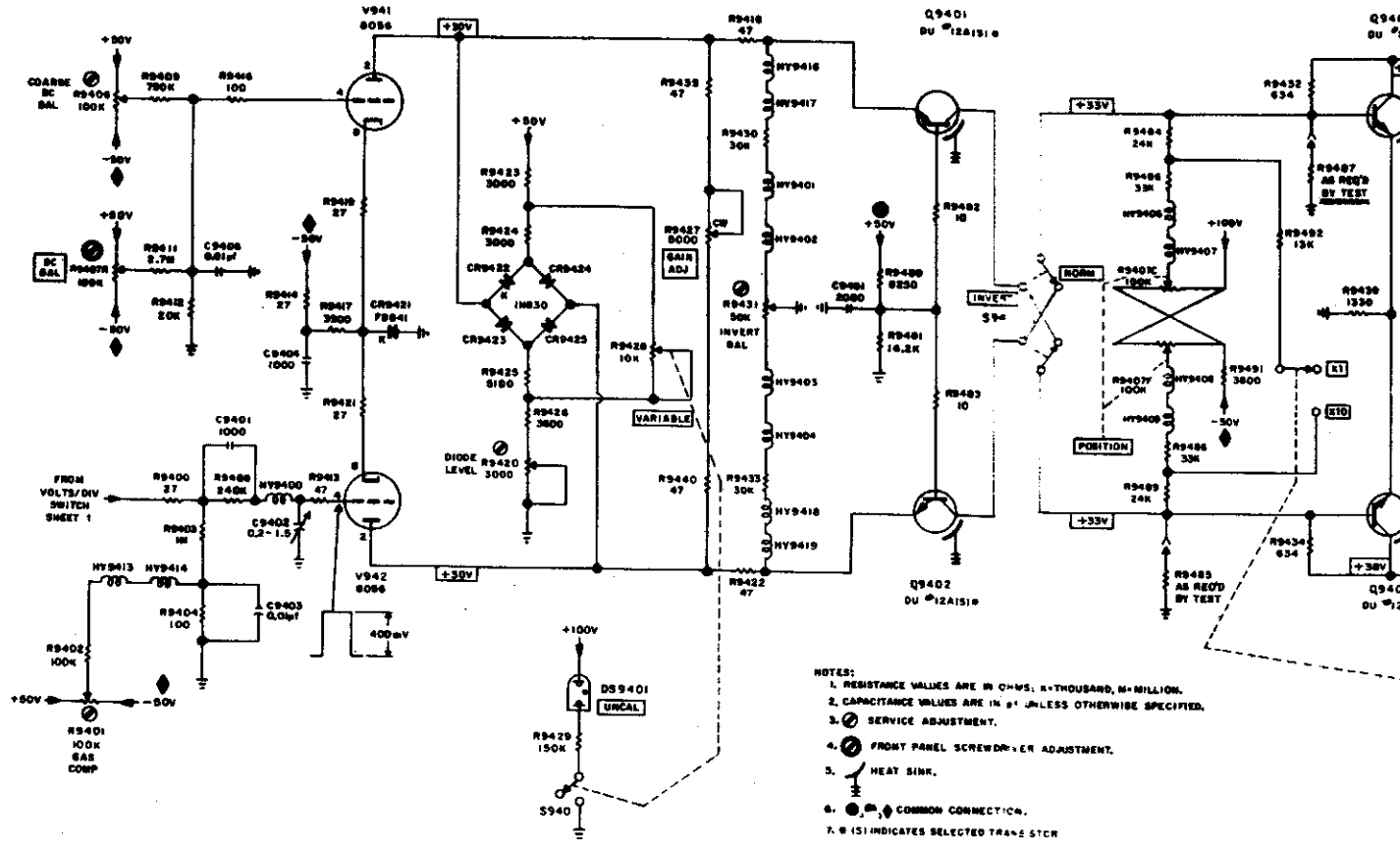
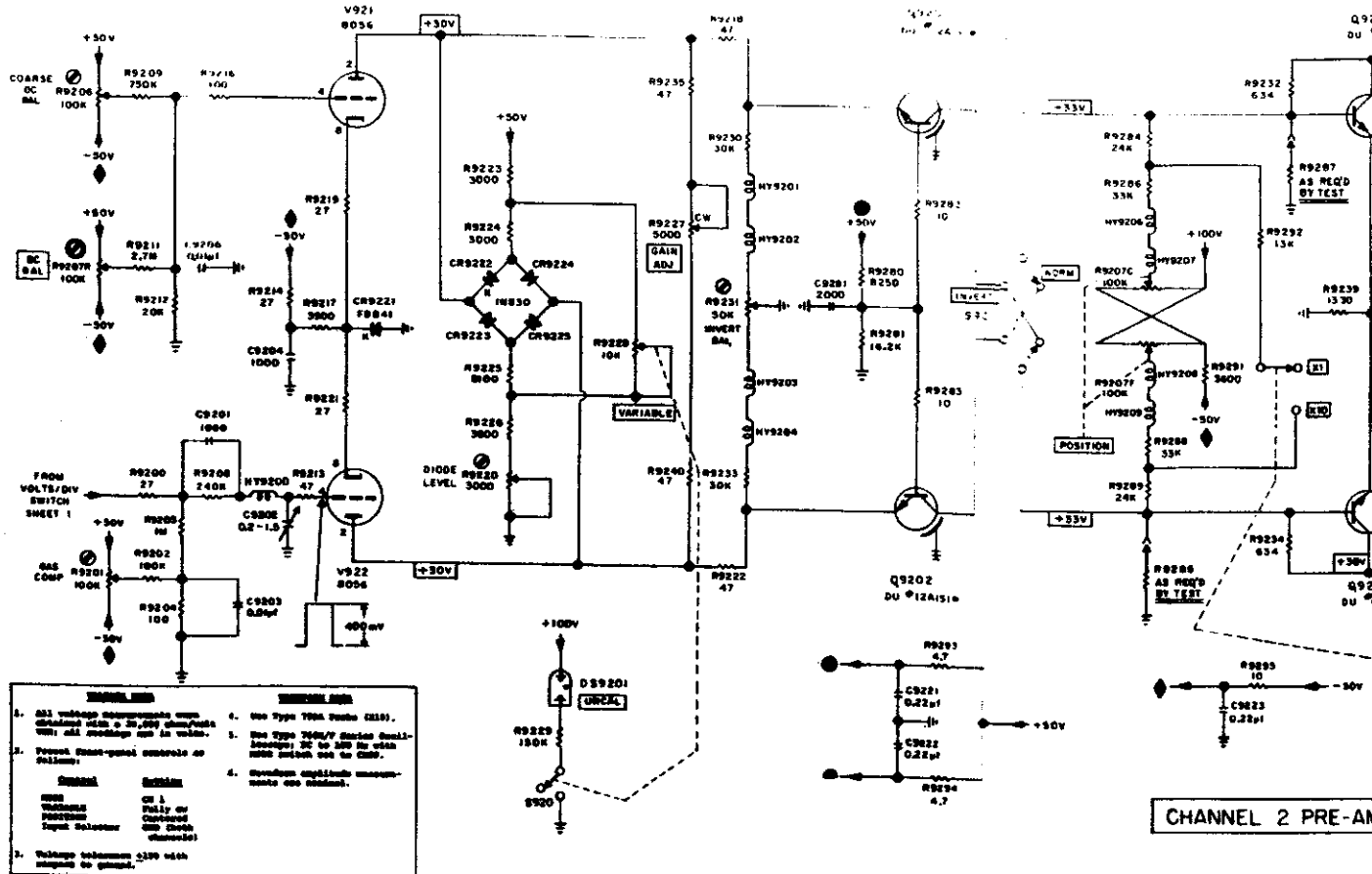
**CHANNELS
1 & 2
ATTENUATOR**



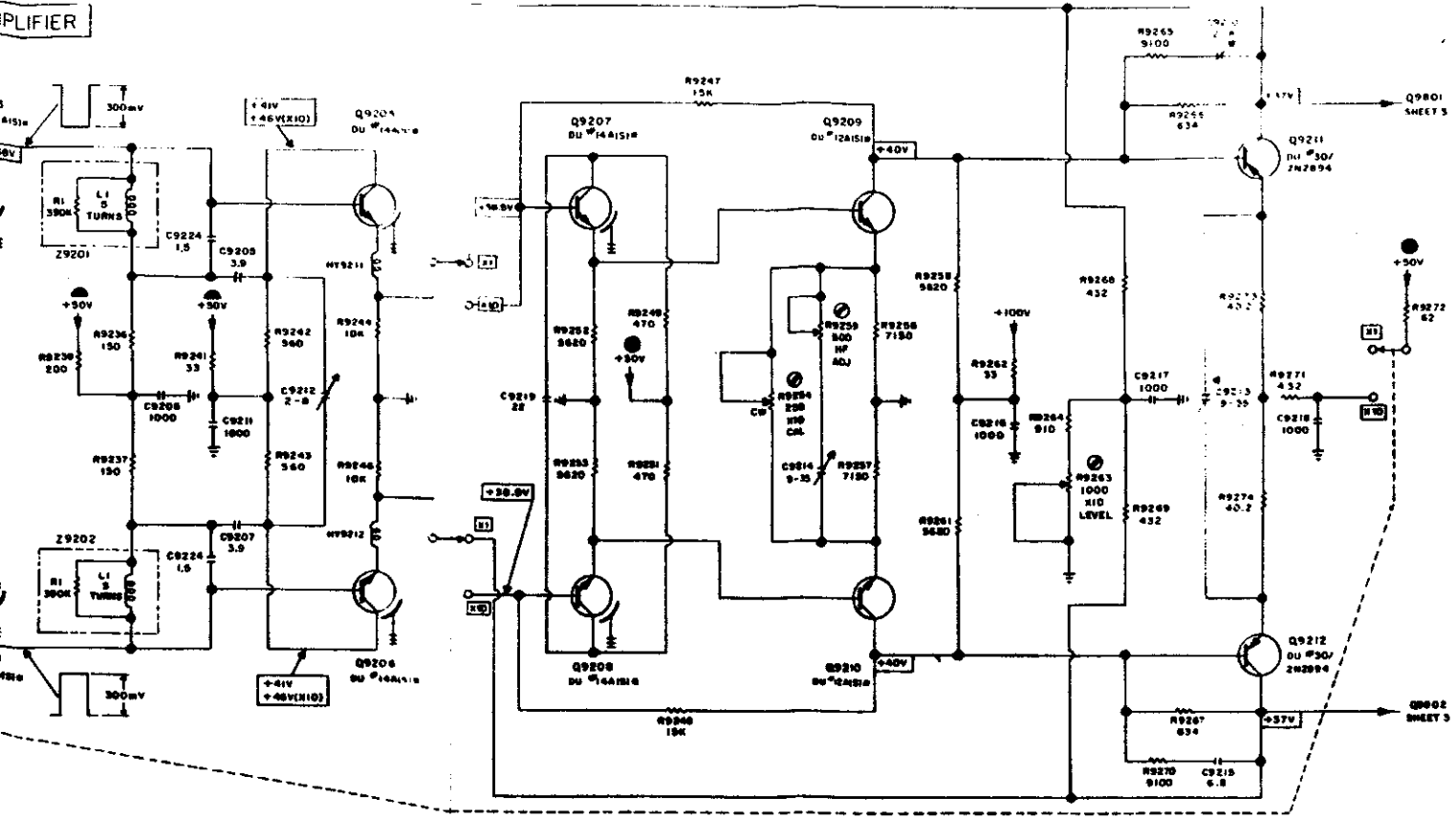
NOTES:
 1. RESISTANCE VALUES ARE IN OHMS, K-THOUSAND, M-MILLION.
 2. CAPACITANCE VALUES ARE IN μ F UNLESS OTHERWISE SPECIFIED.



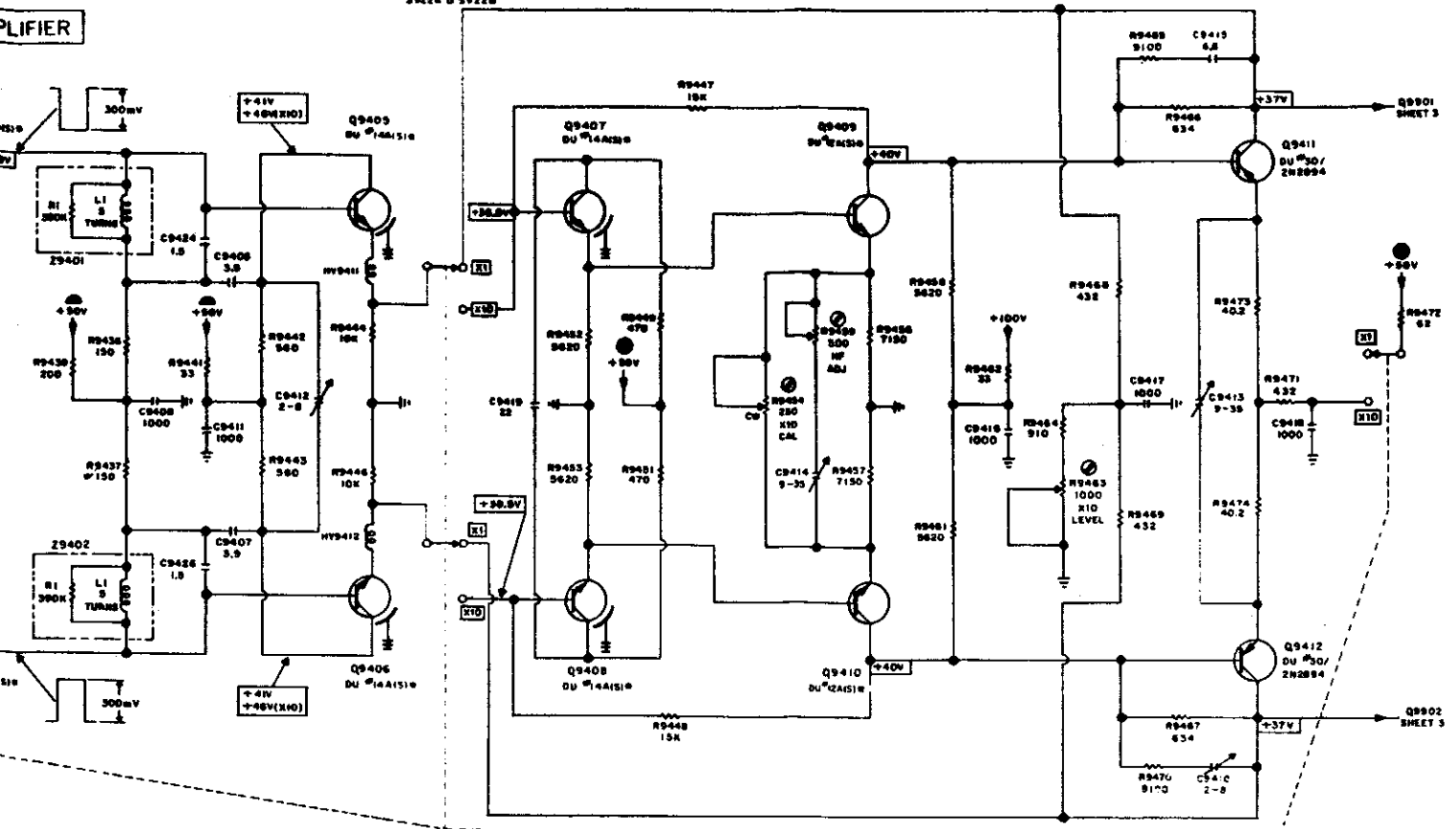
TYPE
79-02A
CHANNELS 1 & 2
ATTENUATORS
SHEET 1 OF 4



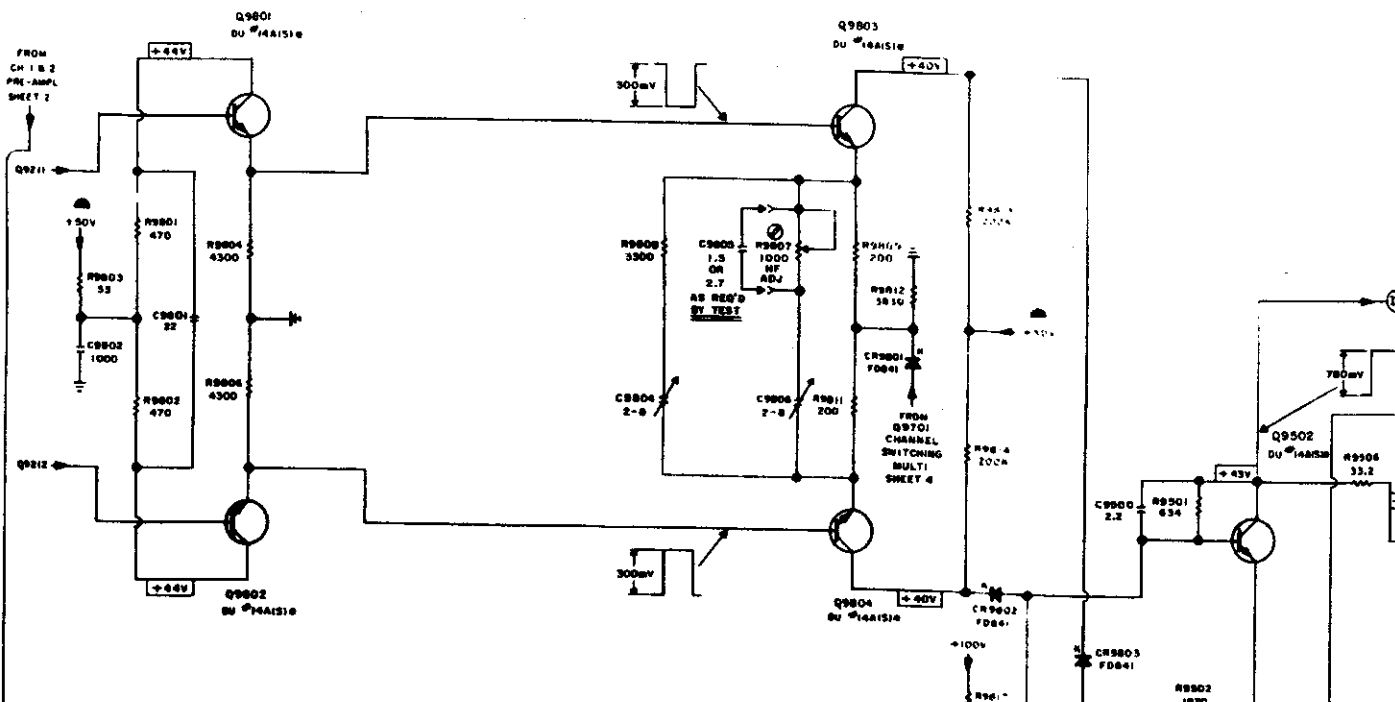
AMPLIFIER



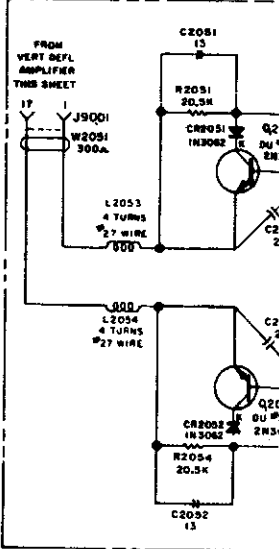
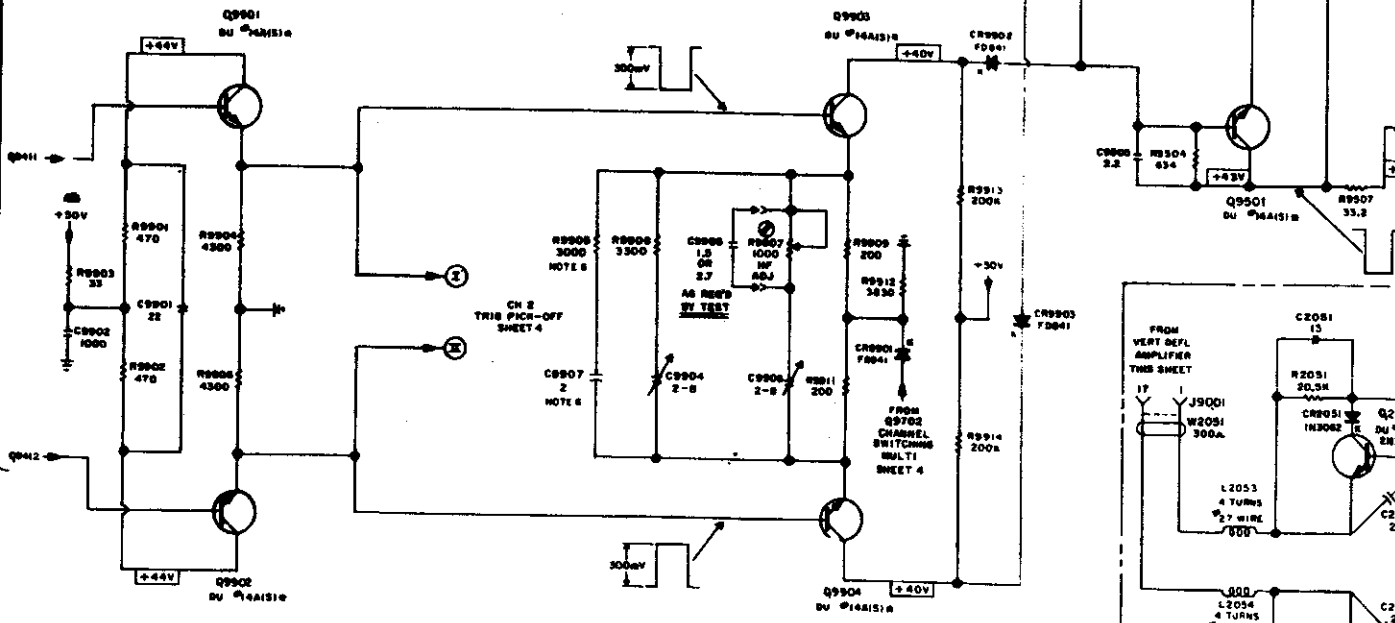
AMPLIFIER



CHANNEL 1 PRE-AMPLIFIER
&
SWITCHING AMPLIFIER



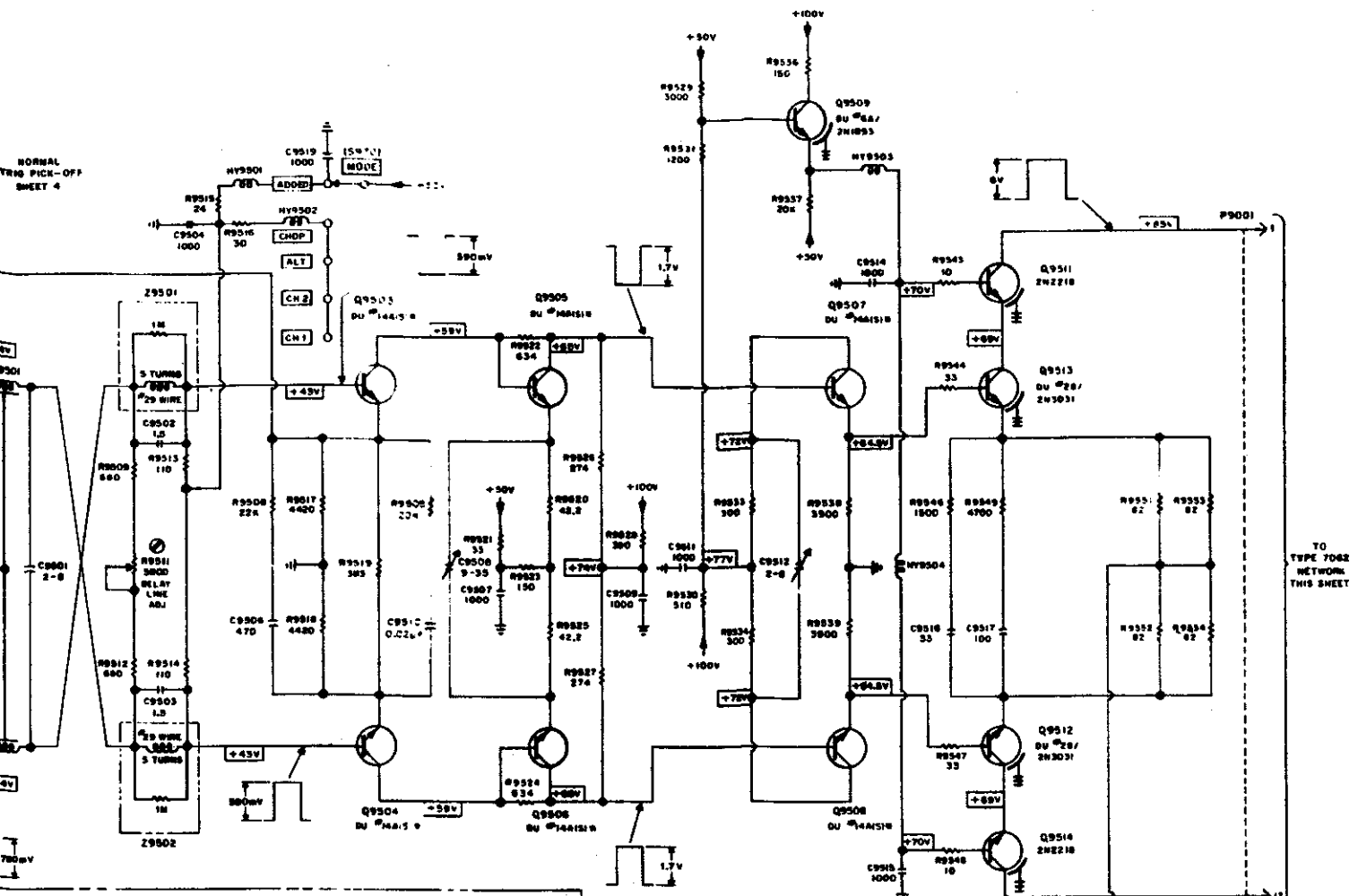
CHANNEL 2 PRE-AMPLIFIER
&
SWITCHING AMPLIFIER



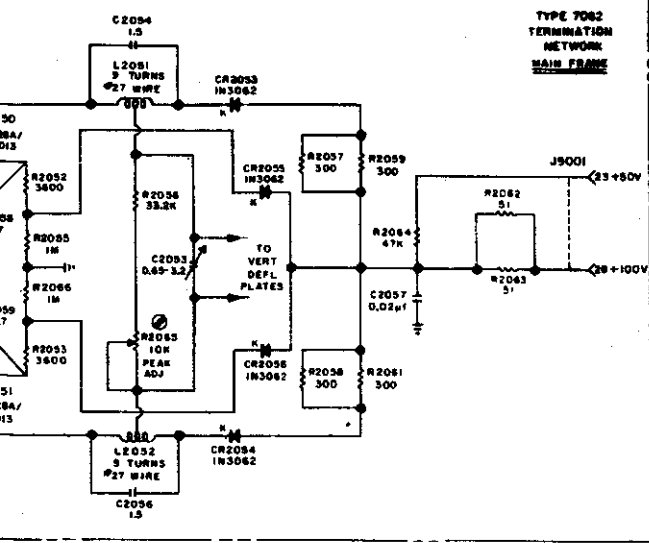
- NOTES:
1. RESISTANCE VALUES ARE IN OHMS, K=THOUSAND, M=MILLION.
 2. CAPACITANCE VALUES ARE IN pF UNLESS OTHERWISE SPECIFIED.
 3. SERVICE ADJUSTMENT.
 4. HEAT SINK.
 5. COMMON CONNECTION. (SEE SHEET 2).
 6. TEST OPTION: REMOVE R9905 & C9907 AS REQUIRED TO PROVIDE OPTIMUM PULSE RESPONSE.
 7. Q IS INDICATES SELECTED TRANSISTOR.

VERTICAL REFLECTION AMPLIFIER

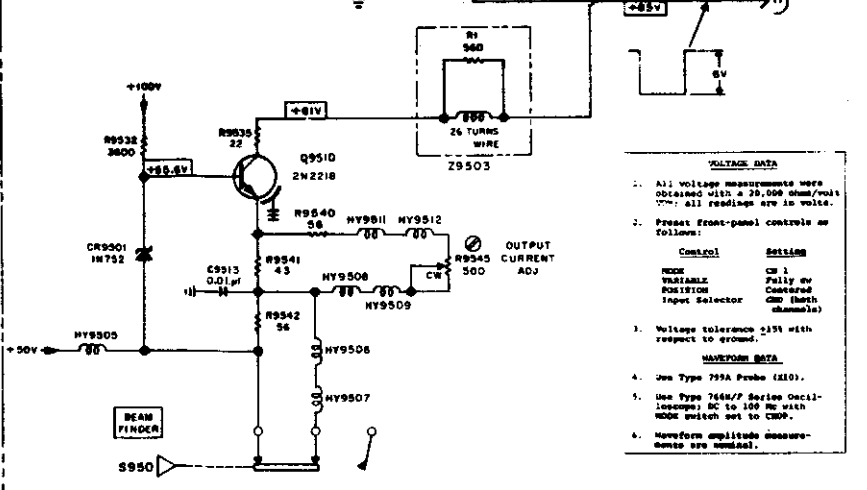
NORMAL TRNG PICK-OFF SHEET 4



TO TYPE 7062 NETWORK THIS SHEET



TYPE 7062 TERMINATION NETWORK
MAIN FRAME

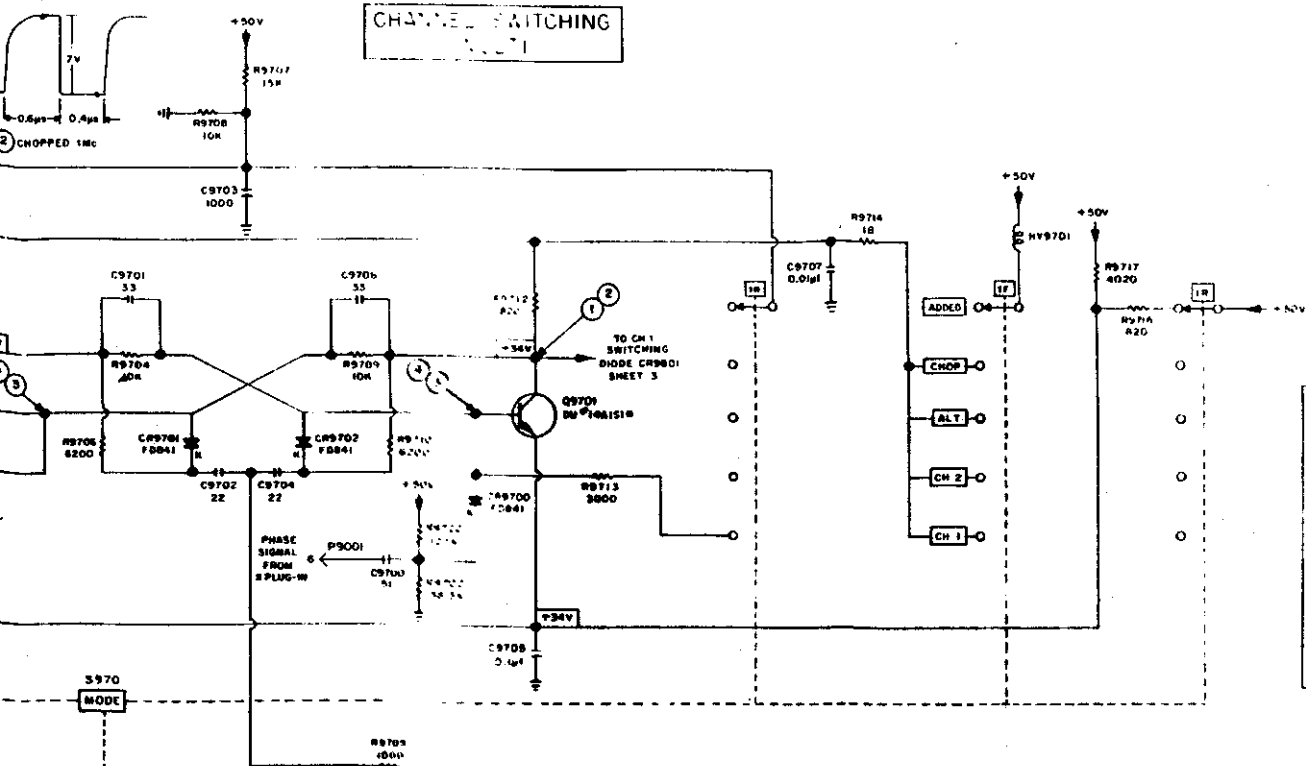


VOLTAGE DATA

- All voltage measurements were obtained with a 20,000 ohm/volt TV; all readings are in volts.
- Reset front-panel controls as follows:
Control Setting
MODE CH 1
POSITION Fully up
Control Centered
Input Selector CW (earth channels)

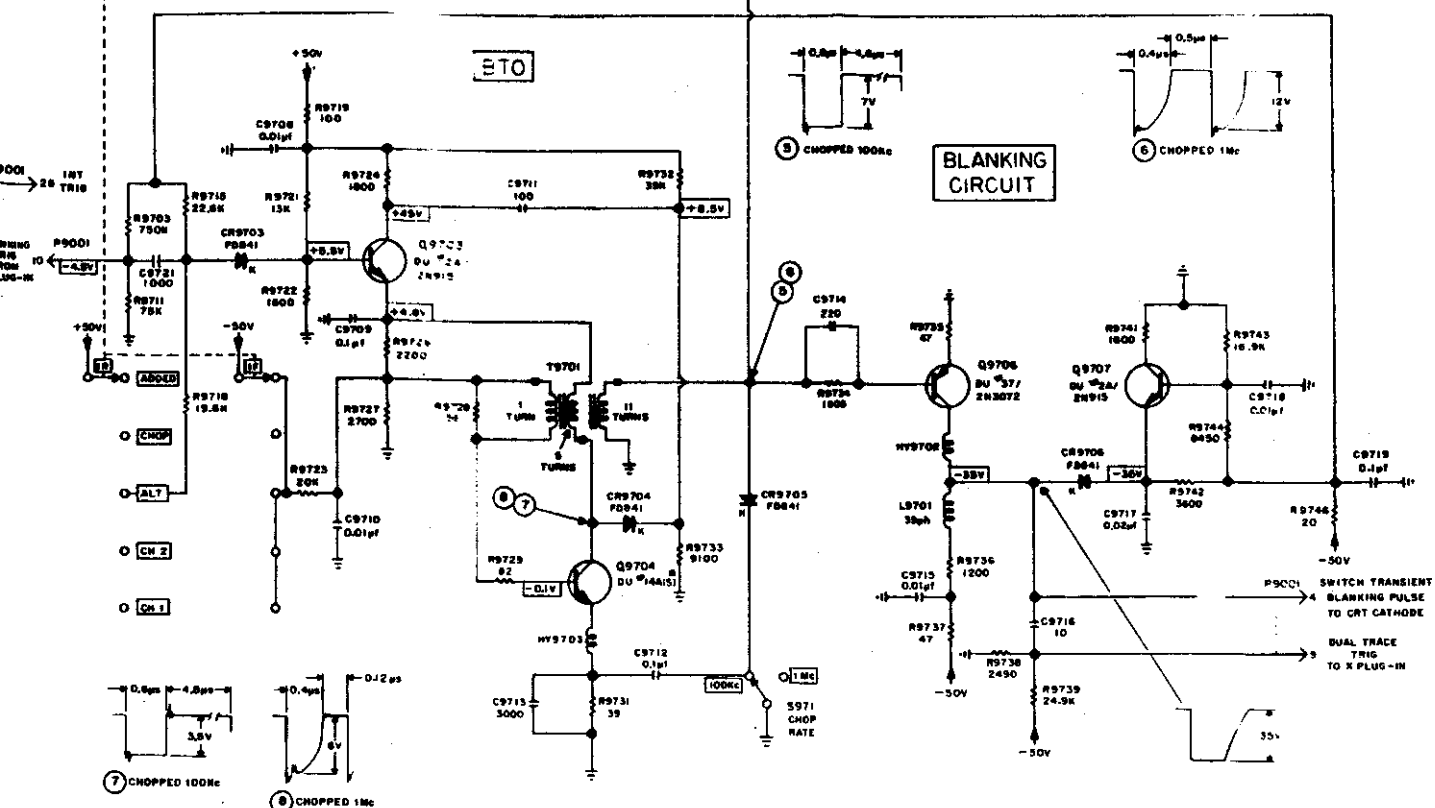
WAVEFORM DATA

- Voltage tolerance ±3% with respect to ground.
- Use Type 799A Probe (20).
- Use Type 746F Series Oscilloscope; DC to 100 Hz with MODE switch set to CW.
- Waveform amplitude measurements are nominal.



- VOLTAGE DATA**
- All voltage measurements were obtained with a 20,000 ohms/volts VOM; all readings are in volts.
 - Present front-panel controls are as follows:

Control	Setting
MODE	CH 1
VARIABLE POSITION	Fully on
Input Selector	Channel 1 (channel 2)
 - Voltage tolerance $\pm 1\%$ with respect to ground.
 - Use Type 79A Probe (E10).
 - Use Type 744/F Surface Oscilloscope; AC to 100 Mc with MODE switch set to CHOP.
 - Waveform amplitude measurements are nominal.



ADDENDUM

FOR

TYPE 79-02A DUAL TRACE PLUG-IN
Reference Manual Part Number 6704 5512

The following S numbers have been assigned to the selected transistors used in this unit.

A. PARTS LIST REVISIONS

<u>Symbol</u>	<u>Part Number</u>	<u>Description</u>
Q9205 to Q9208	CHANGE:	
Q9405 to Q9408		
Q9501, Q9502	2600 3071	DU14A Selected
Q9603, Q9604	2600 8190	DU14A
Q9704		
Q9801 to Q9804	TO READ:	
Q9901 to Q9904		
	2600 3071	Transistor S19128 Sel
	2600 3072	Alternate transistor S19926 Sel.
Q9503 to Q9508	CHANGE:	
Q9605		
Q9609, Q9610	2600 3071	DU14A Selected
Q9701, Q9702	2600 8190	DU14A
	TO READ:	
	2600 3071	Transistor S19128 Sel.

B. SCHEMATICS

Sheet 2, change Q9205, Q9206, Q9207, Q9208, Q9405, Q9406, Q9407, Q9408 from DU14A to S19128 (S) or S19926 (S).

Sheet 3, change Q9801, Q9802, Q9803, Q9804, Q9901, Q9902, Q9903, Q9904, Q9501, Q9502 from DU14A to S19128 (S) or S19926 (S).
Change Q9503, Q9504, Q9505, Q9506, Q9507, Q9508 from DU14A to S19128 (S).

Sheet 4, change Q9605, Q9609, Q9610, Q9701, Q9702 from DU14A to S19128 (S). Change Q9603, Q9604, Q9704 from DU14A to S19128 (S) or S19926 (S).

FAIRCHILD

INSTRUMENTATION

6704 8341
Sheet 1 of 1
PCN #32,494

ADDENDUM
FOR
TYPE 79-02A DUAL TRACE PLUG-IN
(Reference Manual Part Number 6704 5512)

A. PURPOSE

The following change was made to improve the pulse response and to eliminate compression of signal when positioning signal off-screen vertically.

B. PARTS LIST REVISIONS

In Section 6 make the following changes:

1. Change part number of transistors Q9201 thru Q9204 and Q9401 thru Q9404 from 26003084 to 26003111.
2. Change part number and value of resistor R9523 from 02364890, 150 ohms, to 02364720, 100 ohms.
3. Delete networks, peaking, Z9201, Z9202, Z9401 and Z9402.
4. Add coils L9201, L9202, L9401 and L9402, part number 21019511 and description "coil, 85 nanohenries."
5. Add the following part number and description for transistors Q9209, Q9210, Q9409 and Q9410: "26003111, alternate DU#12A (selected)."

C. SCHEMATIC REVISIONS

1. On schematic "Channel 1 and 2 Preamplifiers" sheet 2 of 4, make the following changes:
 - a. Delete reference designations Z9201, Z9202, Z9401 and Z9402 and dashed rectangle.
 - b. Delete reference "R1, 390K" and "L1, 5 turns."
 - c. Delete R1 resistor symbol.
 - d. To remaining coil symbols add reference designations and values as follows:

<u>Before</u>	<u>After</u>
Z9201, Z9202	L9201, L9202 85 nh
Z9401, Z9402	L9401, L9402 85 nh

2. On schematic "Vertical Deflection Amplifier" sheet 3 of 4, change resistor value of R9523 from 150 ohms to 100 ohms.

FAIRCHILD

INSTRUMENTATION

A DIVISION OF FAIRCHILD CAMERA AND INSTRUMENT CORPORATION

6704 8251
Sheet 1 of 1
ECN 32,461

ADDENDUM

FOR

TYPE 79-02A DUAL TRACE PLUG-IN (Reference Manual Part Number 6704 5512)

A. PURPOSE

The following change was made to change CH 1 Input Selector switch to eliminate oscillations when tandem operating the amplifiers for greater input sensitivity.

B. TEXT REVISIONS

1. On Page 1-3 under "Input Selector Switch" heading, change to read as follows:

...Each channel is provided with a 3-position lever switch which permits selection of DC or AC coupling and ground. The GND position provides a base line reference and disconnects the input signal. ...

2. On Page 1-4 under "High Sensitivity Amplifier", change "an internal connection" etc. to read "an external connection" etc.
3. On Page 2-4 under paragraph 2-5 delete first major paragraph referencing channel 1 input selector switch.
4. On Page 2-22, paragraph 2-11 change first paragraph to read as follows:

...The Type 79-02A Dual Trace Amplifier may be set up to provide an input sensitivity of 1 millivolt/division with an accompanying reduction in bandwidth to 25 MHz. This is accomplished by interconnecting the CH 2 OUTPUT connector to CH 1 input connector through a short length of coaxial cable and setting the channels for X10 operation by pulling the VARIABLE controls (Pull X10) out. The output of CH 2 amplifier is now connected in series with the input of CH 1 amplifier. ...
5. Delete reference to CH 2 at CH 1 Input Selector switch, Figures 1-1, 2-1, 2-2, 2-3, 3-1, 3-6 and 6-1.
6. In Figure 6-1 change front panel part number to 3201 3772.

FAIRCHILD

INSTRUMENTATION

A DIVISION OF FAIRCHILD CAMERA AND INSTRUMENT CORPORATION

6704 8321
Page 1 of 2
PCN 32,492

C. PARTS LIST REVISIONS

In Section 6 make the following changes:

DELETE:

<u>Symbol</u>	<u>Part Number</u>	<u>Description</u>	<u>Code</u>	<u>Type</u>
C9615*	0315 2100	10 pf, <u>+10%</u>	ERC	NPO 331
R9602	0236 4690	93.1, <u>+1%</u>	CGW	NS 20
R9605	0234 7970	100	CGW	C20
R9625	0235 4440	composition, 180, 1/4W	ALB	CB
R9621*	0234 8140	510	CGW	C20
S901	0501 7461	lever, 1 section, 4 pos.	FC1	

ADD:

C9618	0319 1070	0.005 uf, 150V		
R9602	0236 4720	100, 1%		
R9625	0235 4460	220		
S901	0501 7451	lever, 1 section, 3 pos.	FC1	

D. SCHEMATIC REVISIONS

1. On Schematic "CH 1 and 2 Attenuators", sheet 1 of 4, delete CH 2 position from S901 and reference to CH 2 output.
2. On Schematic "Trigger & Blanking Circuit", sheet 4 of 4:
 - a. Delete resistor R9605, its connection and reference
 - b. Delete resistor R9621, capacitor C9615 and reference to test option
 - c. Change resistor R9602 value from 93.1 to 100
 - d. Change resistor R9625 value from 180 to 220
 - e. Add capacitor C9618, 0.005 uf in parallel with resistor R9601.