## OPERATING AND SERVICE MANUAL

# RF SECTION 1-1300 M Hz 86602B <br> Including Options 001 and 002 

## SERIAL NUMBERS

This Manual applies directly to instruments with serial numbers prefixed 1519A.

With the changes described in Section VII, this manual also applies to instruments with serial numbers prefixed 1433A.

For additional important information about serial numbers, see INSTRUMENT COVERED BY MANUAL in Section I.
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Thanks


Dave \& Lynn Henderson
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## WARNINGS

## CAUTIONS

## SAFETY

Although this instrument has been designed in accordance with international safety standards, this manual contains information, cautions, and warnings which must be followed to retain the instrument in safe condition. Be sure to read and follow the safety information in Sections II, III, V, and VIII.

BEFORE CONNECTING THIS SYSTEM TO LINE (MAINS) VOLTAGE, the safety and installation instructions found in Sections II and III of the mainframe manual should be followed.

## HIGH VOLTAGE

Adjustments and troubleshooting are often performed with power supplied to the instrument while protective covers are removed. Energy available at many points may constitute a shock hazard.

The multi-pin plug connector which provides interconnection from mainframe to RF Section, will be exposed with the RF Section removed from the right-hand mainframe cavity. With the Line (Mains) Voltage off and power cord disconnected, power supply voltages may still remain and may constitute a shock hazard.

## COMPATIBILITY

Damage to the synthesized signal generator system may result if an option 002 RF Section is used with unmodified Model 8660A or 8660B mainframes with serial prefixes 1349A and below.

## PERFORMANCE TESTING

To avoid the possibility of damage to the instrument or test equipment, read completely through each test before starting it. Then make any preliminary control settings necessary before continuing whth the procedure.

## PLUG-IN REMOVAL

Before removing the RF Section plug-in from the mainframe, remove the line (Mains) voltage by disconnecting the power cable from the power outlet.

## SEMI-RIGID COAX

Slight but repeated bending of the semi-rigid coaxial cable will damage them very quickly. Bend the cables as litte as possible. If necessary, loosen the assembly to release the cable.

MODEL 86602B

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## SECTION I <br> GENERAL INFORMATION

## 1-1. INTRODUCTION

1-2. This manual contains all information required to install, operate, test, adjust and service the Hewlett-Packard Model 86602B RF Section plug-in, hereinafter referred to as the RF Section. For information concerning related equipment, such as the Hewlett-Packard Model 8660 -series mainframes or the Model 11661 Frequency Extension Module, refer to the appropriate manual or manuals.

1-3. This manual is divided into eight sections which provide information as follows:
a. SECTION I, GENERAL INFORMATION, contains the instrument description and specifications as well as the accessory and recommended test equipment list.
b. SECTION II, INSTALLATION, contains information relative to receiving inspection, preparation for use, mounting, packing, and shipping.
c. SECTION III, OPERATION, contains operating instructions for the instrument.
d. SECTION IV, PERFORMANCE TESTS, contains information required to verify that instrument performance is in accordance with published specifications.
e. SECTION V, ADJUSTMENTS, contains information required to properly adjust and align the instrument after repair.
f. SECTION VI, REPLACEABLE PARTS, contains information required to order all replacement parts and assemblies.
g. SECTION VII, MANUAL CHANGES, is reserved to provide backdating and for modification information in late editions of this manual.
h. SECTION VIII, SERVICE, contains descriptions of the circuits, schematic diagrams, parts location diagrams, and troubleshooting procedures to aid the user in maintaining the instrument.

1-4. Figure 1-1 shows the Option 002 RF Section.
1-5. Packaged with this manual is an Operating Information Supplement. This is simply a copy of the first three sections of this manual. This supplement should stay with the instrument for use by the operator. Additional copies of the Operating Information Supplement may be ordered separately through your nearest HewlettPackard office. The part number is listed on the title page of this manual.
$1-6$. On the title page of this manual, below the manual part number, is a "Microfiche" part number. This number may be used to order 4 x 6 -inch microfilm transparencies of the manual. Each microfiche contains up to 60 photoduplicates of the manual pages. The microfiche package also includes the latest Manual Changes supplement as well as all pertinent Service Notes.

## 1-7. SPECIFICATIONS

1-8. Instrument specifications are listed in Table 1-1. These specifications are the performance standards, or limits against which the instrument may be tested.

## 1-9. INSTRUMENTS COVERED BY MANUAL

1-10. This instrument has a two-part serial number. The first four digits and the letter comprise the serial number prefix. The last five digits form the sequential suffix that is unique to each instrument. The contents of this manual apply directly to instruments having the same serial number prefix(es) as listed under SERIAL NUMBERS on the title page.

1-11. For information concerning a serial number prefix not listed on the title page or in the Manual Changes supplement, contact your nearest HewletiPackard office.

## 1-12. MANUAL CHANGE SUPPLEMENTS

1-13. An instrument manufactured after the printing of this manual may have a serial prefix that is not listed on the title page. This unlisted serial

Table 1-1. Models $86602 B / 11661$ Specifications (1 of 3)

## SPECIFICATIONS

## FREQUENCY CHARACTERISTICS

Range: 1.0 to 1299.999999 MHz selectable in 1 Hz steps. Frequencies from 200 kHz to 1 MHz may also be selected with some degradation in specifications.

Accuracy and Stability ${ }^{1}$ : CW frequency accuracy and long term stability are determined by the aging rate of the time base (internal or external) and its sensitivity to changes in temperature and line voltage. Internal reference oscillator accuracy $= \pm$ aging rate $\pm 3 \times 10^{-10} /{ }^{\circ} \mathrm{C} \pm 3 \times 10^{-10} / 1 \%$ change in line voltage.

Switching Time: 6 ms to be within 50 Hz of any new frequency selected; 100 ms to be within 5 Hz of any new frequency selected.

| Largest Digit Changed | Error at: |  |
| :---: | :---: | :---: |
|  | 1 ms | 1 ms |
| 1 Hz <br> 10 Hz | $<1 \mathrm{~Hz}$ | $<1 \mathrm{~Hz}$ |
| 100 Hz | $<100 \mathrm{~Hz}$ | $<1 \mathrm{~Hz}$ |
| 1 kHz <br> 10 kHz | $<500 \mathrm{~Hz}$ | $<10 \mathrm{~Hz}$ |
| 100 kHz <br> 1 MHz | $<500 \mathrm{~Hz}$ | $<50 \mathrm{~Hz}$ |
| 10 MHz | $<500 \mathrm{~Hz}$ | $<50 \mathrm{~Hz}$ |
| 100 MHz, <br> 1 GHz | Undefined | $<50 \mathrm{~Hz}$ |

Typical 86602B/11661
Frequency Switching Characteristics

## Harmonic Signals:

All harmonically related signals are at least 30 dB below the desired output signal for output levels $\leqslant+3 \mathrm{dBm}$. ( 25 dB down for output levels above +3 dBm .)

Spurious Signals (CW, AM, and $\phi$ M only):
80 dB down from carrier at frequencies $<700 \mathrm{MHz}$
80 dB down from carrier within 45 MHz of the carrier at frequencies $\geqslant 700 \mathrm{MHz}$
70 dB down from carrier $>45 \mathrm{MHz}$ from carrier at frequencies $\geqslant 700 \mathrm{MHz}$
50 dB down from carrier on the +10 dBm range.

All Power Line Related spurious signals are 70 dB down from carrier.

## Residual FM (CW, AM, and 2nd $\phi$ M only):

$<1.5 \mathrm{~Hz}-\mathrm{rms}$ in 2 kHz band centered on the carrier.
Signal-to-Phase Noise Ratio (CW, AM, and $\phi \mathbf{M}$ only):
Greater than 45 dB in a 30 kHz band centered on the carrier and excluding a 1 Hz band centered on the carrier.

## Typical SSB Phase Noise Curve:



Typical 86602B Phase Noise

Signal-to-AM Noise Ratio: Greater than 65 dB down in a 30 kHz bandwidth centered on the carrier and excluding a 1 Hz band centered on the carrier

[^0]Table 1-1. Models 86602B/11661 Specifications (2 of 3)

## OUTPUT CHARACTERISTICS

Level: Continuously adjustable from +10 to -146 dBm ( 0.7 Vrms to $0.01 \mu \mathrm{Vrms}$ ) into a $50 \Omega$ resistive load. Output attenuator calibrated in 10 dB steps from 1.0 V full scale ( +10 dBm range) to $0.03 \mu \mathrm{Vrms}$ full scale ( -140 dBm range). Vernier provides continuous adjustment between attenuator ranges. Output level indicated on output level meter calibrated in volts and dBm into 50 ohms.

Accuracy: (Local and remote modes) $\pm 1.5 \mathrm{~dB}$ to $-76 \mathrm{dBm} ; \pm 2.0 \mathrm{~dB}$ to -146 dBm at meter readings between +3 and -6 dB .

Flatness: Output level variation with frequency is less than $\pm 1.0 \mathrm{~dB}$ from $1-1300 \mathrm{MHz}$ at meter readings between +3 and -6 dB .

Level Switching Time: In the remote mode any level change can be accomplished in less than 50 ms . Any change to another level on the same attenuator range can be accomplished in less than 5 ms .

Impedance: $50 \Omega$.
VSWR: $<2.0$ on +10 and 0 dBm range; $<1.3$ on -10 dBm range and below.

## MODULATION CHARACTERISTICS

(With compatible Modulation Sections)

## Amplitude Modulation:

Depth: $0-90 \%$ for RF output level meter readings from +3 to -6 dB and only at +3 dBm and below.

AM 3 dB Bandwidth:

| Center <br> Frequency | AM 3 dB Bandwidth |  |  |
| :--- | :---: | :---: | :---: |
|  | $\mathbf{0}$ to $\mathbf{3 0 \%}$ AM | $\mathbf{0}$ to 70\% AM | $\mathbf{0}$ to $\mathbf{9 0 \%}$ AM |
| $<10 \mathrm{MHz}$ | 10 kHz | 6 kHz | 5 kHz |
| $\geqslant 10 \mathrm{MHz}$ | 100 kHz | 60 kHz | 50 kHz |


| AM Total Harmonic Distortion $^{2}$ |  |  |
| :---: | :---: | :---: |
| AT 30\% AM | AT 70\% AM | AT 90\% AM |
| $<1 \%$ | $<3 \%$ | $<5 \%$ |



Typical AM Distortion (Center Frequency $<10 \mathrm{MHz}$ )


Typical AM Distortion (Center Frequency $\geqslant 10 \mathrm{MHz}$ )

Incidental PM: Less than 0.2 radians peak at $30 \%$ AM.
Incidental FM: Less than 0.2 times the frequency of modulation ( Hz ) at $30 \% \mathrm{AM}$.

[^1]Table 1-1. Models 86602B/11661 Specifications (3 of 3)

## FREQUENCY MODULATION

Rate: DC to 200 kHz with the 86632 B and 86635 A . 20 Hz to 100 kHz with the 86633B.

## Maximum Deviation (peak):

200 kHz with the 86632B and 86635A
100 kHz with the 86633B

Incidental AM: AM sidebands are greater than 60 dB down from the carrier with 75 kHz peak deviation at a 1 kHz rate.

FM Total Harmonic Distortion (at rates up to 20 kHz); $<1 \%$ up to 200 kHz deviation. (External modulating signal distoriton must be less than $0.3 \%$.)


## Typical FM Distortion Curve

PULSE MODULATION
(With the 86631B Auxiliary Section only)
Source: External

Rise/Fall Time: 50 ns.

ON/OFF Ratio: At least 40 dB .
Input Level Required: 8 to 10 V negative voltage turns RF on.

## PHASE MODULATION

(Option 002 Instruments only)
Rate:
with 86635 A dc to 1 MHz
with 86634A
dc to 1 MHz at center frequencies less than 100 MHz dc to 10 MHz at center frequencies greater or equal to 100 MHz .

## Maximum Peak Deviation:

0 to 100 degrees peak. May be overdriven to 2 radians $\left(115^{\circ}\right)$ in the Modulation Section's external dc mode.

## $\phi$ M Distortion:

$<5 \%$ up to 1 MHz rates
$<7 \%$ up to 5 MHz rates
$<15 \%$ up to 10 MHz rates
(External modulation signal distortion must be less than $0.3 \%$ to meet this specification.)

## REMOTE PROGRAMMING

(Through the 8660 -series mainframes)
Frequency: Programmable in 1 Hz steps.
Output Level: Programmable in 1 dB steps from +10 to -146 dBm .

Modulation: See specifications for modulation section installed.

## GENERAL

Leakage: Meets radiated and conducted limits of MIL-I-6181D.

Size: Plug-in to fit 8660 -series mainframe.
Weight: Net $9 \mathrm{lb}(3.9 \mathrm{~kg})$.
prefix indicates that the instrument is different from those documented in this manual. The manual for this instrument is supplied with a yellow Manual Changes supplement that contains "change information" that documents the differences.

1-14. In addjtion to change information, the supplement may contain information for correcting errors in the manual. To keep this manual as current and accurate as possible, Hewlett-Packard recommends that you periodically request the latest Manual Changes supplement. The supplement for this manual is keyed to this manual's print date and part number, both of which appear on the title page. Complimentary copies of the supplement are available from Hewlett-Packard.

## 1-15. DESCRIPTION

1-16. The HP Model 86602B RF Section is one of several RF Sections available for use in an 8660 -series Synthesized Signal Generator System. This RF Section plug-in is used with an option 100 8660-series mainframe (Frequency Extension Module installed). The RF Section provides precisely tuned RF output frequenices over the 1 to 1300 MHz range with 1 Hz frequency resolution ( 8660 -series option 004 instruments have resolutions of 100 Hz .) Frequencies from 200 kHz to 1 MHz can also be generated with some degradation in the amplitude leveling and other related specifications.

1-17. The output power can be set to any level between +10 and --146 dBm by means of the front panel VERNIER and calibrated OUTPUT RANGE controls. A front panel-mounted meter and the OUTPUT RANGE switch indicate the output power and voltage levels delivered by the RF Section to any external load having a characteristic impedance of 50 ohms. Output power levels are maintained within $\pm 1 \mathrm{~dB}$ of selected values through internal leveling of the output signal over the full frequency range of the instrument.

1-18. Amplitude, frequency, phase, or pulse modulation of the RF OUTPUT signal can be accomplished within the RF Section by using the appropriate Auxiliary or Modulation Section plug-in.

1-19. External programming permits remote selection of the output signal frequency in 1 Hz steps ( 100 Hz for option 004 mainframes) and the output power in 1 dB steps over the full operating
range of the instrument. External programming is accomplished via the mainframe computercompatible interface and digital control unit circuits.

## 1-20. OPTIONS

1-21. This RF Section has two options available. They affect the instrument's RF output level, and phase modulation capabilities.

1-22. Option 001. The RF output attenuator is removed. This limits the RF output level range from +10 to -6 dBm .

1-23. Option 002. Circuits are added to provide the phase modulation capability. A compatible modulation section is required.

## 1-24. COMPATIBILITY

1-25. Except for Option 002 instruments, the Model 86602B is compatible with all 8660 -series option 100 mainframes, all AM-FM Modulation Sections and the Auxiliary Section. This RF Section is partially compatible with the $\mathrm{FM} / \phi \mathrm{M}$ Modulation Section.

## CAUTION

## Damage to the signal generator system may result if an option 002 RF Section is used with Model 8660A or 8660B mainframes with serial prefixes 1349A and below.

1-26. Option 002 instruments are compatible with all instruments which are part of the Model 8660 -series Synthesized Signal Generator System except early model 8660A and 8660B Mainframes. Refer to the paragraph entitled Modifications in Section II of this manual for further information.

## 1-27. EQUIPMENT REQUIRED BUT NOT SUPPLIED

## 1-28. System Mainframe

1-29. The mainframe uses phase-locked loops to accurately generate clock, reference, and tuning signals required for operation of the Synthesized Signal Generator System. Front panel-mounted mainframe controls are used to digitally tune two phase-locked loops in the Frequency Extension Module which, in turn, produce two highfrequency output signals that are applied to the RF Section. The RF Section mixes the two signals
and presents their frequency difference at the front panel OUTPUT jack. The output frequency is either the value selected by the mainframe front panel controls or external programming.

1-30. The mainframe power supply provides all dc operating voltages required by the RF Section, Frequency Extension Module, and Modulation Section plug-ins. Remote programming of the plugins is accomplished via the mainframe interface and digital control unit circuits.

## 1-31. Frequency Extension Module

1-32. The Frequency Extension Module plug-in extends the output frequency range of the mainframe to meet the input requirements of the RF Section. The Frequency Extension Module plug-in contains two high-frequency phase-locked loops which receive digital tuning signals, variable synthesized signals, and fixed synthesized signals from the mainframe. The phase-locked loops use the mainframe signals, in conjunction with the output frequency from a 4.43 GHz oscillator that is common to both loops, to produce two highfrequency output signals that are supplied to the RF Section. One output signal is generated by a phase-locked loop using a Voltage Controlled Oscillator (VCO) that is tuneable in 1 Hz steps ( 100 Hz steps for option 004 mainframe) over the 3.95 to 4.05 GHz range. The other output signal is generated by a phase-locked loop using a Yittrium-Iron-Garnet (YIG) oscillator that is tunable in 100 MHz steps over the 3.95 to 2.75 GHz range. The two outputs from the Frequency Extension Module plug-in are applied to the RF Section for mixing, amplification of the converted signal, and final output power level control.

## 1-33. Auxiliary Section

1-34. The Auxiliary Section plug-in provides a means of applying externally generated amplitude or pulse modulation drive signals to modulate the RF Section's output carrier.

## 1-35. Modulation Section Plug-ins

$1-36$. The Model 86630 -series Modulation Section plug-ins can accept external modulation drive signals or generate internal drive signals to amplitude, frequency, phase or pulse modulate the RF Sections output signal.

## 1-37. EQUIPMENT AVAILABLE

1-38. Extender cables, coaxial adapters, and an adjustment tool are available for use in performance testing, adjusting, and maintaining the RF Section. Each piece may be ordered separately or as part of the 11672A Service Kit.

1-39. Extender cards for use in servicing the RF Section and a type N to BNC adapter for use on the front panel RF OUTPUT connector are contained in the HP Rack Mount Kit, Part Number 08660-60070, that is supplied with the mainframe.

## 1-40. SAFETY CONSIDERATIONS

1-41. This instrument has been designed in accordance with international safety standards and has been supplied in safe condition.

1-42. Although this instrument has been designed in accordance with international safety standards, this manual contains information, cautions, and warnings which must be followed to retain the instrument in safe condition. Be sure to read and follow the safety information in Sections II, III, V , and VIII.

## 1-43. RECOMMENDED TEST EQUIPMENT

1-44. Table 1-2 lists the test equipment and accessories recommended for use in testing, adjusting, and servicing the RF Section. If any of the recommended test equipment is unavailable, instruments with equivalent specifications may be used.

Table 1-2. Recommended Test Equipment (1 of 4)

| Item | Critical Specifications | Suggested Model | Use* |
| :---: | :---: | :---: | :---: |
| Adapter (Male Type N to GR874) | Frequency range 100 MHz to 1.3 GHz | HP 1250-0847 | P |
| Adapter, SMA-to-BNC | 2 required | OSM 21190 | P |
| Adapter, SMA-to-OSM Right Angle |  | OSM 219 | P |
| Adapter, Type N-toSMA |  | OSM 21040 | P |
| Amplifier, 20 dB | $\begin{aligned} & \approx 20 \mathrm{~dB} \text { gain at } 30 \mathrm{MHz} \\ & \text { Input } \mathrm{SWR}<1.7 \end{aligned}$ | HP 8447A | P |
| Amplifier, 40 dB | Special | (see Figure 1-2) | P |
| Analyzer, Distortion | 20 Hz to 20 kHz ; must measure $<0.1 \%$ distortion | HP 333A | P |
| Analyzer, Spectrum | Measurement Accuracy $\pm 2.0 \mathrm{~dB}$ from 1 kHz to 110 MHz | HP 8553B with HP 8552B and HP 140T | P, A |
| Analyzer, Spectrum | Measurement Accuracy $\pm 2.0 \mathrm{~dB}$ from 10 MHz to 8 GHz | HP 8555A with HP 8552B and HP 140T | P, A, T |
| Analyzer, Wave | Center frequencies 20 to 40 kHz <br> Resolution bandwidth $\leqslant 3 \mathrm{~Hz}$ <br> Bandpass shape factor $10: 1$ <br> Analog output 0 to 5 V <br> Noise level (at 11 kHz center frequency with a 3 Hz bandwidth) $<-150 \mathrm{dBV}$ | HP 3581A | P |
| Attenuator, 3 dB Fixed | 3 dB | HP 8491A Option 003 | P |
| Attenuator, 10 dB Step | Calibrated at 30 MHz ; refer to calibration curve | HP 355D-H38 (only) | P, A |
| Attenuator, 40 dB Fixed | 40 dB | HP 8491A Option 040 | P |
| Cables, Double Shielded | Minimum input $\leqslant 300 \mathrm{mVrms}$ ( 5 required) | HP 08708-6033 | P |
| Capacitor, 1500 pF |  | HP 0160-2222 | P |
| Capacitor, $100 \mu \mathrm{~F}$ |  | HP 0180-2207 | P |
| Connector, BNC Panel Mount |  | HP 1250-0118 | T |
| * Use: $\mathbf{P}=$ Performance Tests, $\mathrm{A}=$ Adjustments, $\mathbf{T}=$ Troubleshooting |  |  |  |

Table 1-2. Recommended Test Equipment (2 of 4)

| Item | Critical Specifications | Suggested Model | Use* |
| :---: | :---: | :---: | :---: |
| Counter, Computing | 50 kHz to 50 MHz with a 1 ms gate time and external trigger; 1 Hz resolution | HP 5360A with HP 5365A plug-in | P |
| Counter, Frequency | Range: $0.2-1300 \mathrm{MHz}$ <br> Resolution: 1 Hz <br> 10 MHz external reference output <br> 7.2 Vrms output into 170 ohms | HP 5340A | P |
| Coupler, Directional | Frequency range 100 MHz to 1.3 GHz | HP 778D Option 12 | P |
| Detector, Crystal | 1 to 1200 MHz | HP 8471A | P |
| Detector, Crystal | 10 MHz to 1.3 GHz | HP 423A | P, A |
| FM Discriminator | Input frequency 100 kHz to 10 MHz Linear Analog Output 1 V full scale | HP 5210A | P, A |
| Filter, Low Pass, 15 kHz | Special | (see Figure 1-3) | P |
| Filter, Low Pass, 4 MHz | Cutoff frequency: 4 MHz | $\begin{aligned} & \text { CIR-Q-TEL } \\ & \text { FLT } / 21 \mathrm{~B}-4-3 / 50-3 \mathrm{~A} / 3 \mathrm{~B} \end{aligned}$ | P |
| Filter, Low Pass, 2200 MHz | Cutoff frequency: 2200 MHz | HP 360C | P |
| Filters, Low Pass, 100 kHz | 100 kHz at 50 and 600 ohms | Specials (See Figure 1-4) | A |
| Filters, Low Pass, 1 MHz | $1 \mathrm{MHz}-50$ and 600 ohms | Specials (See Figures 1-4) | P, A |
| Filters, Low Pass, 5 and 10 MHz | 5 and $10 \mathrm{MHz}-50$ ohms | Specials (See Figure 1-4) | P |
| Generator, Function | Distortion less than $0.3 \%$ <br> Range: 0.5 Hz to 20 kHz <br> Output level: 0.1 to 2.0 Vrms into 600 ohms | HP 203A | P |
| Generator, Pulse | Output - 10 Vpk with $\leqslant 10$ ns risetime in 600 ohms | HP 8013B | P |
| Generator, Sweep | Sweep Width 0.1 to 100 MHz Output Level +20 to -80 dBm Flatness $\pm 0.25 \mathrm{~dB}$ | HP 8601A | A |
| Generator, Synthesized Signal | +1 Hz from 1 MHz to 1300 MHz <br> +7 dBm output <br> 10 MHz Reference output <br> $>0.5 \mathrm{~V}$ into 170 ohms | HP 8660 with HP 86631 B and HP 86602B plug-ins | P, A |

Table 1-2. Recommended Test Equipment (3 of 4)

| Item | Critical Specifications | Suggested Model | Use* |
| :---: | :---: | :---: | :---: |
| Mixer, Double Balanced | 1 MHz to 110 MHz | HP 10514A | A |
| Mixer, Double Balanced | 300 to 1300 MHz | Watkins-Johnson M1J | P |
| Oscillator, Test | 1 kHz to 10 MHz <br> 1.0 to 2.0 Vrms into 600 or 50 ohms | HP 651B | P, A |
| Oscilloscope | Vertical: <br> Bandwidth 50 MHz with sensitivity of 5 mV / division minimum Horizontal: Sweep time 10 ns to 1 s Delayed sweep External triggering to 100 MHz | HP 180C with HP 1801A and HP 1821A plug-ins | P, A, T |
| Oscilloscope, 10:1 divider probes | Input impedance 10 megohm shunted by 10 pF | HP 10004 | $\mathrm{P}, \mathrm{A}, \mathrm{T}$ |
| Power Meter/Sensor | Range: -10 to +10 dBm from 10 MHz to 1.3 GHz | HP 435A/8481A | P, A, T |
| Power Supply, DC | $0-10$ volts | HP 721A | P |
| Programmer, Marked Card | Capable of programming BCD or HP-IB data | HP 3260A Option 001 | P, A |
| Probe, Logic | TTL Compatible | HP 10525T | T |
| Resistor, 1000 ohm | $\pm 2 \%$ | HP 0757-0280 | P, A |
| Resistor, 10 K ohm | $\pm 2 \%$ | HP 0757-0442 | P |
| Resistor, 100 K ohm | $\pm 2 \%$ | HP 0698-7284 | P |
| Service Kit | Interconnect cables, adaptors, and coaxial cables compatible to 8660 -series plus and jacks | HP 11672A (See Operating Note or mainframe manual for parts list) | A, T |
| Stub, Adjustable | Frequency range 100 MHz to 1.3 GHz | General Radio 874-D50L | P |
| Tee, Coaxial | 2 required | HP 1250-0781 (BNC) | P, A |
| Termination, 50 ohm Feed Thru | 50 ohm | HP 11048C | P |
| * Use: $\mathbf{P}=$ Performance, $\mathrm{A}=$ Adjustments, $\mathrm{T}=$ Troubleshooting |  |  |  |

Table 1-2. Recommended Test Equipment (4 of 4)

| Item | Critical Specifications | Suggested Model | Use* |
| :---: | :---: | :---: | :---: |
| Termination, 50 ohm | 50 ohm , (2 required) | HP 11593A | P |
| Test Set, Phase Modulation | Input Frequency Range 250 to 950 MHz Distortion <br> $<2 \%$ up to 2 MHz rates <br> $<3.5 \%$ up to 5 MHz <br> $<5.0 \%$ up to 10 MHz | HP 8660C-K10 (only) | P, A |
| Voltmeter, AC | Accuracy $\pm 2 \%$ of full scale from 1 Hz to 1 MHz <br> 1 mVrms to 10 Vrms full scale | HP 403B | P, A, T |
| Voltmeter, Digital | ```Range 0.00 to 60.00 volts DC Accuracy \(\pm(0.3 \%\) of reading \(+0.01 \%\) of range) AC Accuracy \(\pm(0.25 \%\) of reading \(+0.05 \%\) of range) 45 Hz to 20 kHz``` | HP 34740A/34702A | P, A, T |
| Voltmeter, Vector | Frequency range 5 to 15 MHz Input level 100 mVrms to 1 Vrms Analog output: $\pm 0.5$ Vdc for $\pm 180^{\circ}$ | HP 8405A | P |

[^2]
## 40 dB TEST AMPLIFIER



Amplifier Specifications

| Gain | 44 dB at $25^{\circ} \mathrm{C}$ |
| :--- | :--- |
| Bandwidth | $100 \mathrm{kHz}(3 \mathrm{~dB}$ down $)$ |
| Noise Bandwidth | 157 kHz |
| Input Impedance | 75 K Ohms |
| Output Impedance | 12 K Ohms |
| Current Drain | 260 Microamperes |
| Output (Maximum) | 1 Volt |
| Dynamic Range | 66 dB |

Figure 1-2. 40 dB Test Amplifier

## 15 kHz LPF



Figure 1-3. 15 kHz Low Pass Filter

## LOW PASS FILTERS



|  | $100 \mathrm{kHz}-\mathbf{5 0}$ ohms |  |  |
| :--- | :--- | :--- | :--- |
|  |  |  |  |
| C1, C4 | $0.015 \mu \mathrm{~F}$ | Mylar | $0160-0194$ |
| C2 | $0.027 \mu \mathrm{~F}$ | Mylar | $0170-0066$ |
| C3 | $0.022 \mu \mathrm{~F}$ | Mylar | $0160-0162$ |
| L1, L2 | $100 \mu \mathrm{H}$ | $9140-0210$ |  |

1 MHz - 50 ohms

| C1, C4 | 1500 pF | $0160-2222$ | C1, C4 130 pF | $0140-0195$ |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| C2 | 3300 pF | $0160-2230$ | C2 | 300 pF | $0160-2207$ |
| C3 | 1600 pF | $0160-2223$ | C3 | 110 pF | $0140-0194$ |
| L1, L2 | $10 \mu \mathrm{H} \pm 10 \%$ | $9140-0114$ | L1, L2 $120 \mu \mathrm{H}$ | $9100-1637$ |  |

5 MHz - 50 ohms
$10 \mathrm{MHz}-50$ ohms

| C1, C2, C4 | 300 pF | $0160-2207$ |
| :--- | :--- | :--- |
| C3 | 680 pF | $0160-3537$ |
| L1, L2 | $2 \mu \mathrm{H}$ | $9100-3345$ |


| C1, C4 | 150 pF | $0140-0196$ |
| :--- | :--- | :--- |
| C2 | 330 pF | $0160-2208$ |
| C3 | 160 pF | $0160-2206$ |
| L1, L2 | $1 \mu \mathrm{H} \pm 10 \%$ | $9140-0096$ |

NOTE
Unless otherwise noted, tolerance of components is $\pm 5 \%$ and capacitors are mica. Part numbers are Hewlett-Packard

Figure 1-4. Low Pass Filters

# SECTION II <br> INSTALLATION 

## 2-1. INTRODUCTION

2-2. This section provides information relative to initial inspection, preparation for use, and storage and shipment of the Model 86602B RF Section plug-in. Initial Inspection provides instructions to be followed when an instrument is received in a damaged condition. Preparation For Use gives all necessary interconnection and installation instructions. Storage and Shipment provides instructions and environmental limitations pertaining to instrument storage. Also provided are packing and packaging instructions which should be followed in preparing the instrument for shipment.

## 2-3. INITIAL INSPECTION

2 -4. Inspect the shipping container for damage. If the shipping container or cushioning material is damaged, it should be kept until the contents of the shipment have been checked for completeness and the instrument has been checked mechanically and electrically. The contents of the shipment should be as shown in Figure 1-1, and procedures for checking electrical performance are given in Section IV. If the contents are incomplete, if there is mechanical damage or defect, or if the instrument does not pass the electrical performance test, notify the nearest Hewlett-Packard office. If the shipping container is damaged, or the cushioning material shows signs of stress, notify the carrier as well as the Hewlett-Packard office. Keep the shipping materials for carrier's inspection. The HP office will arrange for repair or repiacement without waiting for claim settlement.

## 2-5. PREPARATION FOR USE

## 2-6. Power Requirements

2-7. All power required for operation of the RF Section is furnished by the mainframe. This RF Section requires approximately 40 volt-amperes.

## 2-8. Interconnections

2-9. Prior to installing the RF Section plug-in into the mainframe, verify that the Frequency Extension Module plug-in and interconnecting cable assemblies have been installed in accordance with the instructions contained in the Frequency Extension Module manual.

## 2-10. Modifications

2-11. A power supply modification to older versions of Model 8660A and 8660B mainframes are required if they are to be used with the option 002 RF Section.


> Damage to the synthesized signal generator system may result if an option 002 RF Section is used with an older 8660 A or 8660 B mainframe.
$2-12$. Due to the increased power consumption of the option 002 instrument, mainframes with serial prefixes 1349 A and below must be modified by installing a Field Update Kit. For mainframe configurations other than option $003(60 \mathrm{~Hz}$ line operation), order kit number 08660-60273. For option 003 mainframes ( $50-400 \mathrm{~Hz}$ line operation) order kit number 08660-60274.

## NOTE

Verify that a new higher current fuse, HP Part Number 2110-0365, 4A Slow Blow, is used in mainframes with the power supply modification.

## 2-13. Operating Environment

2-14. The RF Section is designed to operate within the following environmental conditions:

Temperature . . . . . . . . . . . . . . . . . . $0^{\circ}$ to $+55^{\circ} \mathrm{C}$
Humidity less than $95 \%$ relative
Altitude less than 15,000 feet

## 2-15. Installation Instructions

## WARNING

The multi-pin plug connector which provides interconnection from mainframe to RF Section, will be exposed with the RF Section removed from the right-hand mainframe cavity. With the Line (Mains) Voltage off and power cord disconnected, power supply voltages may still remain which, if contacted, may constitute a shock hazard.

2-16. Insert the plug-in approximately half-way into the right cavity of the mainframe. Rotate the latch (lower right corner) to the left until it protrudes perpendicular to the front panel. Refer to Figure 2-1, which shows the plug-in partially inserted into the mainframe and the latch rotated to a position that is perpendicular to the plug-in front panel. Push the plug-in all the way into the mainframe cavity and then rotate the latch to the right until it snaps into position.

## 2-17. STORAGE AND SHIPMENT

## 2-18. Environment

$2-19$. The storage and shipping environment of the RF Section should not exceed the following limits:

Temperature $\qquad$ Humidity . . . . . . . . . . . . . . less than $95 \%$ relative Altitude . . . . . . . . . . . . . . . . less than 25,000 feet

## 2-20. Packaging

2-21. Original Type Packaging. Containers and materials identical to those used in factory packaging are available through Hewlett-Packard offices. If the instrument is being returned to Hewlett-Packard for servicing, attach a tag indicating the type of service required, return address, model number, and full serial number. Also mark
the container FRAGILE to assure careful handling. In any correspondence, refer to the instrument by model number and full serial number.

2-22. Other Packaging. The following general instructions should be used for re-packaging with commercially available materials:
a. Wrap the instrument in heavy paper or plastic. (If shipping to a Hewlett-Packard office or service center, attach a tag indicating the type of service required, return address, model number, and full serial number.)
b. Use a strong shipping container. A doublewall carton made of 350 -pound test material is adequate.
c. Use enough shock-absorbing material (3 to 4 -inch layer) around all the sides of the instrument to provide firm cushion and prevent movement inside the container. Protect the control panel with cardboard.
d. Seal the shipping container securely.
e. Mark the shipping container FRAGILE to assure careful handling.


Figure 2-1. RF Section Partially Inserted into Mainframe

## SECTION III OPERATION

## 3-1. INTRODUCTION

$3-2$. This section contains information which will enable the operator to learn to operate and quickly check for proper operation of the RF Section plug-in as part of the Synthesized Signal Generator System.

## 3-3. PANEL FEATURES

3-4. The front and rear panel controls, connectors, and indicators of the RF Section and its options are described by Figure 3-1 and 3-2.

## 3-5. OPERATOR'S CHECKS

3-6. The RF Section, as part of the Synthesized Signal Generator System, accepts inputs from the rest of the system but controls only the RF output level. Even though the controlled circuits for most other functions are within the RF Section, the actual checks are found in the manual of the instrument which controls that function.

3-7. The Operator's Checks in this manual are intended to verify proper operation of the circuits which control and are controlled by the RF output level controls. This includes the meter, the VERNIER control, the OUTPUT RANGE switch, and the Output Range Attenuator when operating in the local mode. When the system is being remotely controlled, the 1 dB and 10 dB remote step attentator switches are checked in place of the VERNIER control and OUTPUT RANGE switch. Refer to Figure 3-3.

## 3-8. OPERATING INSTRUCTIONS

$3-9$. In this system, the mainframe and plug-ins contain the controls for frequency, modulation, and RF level selection. The mainframe controls frequency, the Modulation Section plug-in controls modulation type and level, and the RF Section plug-in controls RF output level. The Operating Instructions for the RF Section plug-in are included in Table 3-1.

## FRONT PANEL FEATURES



## NOTE

The front panel of the option 002 instrument is shown. The standard instrument does not have the term PHASE MODULATION after $1-1300 \mathrm{MHz}$. The option 001 instrument has an OUTPUT RANGE switch which shows only the +10 and 0 dBm ranges.
(1) Meter. Indicates the RF Output level in Vrms and $\mathrm{dBm}(50 \Omega)$ with the scale reference indicated by the OUTPUT RANGE switch.

2 Mechanical Meter Zero Control. Sets the Panel Meter indicator to zero when the mainframe LINE Switch is set to STBY.
(3) output range Switch. Sets the output level range of all except option 001 instruments from
+10 to $-140 \mathrm{dBm}(50 \Omega)$ in 10 dB steps. For option 001 instruments, +10 and 0 dBm ranges only.
(4) OUTPUT Jack. Type-N female coaxial connector. RF Output level +10 to $-146 \mathrm{dBm}(0.7 \mathrm{Vrms}$ to $0.01 \mu \mathrm{Vrms}$ ) into a $50 \Omega$ load. Frequency range is 1 to 1299.999999 MHz in 1 Hz steps.

5 VERNIER Control. RF Output continuously variable within the useable range ( +3 to -6 dB ) as indicated by the meter.

Figure 3-1. Front Panel Controls, Connectors, and Indicators

## REAR PANEL FEATURES


(1) Coaxial Plug. Connects the 3.95 to 2.75 GHz RF Input signal to the RF Section from the Frequency Extension Module.
2 Interconnect Plug. Provides interconnection of power supply voltages; RF and control signals between the RF Section plug-in and the Mainframe, Frequency Extension Module, and Modulation Section plug-in.
(3) Coaxial Plug. Connects the 3.95 to 4.05 GHz LO Input signal to the RF Section plug-in from the Frequency Extension Module.
(4) Serial Number Plate. Metal plate with stamped serial number. Four-digit and letter for prefix. Suffix is unique to an instrument.

## OPERATOR`S CHECKS



## WARNING

BEFORE CONNECTING THIS SYSTEM TO LINE (MAINS) VOLTAGE, the safety and installation instructions found in Sections II and III of the mainframe manual should be followed.

## CAUTION

Damage to the signal generator system may occur if option 002 RF Sections are used with unmodified 8660A and 8660B mainframes with serial prefixes 1349A and below. See the paragraph entitled Modifications in Section II.

NOTE
Refer to Section II for RF Section Installation instructions.

1. Set the System controls as follows:

Mainframe
LINE Switch . . . . . . . . . . . . . . ON
REFERENCE SELECTOR . . . . . . . . EXT
CENTER FREQUENCY . . . . . . . . . . 500 MHz
Modulation Section plug-in
MODE Switch
OFF
RF Section plug-in
OUTPUT RANGE Switch . . . . . . . . . 0 dBm
VERNIER Control . . . . . . . . . . . . +3 dB meter reading

## OPERATOR'S CHECKS

2. Connect the RF Section OUTPUT to the power sensor input. Verify that the amplitude of the 500 MHz signal is approximately +3 dBm .
3. Set the OUTPUT RANGE Switch to +10 dBm and adjust the VERNIER control for $\mathrm{a}-3 \mathrm{~dB}$ meter reading. Verify that the output level is approximately +7 dBm .
4. Connect the RF Section OUTPUT to the frequency counter input through the 3 dB attenuator. Verify that the signal is accurate within $\pm 1 \mathrm{~Hz}$.
5. To check the remote control capabilities of the RF Section, connect a control unit to the mainframe. Repeat steps 1 through 4 while the system is remotely programmed from an external source. Application Note 164-1 "Programming the 8660A/B Synthesized Signal Generator" provides the information needed for remote BCD operation of this system. Application Note 164-2 "Calculator Control of the 8660A/B/C Synthesized Signal Generator" provides the information needed for calculator control of the system using the HP-IB (option 005 ). Section III of the mainframe manual contains the same information in abridged form.

## OPERATING INSTRUCTIONS

## TURN ON

## WARNING

BEFORE CONNECTING THIS SYSTEM TO THE LINE (MAINS) VOLTAGE, the safety and installation instructions found in Sections II and III of the mainframe manual should be followed.

## CAUTION

Damage to the signal generator system may occur if option 002 RF Sections are used with unmodified 8660A and 8660B mainframes with serial prefixes 1349A and below. See the paragraph entitled Modifications in Section II.

NOTE
Refer to Section II for RF Section Installation Instructions.

1. Set the mainframe's LINE Switch to ON and the rear panel REFERENCE SELECTOR Switch to INT. Wait for the mainframe "oven" indication to go out.

## FREQUENCY SELECTION

2. Refer to Section III of the mainframe operating and service manual for information on system frequency selection.

## RF OUTPUT LEVEL

3. dBm . Set the OUTPUT RANGE switch to within +3 and -6 dB of the desired output level. Adjust the VERNIER control for a meter reading which when added to the OUTPUT RANGE switch indication equals the desired output level.
4. VOLTS. To set the RF output level in rms volts, the OUTPUT RANGE switch selected the full scale meter reading and the VERNIER control is adjusted for the correct voltage reading on the meter. The voltage level for meter scale 1.0 should not be set below 0.32 of full scale. The voltage level should not be set below 1 when using the meter scale of 3 .

## NOTE

In order to achieve the output level accuracy specified, the level selected must be $\leqslant+10 \mathrm{dBm}$ and the RF Section front panel meter reading must be as stated above.
5. Connect the RF Output to the Device Under Test. The front panel meter reading of RF Output level will be correct only if the input impedance of the Device Under Test is $50 \Omega$.

## MODULATION SELECTION

6. Refer to Section III of the Modulation Section plug-in operating and service manual for information relating to selection of modulation type and level.

## REMOTE OPERATION

7. Application Note 164-1 "Programming the 8660A/B Synthesized Signal Generator" provides most of the information needed for remote BCD operation of this system. AN 164-2 "Calculator Control of the 8660A/B/C Synthesized Signal Generator" provides information for remote HP-IB operation of this system. In abridged form, Section III of the mainframe manuals contain the same information.

## SECTION IV PERFORMANCE TESTS

## 4-1. INTRODUCTION

$4-2$. The procedures in this section test the instrument's electrical performance using the specifications of Table $1-1$ as the performance standards. All tests can be performed without access to the interior of the instrument. A simpler operational test is included in Section III under Operator's Checks.

### 4.3. EQUIPMENT REQUIRED

4-4. Equipment required for the performance tests is listed in the Recommended Test Equipment table in Section I. Any equipment that satisfies the critical specifications given in the table may be substituted for the recommended model(s).

## 4-5. TEST RECORD

$4-6$. Results of the performance tests may be tabulated on the Test Record at the end of these procedures. The Test Record lists all of the tested specifications and their acceptable limits. Test
results recorded at incoming inspection can be used for comparison in periodic maintenance and troubleshooting, and after repairs or adjustments.

## 4-7. PERFORMANCE TESTS

$4-8$. For each test, the specifications are written exactly as they appear in the specification table in Section I. Next, a description of the test and any special instructions or problem areas are included. Most tests that require test equipment have a setup drawing; each has a list of required equipment. The initial steps of each procedure give control settings required for that particular list.


To avoid the possibility of damage to the instrument or test equipment, read completely through each test before starting it. Then make any preliminary control settings before continuing with the procedure.

## PERFORMANCE TESTS

## 4-9. FREQUENCY RANGE

## SPECIFICATION:

1 to 1299.999999 MHz selectable in 1 Hz steps. Frequencies from 200 to kHz to 1 MHz may also be selected with some degradation in specifications.

## DESCRIPTION:

The Synthesized Signal Generator System RF OUTPUT is monitored by a frequency counter which supplies a common time base reference signal. The frequencies are checked at the extremes. Any specified frequency may be checked.


Figure 4-1. Frequency Range Test Setup
EQUIPMENT:

$$
\begin{aligned}
& \text { Frequency Counter . . . . . . . . . . . HP 5340A } \\
& 10 \text { dB Fixed Attenuator . . . . . . . . . HP 8491A Opt } 003
\end{aligned}
$$

## NOTE

In the following procedure, allow for accuracy of counter used. Model recommended is specified at $\pm 1$ count.

1. Connect frequency counter 10 MHz output reference signal to mainframe EXT REF input as shown in Figure 4-1 and set mainframe rear panel REF switch to EXT.
2. Set the RF Section OUTPUT RANGE switch to 0 dBm ; set the VERNIER control full CW.
3. Set mainframe center frequency to 1.000000 MHz and check RF section output frequency with counter. Record the frequency.

$$
0.999999
$$

4. Set mainframe center frequency to 1299.999999 MHz (Option 004 mainframe set to 1299.9999 MHz ) and check RF Section output frequency with counter. Record the frequency.

## 4-10. FREQUENCY ACCURACY AND STABILITY

## SPECIFICATION:

CW frequency accuracy and long term stability are determined by the aging rate of the time base (internal or external) and its sensitivity to changes in temperature and line voltage. Internal reference oscillator accuracy $= \pm$ aging rate $\pm 3 \times 10^{-10} 0^{\circ} \mathrm{C} \pm 3 \times 10^{-10} / 1 \%$ change in line voltage. (Aging rate for the time base in the standard mainframe is $3 \times 10^{-8} /$ day; for option 001 mainframes, $3 \times 10^{-9} /$ day.)

## NOTE

If there is any reason to doubt the mainframe crystal oscillator accuracy or stability, refer to the performance test in Section IV of the mainframe manual.

## 4-11. FREQUENCY SWITCHING TIME

## SPECIFICATION:

6 ms to be within 50 Hz of any new frequency selected; 100 ms to be within 0.5 Hz of any new frequency selected.

## DESCRIPTION:

A change in the Synthesized Signal Generator System's frequency is remotely programmed; after a preset time interval the frequency is measured. A trigger pulse from the programming device is first coupled to the oscilloscope. The pulse is delayed a preset interval by the oscilloscope and then coupled to the computing counter at which time the frequency is measured.

NOTE
The frequencies in this test were selected for worst-case conditions (longest switching time).

## 4-11. FREQUENCY SWITCHING TIME (Cont'd)



Figure 4-2. Frequency Switching Time Test Setup

## EQUIPMENT:

DC Power Supply . . . . . . . . . . . . . HP 721A
Computing Counter . . . . . . . . . . . . . . HP 5360A/5365A
Marked Card Programmer
Oscilloscope . . . . . . . . . . . . . . . . . . HP 3260A Opt 001
Coaxial Tee . . . . . . . . . . . . . . . HP 180C/1801A/1821A

## PROCEDURE:

1. Connect the dc power supply +5 volt output through a 1000 ohm resistor to pin 17 of the mating connector for J3. Pin 17 (flag) of the Marked Card Programmer output connector is also cinnected to the oscilloscope ext trigger input.
2. Connect the marked card programmer to mainframe rear panel connector J3.
3. Connect oscilloscope delayed sweep output through a BNC TEE to oscilloscope channel A vertical input and to computing counter rear panel external time measurement input.
4. Set counter controls as follows: rear panel switch to trigger; " $B$ " channel to X 1 sensitivity; module switch pressed; digits displayed for necessary resolution; measurement time to 1 ; counter gate time to 1 ms .
5. Program the System for 29.999999 MHz . Set the mainframe rear panel reference switch to external.
6. Set oscilloscope controls as follows: trigger to ac slow; ext, negative slope, trigger level at about 9:00 o'clock; sweep mode auto; delay trigger auto; main sweep 1 ms ; delay sweep $0.1 \mu \mathrm{~s}$; main sweep mode.
7. Set oscilloscope trace to start at left vertical graticule line. Use oscilloscope delay control to delay spike 5.5 divisions from CRT left graticule line.
8. Switch oscilloscope sweep mode from auto to normal.

## PERFORMANCE TESTS

## 4-11. FREQUENCY SWITCHING TIME (Cont'd)

9. Program the system for 30.000000 MHz . Frequency displayed on computing counter should be $30 \mathrm{MHz} \pm 50 \mathrm{~Hz}$. Record the frequency.
29.999950 $\qquad$ 30.000050 MHz
10. Program the system for 29.999999 MHz . Frequency displayed on counter should be within $\pm 50 \mathrm{~Hz}$ of 29.999999 MHz .
29.999949 30.000049 MHz
11. Set Oscilloscope normal sweep for 10 ms and delay sweep to $1 \mu \mathrm{~s}$.
12. Set Oscilloscope sweep mode to auto and delay control for delay spike 9.5 divisions from the CRT left graticule line.
13. Set Oscilloscope main trigger to normal and computing counter gate time to 10 ms .
14. Program the System for 30.000000 MHz . Frequency displayed on computing counter should be within $\pm 5 \mathrm{~Hz}$ or programmed frequency.
29.999995
30.000005 MHz
15. Program the System for 29.999999 MHz . Frequency Displayed on computing counter should be within $\pm 5 \mathrm{~Hz}$ of programmed frequency.
29.999994 $\qquad$ 30.000004 MHz

NOTE
To reduce the effect of random errors, steps 5 through 10 and 13 through 15 may be repeated several times ( 5 minimum). Record the average frequency.

## 4-12. OUTPUT LEVEL SWITCHING TIME

## SPECIFICATION:

In remote mode, any level change can be accomplished in less than 50 ms . Any change to another level on the same attenuator range can be accomplished in 5 ms .

## DESCRIPTION:

The Synthesized Signal Generator System RF OUTPUT level (attenuation) is remotely programmed while the RF OUTPUT is detected and monitored by an oscilloscope. Because the oscilloscope is triggered by the programming device, the time needed to effect the level change may be measured directly on the oscilloscope CRT.

## 4-12. OUTPUT LEVEL SWITCHING TIME (Cont'd)



Figure 4-3. Output Level Switching Time Test Setup
EQUIPMENT:
Marked Card Programmer
Oscilloscope . . . . . . . . . . . . . . . . . .

## PROCEDURE:

1. Connect equipment as illustrated in Figure 4-3. Note that $\pm 5$ volt output from DC Power Supply is connected through a 1000 ohm resistor to pin 17 of mating connector to J3 and to Oscilloscope external trigger input.
2. Connect RF Section OUTPUT through crystal detector to oscilloscope Channel A input.
3. Set Oscilloscope controls as follows: Main Time/Div, 5 ms ; Vertical input, dc coupled, $0.2 \mathrm{~V} / \mathrm{Div}$; Normal Sweep; Ext Trigger, negative slope, AC slow Trigger level about 9:00 o'clock.
4. Program the System's center frequency for 500 MHz and 10 dB attenuation of the RF output signal. Reprogram for 19 dB attenuation. Switching time should be less than 5 ms . Record switching time.

$$
10 \text { to } 19 \mathrm{~dB}
$$

5. Program RF Section attenuation for 10 dB , then for 30 dB . Switching time should be less than 50 ms .

$$
10 \text { to } 30 \mathrm{~dB} \longrightarrow 50 \mathrm{~ms}
$$

## 4-12. OUTPUT LEVEL SWITCHING TIME (Cont'd)

6. Repeat steps 4 and 5 with center frequency set to 1 MHz .

10 to 19 dB $\qquad$ 5 ms

## 4-13A. OUTPUT ACCURACY

SPECIFICATION: (for local and remote modes)
$\pm 1.5 \mathrm{~dB}$ to $-76 \mathrm{dBm} ; \pm 2.0 \mathrm{~dB}$ to -146 dBm at meter readings between +3 and -6 dB .

DESCRIPTION:
The RF level accuracy for the +10 and 0 dBm ranges is measured with a power meter. For the lower ranges, an IF substitution measurement technique is used.

RF level (attenuation) measurements using IF substitution is accomplished by 1) converting the RF output to a low frequency IF signal, 2) offsetting the decrease in RF level (increase in attenuation) by an equal decrease in IF attenuation. This maintains a fairly constant output level at the IF load. The intermediate frequency is selected on the basis of availability of a precision attenuator. Therefore, any variation in output level from an established reference is primarily due to the RF attenuator.

4-13A. OUTPUT ACCURACY (Cont'd)


EQUIPMENT:

| Power Meter/Sensor | HP 435A/8481A |
| :---: | :---: |
| Synthesized Signal Generator | HP 8660C/86602B/86631B |
| 40 dB Attenuator | HP 8491A Option 040 |
| Mixer | Watkins-Johnson M1J |
| 4 MHz Low Pass Filter | CIRC-Q-TEL FLT/21B- $4-3 / 50-3 \mathrm{~A} / 3 \mathrm{~B}$ |
| Coaxial Tee | 1250-0781 (BNC) |
| 50 Ohm Termination | HP 11593A |
| 40 dB Amplifier | (See Figure 1-2) |
| Double Shielded Cables (5 required) | HP 08708-6033 |
| Capacitor, $100 \mu \mathrm{~F}$ | HP 0180-2207 |
| Resistor, $100 \mathrm{k} \Omega$ | HP 0698-7284 |
| Type N-to SMA Adaptor | OSM 21040 |
| SMA-to-OSM Right Angle Adapter | OSM 219 |
| SMA-to-BNC Adapter (2) | OSM 21190 |
| 10 dB Step Attenuator | HP 355D Option H38 |
| Wave Analyzer | HP 3581A |

## 4-13A. OUTPUT ACCURACY (Cont'd)

## PROCEDURE:

1. Set the System Under Test Controls for a center frequency of 1000.000000 MHz and an output level of +10 dBm .
2. Set the power meter controls for the +15 dBm range.
3. Connect the power sensor to the RF Section OUTPUT jack of the System Under Test.
4. Set the RF Section controls as shown in the table below and verify that the RF output level is within the specified tolerance.

| Synthesized Signal Generator System |  | Power Meter Reading (dBm) |
| :---: | :---: | :---: |
| OUTPUT RANGE Switch (dBm) | Panel Meter Reading (dB) |  |
| +10 | 0 | $+8.5 \longrightarrow+11.5$ |
| +10 | -3 | $+5.5 \longrightarrow+8.5$ |
| +10 | -6 | +2.5 |
| 0 | -6 | $-7.5-$ - -4.5 |
| 0 | -3 | $-4.5-\quad-1.5$ |
| 0 | 0 | $-1.5<{ }^{+}+1.5$ |
| 0 | +3 | ${ }^{+1.5}+{ }^{+} 4.5$ |

## NOTE

Be careful not to vary the RF Section's VERNIER control setting throughout the rest of this procedure.
5. Connect the 40 dB attenuator directly to the OUTPUT jack of the RF Section in place of the power sensor.
6. Connect the " $R$ " port of the mixer directly to the 40 dB attenuator using the Type N-to SMA adapter and the SMA-to-OSM right angle adapter.
7. Connect the 4 MHz Low Pass Filter to the "I" port of the mixer with a SMA-to-BNC adapter.
8. Connect the cable from the Reference System output to the "L" port of the mixer with a SMA-to-BNC adapter.

NOTE
Be sure all connections are tight to prevent RF leakage.
9. Set the reference system controls for a center frequency of 1000.011000 and an output level of +7 dBm . Set the rear panel reference selector to external.
10. Set the 10 dB Step Attenuator to 50 dB .

## PERFORMANCE TESTS

## 4-13A. OUTPUT ACCURACY (Cont'd)

11. Set the wave analyzer controls as follows: frequency 11 kHz , resolution bandwidth 3 Hz , sweep mode off, dBv/LIN - dBm $600 \Omega$ switch to $\mathrm{dBv} / \mathrm{LIN}$, amplitude reference level -40 dB , AFC switch unlock and scale 10 dB .
12. Connect the other equipment which follows the 4 MHz Low Pass Filter as shown in Figure 4-4A.
13. Tune the wave analyzer frequency control for the maximum meter reading. Adjust the input sensitivity and vernier controls for a midscale meter reading. Press the AFC control for frequency lock.
14. Wait 30 seconds for the DVM reading to stabilize. Record the DVM reading. This is the reference level equivalent to the last power meter reading ( $\approx+3 \mathrm{dBm}$ ).
15. Use the following formula to calculate the obsolute RF output level from the System Under Test:
$\mathrm{dBm}=\mathrm{dBm}_{1}-\Delta \mathrm{dB}+2\left(\mathrm{~V}-\mathrm{V}_{\mathrm{ref}}\right)$
dBm is the RF output level
$\mathrm{dBm}^{1}$ is the actual RF level measured at the $+3 \mathrm{dBm}(0 \mathrm{dBm}$ OUTPU'T RANGE setting) in Step 4.
$\Delta \mathrm{dB}$ is the difference in 10 dB step attenuator setting.
V is the DVM reading for each individual OUTPUT RANGE.
$V_{\text {ref }}$ is the reference DVM reading.

## NOTE

The wave analyzer recorder output sensitivity is $2 d B /$ volt.
16. Set the RF Section OU'TPUT RANGE switch to -10 dBm ; set the 10 dB step attenuator to the 40 dB . Wait 30 seconds for the reading to stabilize. Record the DVM reading in the table following step 17. Calculate and record the RF level in the table.

EXAMPLE:

$$
\begin{aligned}
\mathrm{dBm}= & \mathrm{dBm}_{1}-(\Delta \mathrm{dB})+2\left(\mathrm{~V}_{1}-\mathrm{V}_{\mathrm{ref}}\right) \\
& \mathrm{dBm}_{1}=2.8 \mathrm{dBm} \\
& \Delta \mathrm{~dB}=10 \mathrm{~dB} \\
& \mathrm{~V}_{1}=2.388 \mathrm{Vdc} \\
& \mathrm{~V}_{\mathrm{ref}}=2.433 \mathrm{Vdc}(\text { from step } 14) \\
\mathrm{dBm}= & 2.8-(10)+2(2.388-2.433) \\
= & 2.8-10+2(-0.045) \\
= & -7.29 \mathrm{dBm}
\end{aligned}
$$

## PERFORMANCE TESTS

## 4-13A. OUTPUT ACCURACY (Cont'd)

17. Continue as in step 16 , to measure, record and calculate the DVM reading and RF level for each OUTPUT RANGE setting as shown in the following table.

| OUTPUT RANGE <br> Switch (dBm) | 10 dB Step <br> Attenuator <br> (dB) | DVM <br> Reading <br> (Vdc) | Absolute RF Output <br> Level (dBm) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Min. | Actual | Max. |  |
| 0 | 50 | - | +1.5 |  | +4.5 |
| -10 | 40 | - | -8.5 | - | -5.5 |
| -20 | 30 | - | -18.5 | - | -15.5 |
| -30 | 20 | - | -28.5 | - | -25.5 |
| -40 | 10 | - | -38.5 | - | -35.5 |
| -50 | 0 | - | -48.5 | - | -45.5 |

18. Set the 10 dB step attenuator to 50 dB .
19. Remove the 40 dB attenuator and connect the mixer directly to the OUTPUT jack of the system under test.
20. Increase the wave analyzer's input sensitivity by 10 dB . If necessary, adjust the input sensitivity vernier for a midscale meter reading.
21. Transfer the last calculated RF output level on the preceding table to the first line on the following table. Wait 30 seconds and record the new DVM reading ( $\mathrm{V}_{\mathrm{ref}}$ ).
22. Use the formula and the new $\mathrm{V}_{\text {ref }}$ level to calculate the RF level for each range shown in the following table.

| OUTPUT RANGE <br> Switch (dBm) | 10 dB Step <br> Attenuator <br> (dB) | DVM <br> Reading <br> (Vdc) | Absolute RF Output <br> Level (dBm) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Actual | Max. |
|  | 50 | - | -48.5 | - | -45.5 |
| -60 | 40 | - | -58.5 | - | -55.5 |
| -70 | 30 | - | -68.5 | - | -65.5 |
| -80 | 20 | - | -79.0 | - | -75.0 |
| -90 | 10 | - | -89.0 | - | -85.0 |
| -100 | 0 | - | -99.0 | - | -95.0 |

23. Set the wave analyzer's AFC switch to unlock (OFF). Adjust the frequency control for the peak reading equal to the last recorded DVM reading on the previous table.
24. Set the 10 dB step attenuator to 30 dB .

## PERFORMANCE TESTS

## 4-13A. OUTPUT ACCURACY (Cont'd)

25. Set the wave analyzer amplitude reference level to -60 dB . Increase the input sensitivity 10 dB .
26. Transfer the last RF output level reading on the preceding table to the first line of the following table. After 30 seconds record the new DVM reference on the first line of the following table.
27. Measure, calculate, and record the DVM reading and RF level for each OUTPUT RANGE Setting as shown in the following table. Due to the high noise levels evident on this test, there is appreciable deviation in the wave analyzer and DVM readings. Record the average reading.

| OUTPUT RANGE <br> Switch (dBm) | 10 dB Step <br> Attenuator <br> (dB) | DVM <br> Reading <br> (Vdc) | Absolute RF Output <br> Level (dBm) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. | Actual | Max. |
|  | 30 | - | -99.0 |  | -95.0 |
| -110 | 20 | - | -109.0 | - | -105.0 |
| -120 | 10 | - | -119.0 | - | -115.0 |
| -130 | 0 | -129.0 | - | -125.0 |  |

NOTE

Output level accuracy may be checked at any frequency between 300 and 2000 MHz using this procedure. This procedure may also be used at the frequency extremes if a well shielded mixer specified for the desired frequency range is used in place of the Watkins-Johnson M1J.

## 4-13B. OUTPUT ACCURACY - ALTERNATE PROCEDURE

## SPECIFICATION:

$\pm 1.5 \mathrm{~dB}$ to $-76 \mathrm{dBm} ; \pm 2.0 \mathrm{~dB}$ to -146 dBm at meter readings between +3 and -6 dB .

## DESCRIPTION:

The RF Level Accuracy for the +10 and 0 dBm ranges is measured with a power meter. A reference level is established and accuracy is checked from 0 dBm to -80 dBm by comparing the RF Section attenuation against a calibrated 10 dB step attenuator.

## NOTE

This procedure checks all sections of the RF Section Attenuator separately. Also, the $10 \mathrm{~dB}, 20 \mathrm{~dB}$, and 40 dB sections are checked in all possible combinations. The sum of the -70 dBm inaccuracy at -80 dBm shall not exceed +1.0 dB .

4-13B. OUTPUT ACCURACY - ALTERNATE PROCEDURE (Cont'd)


Figure 4-4B. Output Accuracy Test Setup (Alternate Procedure)
EQUIPMENT:
Spectrum Analyzer . . . . . . . . . . . . . HP 8555A/8552B/140T
Power Meter/Sensor . . . . . . . . . . . . . . . . . HP 435A/8481A
10 dB Step Attenuator
20 dB Amplifier . . . . . . . . . . . . . . . . . . .

PROCEDURE:

1. Set the system controls for a frequency of 30 MHz and an output level of +10 dBm .
2. Connect the power sensor to the RF Section's OUTPUT jack.
3. Set the RF Output Level as shown in the table below and verify that the level is within the specified tolerance.

| Synthesized Signal Generator System |  | Power Meter Reading (dBm) |
| :---: | :---: | :---: |
| OUTPUT RANGE Switch (dBm) | Panel Meter Reading (dB) |  |
| +10 | 0 | $+8.5 \longrightarrow+11.5$ |
| +10 | -3 | $+5.5 \longrightarrow+8.5$ |
| +10 | -6 | $+2.5 \longrightarrow+5.5$ |
| 0 | -6 | $-7.5 \longrightarrow-4.5$ |
| 0 | -3 | $-4.5-1.5$ |
| 0 | 0 | $-1.5 \longrightarrow+1.5$ |
| 0 | + 3 | $+1.5 \longrightarrow+4.5$ |

## 4-13B. OUTPUT ACCURACY - ALTERNATE PROCEDURE (Cont'd)

NOTE
Do not change the RF Section VERNIER Control Setting until this procedure is completed.
4. Set the spectrum analyzer controls as follows: center frequency 30 MHz , frequency span per division 5 kHz , resolution bandwidth 3 kHz , input attenuation 10 dB , vertical sensitivity per division 2 dB , and sweep time per division 5 ms .
5. Set the 10 dB Step attenuator switch to the 80 dB range.
6. Connect the equipment as shown in Figure 4-4B.
7. Adjust the reference level range and vernier to extablish a reference level on the analyzer display.
8. On the first line of the following table, record the power meter reading shown on the preceding table for the OUTPUT RANGE Setting of 0 dBm and the panel meter reading of +3 dB . This is the absolute RF level which corresponds to the display reference.
9. Set the OUTPUT RANGE switch and the 10 dB step attenuator range switch settings as shown on each line of the following table. Record the display variation from the established reference.
10. Calculate the RF level using the following formula:
$\mathrm{dBm}=\mathrm{dBm}^{1}-\Delta \mathrm{dB}_{10}+\Delta \mathrm{dB}$
dBm is the RF output level
$\mathrm{dBm}^{1}$ is the RF level measured at +3 dBm ( 0 dBm OUTPUT RANGE setting) in step 3.
$\Delta \mathrm{dB}_{10}$ is the change in 10 dB Step Attenuator level
$\Delta \mathrm{dB}$ is the variation from the established display reference for each OUTPUT RANGE setting.

For example, results of the first step are:

$$
\begin{aligned}
\mathrm{dBm}_{1} & =+2.8 \\
\Delta \mathrm{~dB}_{10} & =10 \\
\Delta \mathrm{~dB} & =-0.2 \\
\mathrm{dBm} & =+2.8 \mathrm{dBm}-10 \mathrm{~dB}+(-0.2) \mathrm{dB} \\
& =-7.4 \mathrm{dBm}
\end{aligned}
$$

4-13B. OUTPUT ACCURACY - ALTERNATE PROCEDURE (Cont'd)

| OUTPUT RANGE <br> Switch (dBm) | 10 dB Step <br> Attenuator <br> (dB) | RF Output Level <br> (dBm) |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Min. | Measured | Max. |
| 0 | 80 | +1.5 | - | +4.5 |
| -10 | 70 | -8.5 | - | -5.5 |
| -20 | 60 | -18.5 | - | -15.5 |
| -30 | 50 | -28.5 | - | -25.5 |
| -40 | 40 | -38.5 | - | -35.5 |
| -50 | 30 | -48.5 | - | -45.5 |
| -60 | 20 | -58.5 | - | -55.5 |
| -70 | 10 | -68.5 | - | -65.5 |
| -80 | 0 | -79.0 | - | -75.0 |

11. Subtract the two levels obtained for OUTPUT RANGES of -70 and --80 dBm . The level change should be $10 \pm 1 \mathrm{~dB}$.

9 dB

## 4-14. OUTPUT FLATNESS

## SPECIFICATION:

Output level variation with frequency is less than $\pm 1.0 \mathrm{~dB}$ from $1-1300 \mathrm{MHz}$ at front panel meter readings between +3 and -6 dB .

## DESCRIPTION:

After an output level reference is established, power level measurements are made at various frequencies across the range of the Synthesized Signal Generator System. The Output levels must fall within the limits specified.

EQUIPMENT:
Power Meter/Sensor .
HP 435A/8481A

## PROCEDURE:

1. Zero the Power Meter.
2. Set the system center frequency to 1000 MHz .
3. Set the Power Meter range switch to 0 dBm ; set the RF Section OUTPUT RANGE Switch and VERNIER Control for an output level of -1.0 dBm as read on the power meter.

## 4-14. OUTPUT FLATNESS (Cont'd)

4. Measure and record the power level indicated by the Power Meter at the following center frequencies: $1 \mathrm{MHz}, 10 \mathrm{MHz}, 100 \mathrm{MHz}, 200,400,600,800$, and 1299 MHz .

| 1 MHz | $-2.0 \ldots 0.0 \mathrm{dBm}$ |
| :---: | :---: |
| 10 MHz | -2.0 _ 0.0 dBm |
| 100 MHz | $-2.0 \square$ |
| 200 MHz | $-2.0 \square 0.0 \mathrm{dBm}$ |
| 400 MHz | $-2.0 \square 0.0 \mathrm{dBm}$ |
| 600 MHz | $-2.0 \square 0.0 \mathrm{dBm}^{-}$ |
| 800 MHz | $-2.0 \square 0.0 \mathrm{dBm}^{-}$ |
| 1299 MHz | $-2.0 \ldots 0.0 \mathrm{~dB}$ |

## 4-15. HARMONIC SIGNALS

## SPECIFICATION:

All harmonically related signals are at least 30 dB below the desired output signal for output levels $\leqslant+3 \mathrm{dBm}$. ( 25 dB down for output levels above +3 dBm .)

## DESCRIPTION:

A spectrum analyzer is used to measure the relative levels of the second and third carrier harmonics with respect to the carrier fundamental at various center frequencies.

## EQUIPMENT:

Spectrum Analyzer . . . . . . . . . . . . HP 8555A/8552B/140T

## PROCEDURE:

1. Set the system center frequency to 1299 MHz ; set the RF Section OUTPUT RANGE switch and VERNIER control for an output level of +10 dBm .
2. Connect the power meter/sensor to the system RF OUTPUT jack.
3. Readjust the VERNIER control for a power meter reading of +10 dBm .
4. Set the spectrum analyzer input attenuation to 30 dB . Connect the RF Section OUTPUT jack to the spectrum analyzer RF input.
5. Set the other spectrum analyzer controls for convenient viewing of the carrier. Adjust the controls as necessary to view the second and third harmonics. Record the harmonic levels relative to the fundamental signal.

Second Third $1299 \mathrm{MHz} \geqslant 25 \mathrm{~dB}$ down $\qquad$

## PERFORMANCE TESTS

## 4-15. HARMONIC SIGNALS (Cont'd)

6. Repeat steps 1 through 5 at the other frequencies listed. Record the levels.

| 1000 MHz | $\geqslant 25 \mathrm{~dB}$ down | Second | Third |
| ---: | :--- | :--- | :--- |
| 500 MHz | $\geqslant 25 \mathrm{~dB}$ down | - |  |
| 100 MHz | $\geqslant 25 \mathrm{~dB}$ down | - |  |
| 10 MHz | $\geqslant 25 \mathrm{~dB}$ down | - |  |

7. Set the system center frequency to 100 MHz ; set the RF Section OUTPUT RANGE switch to 0 dBm and the VERNIER control for a front panel meter reading of +3 dB . Record the harmonic levels.

Second Third

4-16. PULSE MODULATION RISETIME

## SPECIFICATION:

50 nanoseconds.
DESCRIPTION:
The external pulse generator output is coupled to the RF Section plug-in through the Model 86631B Auxiliary Section. The pulse modulated signal is detected and the rise time measured with an oscilloscope.

## 4-16. PULSE MODULATION RISETIME (Cont'd)



Figure 4-5. Pulse Modulation Risetime Test Setup
EQUIPMENT:
Pulse Generator.....
Oscilloscope . . . . . . . . . . . . . . . . . . .

## PROCEDURE:

1. Set System center frequency to 1200 MHz .
2. Set the RF Section OUTPUT RANGE switch and VERNIER control for an output of +10 dBm .
3. Set the Auxiliary Section external modulation switch to pulse; set pulse level control full cw.
4. Adjust pulse generator output for -10 Vpk (into $50 \Omega$ ) with risetime $\leqslant 10 \mathrm{~ns}$; set pulse repetition rate and width to convenient values.
5. Connect equipment as illustrated in Figure 4-5.
6. Adjust oscilloscope to display leading edge of detected pulse modulated RF signal. Risetime, as measured between the $10 \%$ and $90 \%$ amplitude points on leading edge, should be 50 nanoseconds or less.
$\qquad$

## PERFORMANCE TESTS

## 4-17. PULSE MODULATION ON/OFF RATIO

## SPECIFICATION:

At least 40 dB .

## DESCRIPTION:

An HP Model 86631B Auxiliary Section is inserted in the left drawer of the Synthesized Signal Generator System. The RF Section OUTPUT is monitored by a spectrum analyzer. The carrier reference is set on the display with the Auxiliary Section external modulation switch set first to Off (equivalent to pulse-on). Then the modulation switch is set to Pulse (equivalent to pulse-off without an external pulse input). The ratio of the pulse-off level to the carrier reference is the on/off ratio.

EQUIPMENT:
Spectrum Analyzer . . . . . . . . . . . . HP 8555A/8552B/140T

## PROCEDURE:

1. Set System center frequency to 500 MHz, RF Section OUTPUT RANGE Switch and VERNIER control for an output level of +10 dBm , and Auxiliary Section external modulation switch to off.
2. Set the spectrum analyzer input attenuation to 30 dB ; connect the RF Section OUTPUT to the analyz'er $R F$ input.
3. Adjust the analyzer controls for a CRT display of the carrier. Establish the reference by positioning the carrier peak on the top horizontal graticule line.
4. Set the Auxiliary Section external modulation switch to Pulse and the Pulse Level control fully clockwise. The signal displayed on Spectrum Analyzer should be $>40 \mathrm{~dB}$ down with respect to the reference. Record the indication.

40 dB down $\qquad$

## 4-18. AMPLITUDE MODULATION DEPTH AND 3 dB BANDWIDTH

## SPECIFICATION:

Depth: $0-90 \%$ for RF output level meter readings from +3 to -6 dB and only at +3 dBm and below. 3 dB Bandwidth: At center frequencies $<10 \mathrm{MHz}$

10 kHz from $0-30 \% \mathrm{AM}$
6 kHz from $0-70 \% \mathrm{AM}$
5 kHz from $0-90 \% \mathrm{AM}$
At center frequencies $\geqslant 10 \mathrm{MHz}$
100 kHz from $0-30 \% \mathrm{AM}$
60 kHz from $0-70 \% \mathrm{AM}$
50 kHz from $0-90 \% \mathrm{AM}$

## NOTE

To check AM accuracy, refer to section IV of the appro-
priate modulation section Operating and Service manual.

## PERFORMANCE TESTS

## 4-18. AMPLITUDE MODULATION DEPTH AND 3 dB BANDWIDTH (Cont'd)

## DESCRIPTION:

The system Rf output is amplitude modulated. The signal is demodulated by a peak detector in a spectrum analyzer (the frequency span width is set to zero). The ac and dc components are measured with a voltmeter at the detector (vertical) output. First, the dc component is set to -283 mVdc plus a detector offset correction. Then, the ac component is measured. The AM level (\%) is $1 / 2$ (one half) the rms output.

Because of the required measurement accuracy, the accuracy of the spectrum analyzer's detector offset must be known to $\pm 2 \mathrm{mVdc}$. The offset voltage is calculated by measuring the change in the detector output for a change in the RF input and assuming a linear detector over the range of the levels used.


Figure 4-6. Amplitude Modulation Depth and 3 dB Bandwidth Test Setup

## EQUIPMENT:



## PERFORMANCE TESTS

## 4-18. AMPLITUDE MODULATION DEPTH AND 3 dB BANDWIDTH (Cont'd)

## PROCEDURE:

1. Connect the equipment as shown in Figure 4-6 (step 1).
2. Set the synthesized signal generator controls as follows: center frequency 30 MHz , OUTPUT RANGE -10 dBm , VERNIER control for a panel meter reading of 0 dB , and AM off.
3. Let the spectrum analyzer warm up for 1 hour to minimize drift of the spectrum analyzer detector output. Set 10 dB step attenuator to 10 dB attenuation.
4. Set the spectrum analyzer center frequency to 30 MHz , frequency span per division 5 MHz , resolution bandwidth 300 kHz ; input attenuation to 20 dB , and vertical sensitivity per division 10 dB . Adjust the center frequency control to center the display. Set the frequency span to zero and tune to peak the trace.

## NOTE

Throughout this test, continually check that the signal is peaked for maximum deflection. Tune the center frequency control for maximum signal deflection.
5. Set the vertical scale to linear and adjust the reference level vernier for a digital voltmeter reading of -200 mVdc .
6. Set the 10 dB step attenuator to 0 dB and record the digital voltmeter reading.
$\qquad$ mVdc
7. Set the 10 dB Step Attenuator to 20 dB and record the digital voltmeter reading.
$\qquad$ mVdc
8. Calculate the offset voltage using the following formula:

$$
\mathrm{V}_{\mathrm{off}}=\frac{\mathrm{mVdc}+200 \alpha}{1-\alpha}
$$

Where $\mathrm{V}_{\text {off }}$ is the offset voltage in millivolts
mVdc is the DVM reading in millivolts $\alpha$ is 3.16 (step 5) or 0.316 (step 6).

For example:

$$
\begin{aligned}
& \mathrm{mVdc}=-687 \text { in step } 5 \\
& \text { therefore } V_{\text {off }}=\frac{-687+200(3.16)}{1-(3.16)}=+25.5 \mathrm{mVdc}
\end{aligned}
$$

9. Find the value of $\mathrm{V}_{\text {off }}$ for step 6. The difference between the two should be $<4 \mathrm{~m} \mathrm{Vdc}$. Use the average value of $\mathrm{V}_{\text {off }}$ -
10. Set the 10 dB step Attenuator to 10 dB .

## 4-18. AMPLITUDE MODULATION DEPTH AND 3 dB BANDWIDTH (Cont'd)

11. Set the system center frequency to 500 MHz , the modulation mode to AM , the modulation source to external, and a modulation level of $30 \%$ ( 0.3 Vrms input to an Auxiliary Section; 1.5 Vrms to a Modulation Section) at a 1 kHz rate.
12. Set the spectrum analyzer center frequency control to 500 MHz , frequency span to zero, and peak the trace. Set the reference level vernier for a digital voltmeter reading of $-283 \mathrm{mVdc}+\mathrm{V}_{\text {off }}$. See Steps 8 and 9 .
13. Set the DVM controls to measure the peak detector's ac component. The modulation level (\%) is $1 / 2$ (one-half) the DVM reading (Vrms). Record the reading for $30 \% \mathrm{AM}$.

50 mVrms 70 mVrms
14. Set the modulation section (test oscillator) controls for $70 \%$ AM. Record the DVM reading.

130 mVrms $\qquad$ 150 mVrms
15. Set the modulation section (test oscillator) controls for $90 \%$ AM. Record the DVM reading

170 mVrms $\qquad$ 190 mVrms
16. Connect the crystal detector to the RF Section OUTPUT jack.
17. Set the modulation section and test oscillator controls for an AM level of $30 \%$ ( 0.3 Vrms input to an auxiliary section; 1.5 Vrms to a modulation section) at a 5 kHz rate.
18. Set the oscilloscope controls for a 5 division peak-to-peak display of the demodulated signal.
19. Increase the test oscillator frequency to 100 kHz . The signal amplitude should be $\geqslant 3.5$ divisions peak-to-peak.

$$
3.5 \text { div. } \mathrm{p}-\mathrm{p}
$$

20. Install the 1500 Pf capacitor as shown in Figure 4-6.
21. Repeat steps 17 through 19 with center frequency set to 9 MHz . Increase the test oscillator frequency from 5 to 10 kHz . Record the signal amplitude.
[^3]
## 4-19. FREOUENCY MODULATION RATE AND DEVIATION

## SPECIFICATION:

Rate: DC to 200 kHz with the 86632 B or 86635 A .
20 Hz to 100 kHz with the 86633 B .
Maximum Deviation (Peak):
200 kHz with the 86632B and 86635A.
100 kHz with the 86633B.

## NOTE

To check the frequency modulation rate and deviation, refer to the performance test in Section IV of the applicable modulation section manual.

## 4-20. OUTPUT IMPEDANCE AND VSWR

## SPECIFICATION:

Impedance: $50 \Omega$
VSWR: $<2.0$ on +10 and 0 dBm ranges $;<1.3$ on -10 dBm range and below.

## DESCRIPTION:

The Synthesized Signal Generator System's output signal is reflected back into the RF OUTPUT jack by a coaxial short at the end of an adjustable stub (a variable length of air-line). This reflected signal is re-reflected by any mismatch at the jack. The re-reflected signal combines with the output signal according to the relative phase and magnitude of the two signals. The combined signal is monitored by a directional coupler and then measured by a voltmeter or spectrum analyzer. Maximum and minimum power levels are noted as the electrical length of the stub is varied (i.e. the electrical distance from the RF OUTPUT jack to the coaxial short is varied). The maximum allowable change in voltage or dB is calculated from the following formulas.

$$
\begin{aligned}
\mathrm{VSWR} & =\frac{\mathrm{V}_{\max }}{\mathrm{V}_{\min }} \\
\mathrm{V}_{\max } & =(\mathrm{VSWR})\left(\mathrm{V}_{\min }\right) \\
\mathrm{dB} & =20 \log \left(\frac{\mathrm{~V}_{\max }}{\mathrm{V}_{\min }}\right) \\
\mathrm{dB} & =20 \log (\mathrm{VSWR})
\end{aligned}
$$

## 4-20. OUTPUT IMPEDANCE AND VSWR (Cont’d)



Figure 4-7. Output Impedance Test Setup
EQUIPMENT:


## PROCEDURE:

1. Set the Synthesized Signal Generator system center frequency to 500 MHz , the OUTPUT RANGE switch to +10 dBm , and the VERNIER control for a panel meter reading of 0 dB .
2. Set up the equipment as shown in Figure 4-7.
3. Set the spectrum analyzer controls for a convenient display of the signal. Set the vertical sensitivity to 2 dB per division.
4. Adjust the stub for a minimum indication on the spectrum analyzer display. Adjust the reference level range and vernier controls for a convenient reference level.
5. Adjust the stub for a maximum indication on the display. The signal level increase should be $<6 \mathrm{~dB}$ (VSWR <2.0).
6. Set the system's OUTPUT RANGE switch to 0 dBm . Adjust the VERNIER control for a panel meter reading of +3 dB .
7. Repeat steps 3 and 4. The signal level increase should be $<6 \mathrm{~dB}$ (VSWR $<2.0$ ).
8. Set the system's OUTPUT RANGE switch to -10 dBm .

## PERFORMANCE TESTS

## 4-20. OUTPUT IMPEDANCE AND VSWR (Cont'd)

9. Repeat steps 3 and 4. The signal level increase should be $<2.3 \mathrm{~dB}$ (VSWR $<1.3$ ).
10. If desired, repeat at other frequencies between 100 MHz and 1 GHz .

## NOTE

The steps given above effectively check VSWR at all settings of the output attenuator.

## 4-21. SIGNAL-TO-PHASE NOISE RATIO

SPECIFICATION: (For AM, CW, and $\phi \mathrm{M}$ modes only)
Greater than 45 dB in a 30 kHz band centered on the carrier and excluding a 1 Hz band centered on the carrier.

## DESCRIPTION:

AC voltage measurements proportional to carrier amplitude and residual carrier phase deviation are compared for the signal-to-phase noise ratio. The Synthesized Signal Generator System's reference and RF output (carrier) signals are mixed and the difference frequency is monitored by an oscilloscope and ac voltmeter. The mixer output (proportional to the carrier amplitude) is noted. The two signals are then frequency synchronized with phase difference of $180^{\circ}$. (This phase difference provides maximum resolution for voltage measurements at the mixer output which are proportional to the change of phase of the RF output signal.) This ac voltage is proportional to the phase noise and when compared to the carrier voltage yields the signal-to-phase noise ratio.

## NOTE

A $3 d B$ correction factor takes into account the non-correlated noise contribution of the reference system. The noise levels of the reference system and the system under test are assumed to be equal.

## PERFORMANCE TESTS

## 4-21. SIGNAL-TO-PHASE NOISE RATIO (Cont'd)



Figure 4-8. Signal-to-Phase Noise Ratio Test Setup

## EQUIPMENT:

$$
\begin{aligned}
& \text { Synthesized Signal Generator System } \\
& \text { Oscilloscope . }
\end{aligned} .
$$

## PROCEDURE:

1. Set the controls of the system under test as follows: center frequency 500.001000 MHz and the output level to -47 dBm (OUTPUT RANGE switch set to -50 dBm ).
2. Set the controls of the reference system as follows: center frequency 500.000000 MHz and the output level to +7 dBm .
3. Connect the equipment as shown in Figure 4-8.
4. Record the relative ac voltmeter reading.

## 4-21. SIGNAL-TO-PHASE NOISE RATIO (Cont'd)

5. Set the system under test OUTPUT RANGE switch to $-10 \mathrm{dBm}(-7 \mathrm{dBm}$ output level).
6. Adjust the oscilloscope display of the 1 kHz signal for an amplitude of eight divisions. Set the oscilloscope vertical input to ground and adjust the vertical position control so the trace lies over the center horizontal line of the graticule. Set the vertical input to dc coupled.
7. Set the system under test center frequency to 500.000001 MHz and note that oscilloscope baseline trace alternately rises and falls over eight-division display. ( 510.0001 MHz ; Option 004).
8. Reset the center frequency to 500.000000 MHz at a time that causes the oscilloscope baseline trace to stop within $\pm 1 / 10$ division of the center horizontal line of the graticule.
9. Read the noise level on the ac voltmeter. Signal-to-phase noise ratio equals the sum of the attenuator change and the reference system noise contribution minus the change in voltmeter reading (in dB ). Signal-to-phase noise ratio $=40 \mathrm{~dB}+3 \mathrm{~dB}-( \pm \Delta \mathrm{dB})$. For example, the voltmeter reading is 8 dB below the reference $(-8 \mathrm{~dB})$. Therefore, the signal-to-phase noise ratio $=40+3-(-8)=51 \mathrm{~dB}$ down.
10. Record the ratio.

45 dB down $\qquad$

## 4-22. SIGNAL-TO-AM NOISE RATIO

## SPECIFICATION:

Greater than 65 dB in a 30 kHz bandwidth centered on the carrier excluding a 1 Hz band centered on the carrier.

## DESCRIPTION:

A comparison of ac voltage measurements proportional to carrier amplitude and AM noise yields the signal-to-AM noise ratio. First, a carrier reference level is determined by measuring the detected ac voltage for $30 \% \mathrm{AM}$ (the detected signal is 10.5 dB below the carrier level). Then the AM noise level is measured and the signal-to-AM noise ratio is determined.

## 4-22. SIGNAL-TO-AM NOISE RATIO (Cont'd)



Figure 4-9. Signal-to-AM Noise Ratio Test Setup.

## EQUIPMENT:



## PROCEDURE:

1. Set the 10 dB step attenuator to 50 dB .
2. Set the system center frequency to 500 MHz and the RF output level to $+3 \mathrm{dBm}(0 \mathrm{dBm}$ OUTPUT RANGE).
3. Connect the equipment as shown in Figure 4-9.
4. Set the system's modulation section controls for the AM mode and an external modulation source. The modulation level control and/or the test oscillator controls are set for a modulation level of $30 \%$ ( 0.3 Vrms to an auxiliary section; 1.5 Vrms to a modulation section) at a 1 kHz rate.

## NOTE

The ac voltmeter can be used to monitor the modulation or auxiliary section input voltage while it is being set.
5. Record the ac voltmeter reading of the 40 dB amplifier output in dB .

## PERFORMANCE TESTS

## 4-22. SIGNAL-TO-AM NOISE RATIO (Cont'd)

6. Set the system's modulation mode to off.
7. Set the 10 dB step attenuator to 0 dB .
8. Record the ac voltmeter reading.
9. The signal-to-AM noise ratio is equal to the sum of the change in attenuation level and the level of the $30 \%$ AM level relative to the carrier minus the change in ac voltmeter reading in dB . Therefore, signal-to-AM noise ratio $=50 \mathrm{~dB}+10.5 \mathrm{~dB}-( \pm \Delta \mathrm{dB})$. For example, the ac voltmeter reading is 12 dB down (below) the reference level and the signal-to-AM noise ratio $=50+10.5-(-12)$ or 72.5 dB down.
10. Record the ratio.

65 dB down $\qquad$

## 4-23. RESIDUAL FM

## SPECIFICATION:

In the CW, AM, and $\emptyset \mathrm{M}$ modes, less than $1.5 \mathrm{~Hz}-\mathrm{rms}$ in a 2 kHz band centered on the carrier.

## DESCRIPTION:

Because residual FM and Phase Noise cannot be measured separately and because the Residual FM is the smaller part of the total measurement ( $\approx 1 / 4$ ), this measurement is indirectly made in the Signal-to-Phase Noise Ratio test.

## 4-24. AMPLITUDE MODULATION DISTORTION

## SPECIFICATION:

AM distortion at $30 \% \mathrm{AM}$ is $<1 \%$, at $70 \% \mathrm{AM}$ is $<3 \%$, and at $90 \% \mathrm{AM}$ is $<5 \%$.

## NOTES

1. The AM distortion specification applies only at 400 and 1000 Hz rates, with a front panel meter indication of 0 to $+3 d B$, and at OUTPUT RANGE switch settings of $\leqslant 0 \mathrm{dBm}$. At a meter indication of $-6 d B$, the distortion approximately doubles. The modulating signal distortion must be $<0.3 \%$ for the system performance to meet the specifications.

## PERFORMANCE TESTS

## 4-24. AMPLITUDE MODULATION DISTORTION (Cont'd)

## Notes (Cont'd)

2. If the signal generator system does not meet the $A M$ distortion specification, refer to the Systems Troubleshooting information in Section VIII (Service Sheet 1) in this manual.

## DESCRIPTION:

To measure AM distortion, a distortion analyzer is connected to the video output of a spectrum analyzer. In the zero frequency-span mode, the video output of the spectrum analyzer is the detected RF signal. The signal generator system controls are set for a specific AM level and the distortion level is measured.


Figure 4-10. Amplitude Modulation Distortion Test Setup.
EQUIPMENT:

$$
\begin{aligned}
& \text { Distortion Analyzer . . . . . . . . . . . . . HP 333A } \\
& \text { Spectrum Analyzer . . . . . . . . . . . . . . . . HP 8555A/8552B/140T } \\
& \text { Function Generator . . . . . . . . . . . . . . HP 203A } \\
& \text { AC Voltmeter . . . . . . . . . . . . . . HP 403B }
\end{aligned}
$$

## PROCEDURE:

1. Set the signal generator system controls for a center frequency of 1000 MHz , the output level to -20 dBm (OUTPUT RANGE -20 dBm ), and the modulation mode to off.
2. Set the spectrum analyzer center frequency to 1000 MHz , frequency span per division 1 MHz , resolution bandwidth 300 kHz , input attenuation 20 dB , and vertical sensitivity per division 10 dB .
3. Connect the equipment as shown in Figure 4-10.

## PERFORMANCE TESTS

## 4-24. AMPLITUDE MODULATION DISTORTION (Cont'd)

4. Set the spectrum analyzer's tuning stabilizer to on. Adjust the center frequency fine tune to center the signal on the display. Set the reference switch and vernier to center the trace vertically.
5. Set the frequency span per division to zero, and the vertical scale to linear. Peak the trace by adjusting the fine tune center frequency control. Center the trace vertically with the vertical sensitivity and vernier controls.
6. Set the signal generator system's modulation mode to AM, the source to external, and set the modulation level to $30 \%$. If a modulation section plug-in is installed in the Signal Generator mainframe, set the test oscillator controls to 1.5 Vrms at 1000 Hz . If an auxiliary section plug-in is installed, set the test oscillator controls to 0.3 Vrms at 1000 Hz .
7. Measure the total harmonic distortion. With the trace peaked on the display, the distortion should be less than $1 \%$.
8. Set the System modulation level to $70 \%$ AM. If the Auxiliary Section plug-in is being used, set the test oscillator to an output of 0.7 Vrms .
9. Measure the total harmonic distortion. With the trace peaked on the display, the distortion should be less than $3 \%$.
10. Set the system modulation level to $90 \%$ AM. $\qquad$
11. Set the system modulation level to $90 \%$ AM. If the Auxiliary Section plug-in is being used, set the test oscillator to an output of 0.9 Vrms .
12. Measure the total harmonic distortion. With the trace peaked on the display, the distortion should be less than $5 \%$.

## PERFORMANCE TESTS

## 4-25. INCIDENTAL PHASE MODULATION

SPECIFICATION:
At $30 \% \mathrm{AM}<0.2$ radians

## DESCRIPTION:

The phase difference between the signal generators is monitored with a vector voltmeter. Amplitude modulation is applied to the system under test. The peak-to-peak phase variation incidental to the amplitude modulation is read on the vector voltmeter.


Figure 4-11. Incidental Phase Modulation Test Setup.
EQUIPMENT:
Synthesized Signal Generator . . . . . . . . HP 8660C/86602B/86631B
Function Generator . . . . . . . . . . . . . . HP 203A
Vector Voltmeter (with $10: 1$ voltage divider

| probe) . . . . . . . . . . . . . . . . . . . . HP 8405A |
| :--- |


| AC Voltmeter . . . . . . . . . . . . . . . . . . . . HP 403B |
| :--- |
| Mixer . . . . . . . . . . . . . . . . . . . . Watkins-Johnson M1J |

## PERFORMANCE TESTS

## 4-25. INCIDENTAL PHASE MODULATION (Cont'd)

## PROCEDURE:

1. Set the system under test rear panel reference selector to external, center frequency 500 MHz , output level -10 dBm (OUTPUT RANGE -10 dBm ) and AM mode to off.
2. Set the reference system center frequency to 510 MHz and the output level to +7 dBm (OUTPUT RANGE +10 dBm ).
3. Connect the equipment as shown in Figure 4-11.
4. Adjust the vector voltmeter's frequency range control to 10 MHz , phase range switch to $\pm 18^{\circ}$, and the phase meter offset switch for a near or on scale phase reading (Phase reading will drift somewhat due to phase drift in the synthesized signal generator outputs).
5. Set the system under test modulation mode to AM, the source to external, and the modulation level to $30 \%$. Set the input level to 0.3 Vrms at 1 kHz if an auxiliary section is inserted into the mainframe of the system under test. If a modulation section is used, the input level should be 1.5 Vrms at 1 kHz . Use the external dc source if an 86632 B or 86633 B Modulation Section is used.
6. Set the function generator controls for a modulation rate of 0.5 Hz . (The low rate is necessary for the vector voltmeter's metering circuitry. The modulation level is still $30 \%$.)
7. The phase reading will vary at a 0.5 Hz rate. If necessary, readjust the vector voltmeter's phase meter offset switch for an on scale reading.
8. Note the peak-to-peak phase variation caused by the 0.5 Hz AM . Visually disregard the random phase variations caused by phase drift in the synthesized signal generator outputs. Divide the reading by 2 to obtain the peak phase deviation. The phase deviation should be less than $11.5^{\circ}$ - peak ( 0.2 radians-peak)

## PERFORMANCE TESTS

## 4-26. FREQUENCY MODULATION DISTORTION

## SPECIFICATION:

Total harmonic distortion for modulation rates up to $20 \mathrm{kHz},<1 \%$ up to 200 kHz peak deviation.
Distortion from an external source must be $<0.3 \%$ to meet these specifications.

## NOTES

1. In the FM mode, typical Residual FM in a 0.3 to 3 kHz audio bandwidth is $<15 \mathrm{~Hz}$ and may limit minimum Noise and Distortion measurements at deviations $<2 \mathrm{kHz}$ peak.
2. If the signal generator system does not meet the FM distortion specification, refer to the System's Troubleshooting information in Section VIII (Service Sheet 1) in this manual.


Typical FM Distortion Curve

## DESCRIPTION:

A test oscillator input is used to frequency modulate the RF OUTPUT of the Synthesized Signal Generator System. The output is connected to a FM discriminator. To eliminate the carrier, the demodulated signal is passed through a 100 kHz lowpass filter at the discriminator output. The amplitude of the first harmonic is established as the reference level on the wave analyzer. The levels of the second and third harmonics are measured, added, and the total is compared to the reference level to indicate the level of FM distortion.

## NOTE

This procedure is valid only if the HP 86635A is used.

## PERFORMANCE TESTS

## 4-26. FREQUENCY MODULATION DISTORTION (Cont'd)



Figure 4-12. Frequency Modulation Distortion Test Setup.
EQUIPMENT:

> FM Discriminator
> Wave Analyzer . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 210 A
> Function Generator . . . . . . . . . . . . . HP 3581A

## NOTE

This performance test is normally performed with either an HP model 86632B or 86635A Modulation Section inserted into the signal generator mainframe. Control settings in parenthesis apply only to the Model 86633B.

1. Set the signal generator system center frequency to 8.5 MHz and set the OUTPUT RANGE switch to +10 dBm . Adjust the VERNIER control for a -3 dB meter reading.
2. Connect equipment as illustrated in Figure 4-12.
3. Set Modulation Section MODE to FM X10 (FM X1) and source switch to EXTERNAL AC. Adjust Modulation Section modulation level control for $200 \mathrm{kHz}(100 \mathrm{kHz})$ peak deviation and press FM CF CAL switch.

## NOTE

The $86633 B$ does not have an FM CF CAL switch.
4. Set the function generator output for 10 kHz at 1.5 Vrms .
5. Install a 100 kHz low pass filter in the FM Discriminator. (Refer to the FM Discriminator Operating and Service Manual for details ).

## PERFORMANCE TESTS

## 4-26. FREQUENCY MODULATION DISTORTION (Cont'd)

6. Adjust the FM Discriminator for 1 volt rms input sensitivity. Set the controls for the 10 MHz range.
7. Set the wave analyzer scale switch to 90 dB , reference level to normal, resolution bandwidth 30 Hz , sweep mode off, and AFC on.
8. Peak the meter reading near 10 kHz with the frequency control. Verify that the AFC locks and the amplitude is $\approx-37 \mathrm{dBV}$ ( 14.4 mVrms ). Use the input sensitivity switch and vernier control and the amplitude reference level control to establish a reference level at 0 dB .
9. Set the frequency to $\approx 20 \mathrm{kHz}$ (second harmonic) and peak the meter reading. Record the meter reading.
10. Set the frequency to $\approx 30 \mathrm{kHz}$ (third harmonic) and peak the meter reading. Record the meter reading.
11. Use Table 4-1 to obtain power ratios for the levels recorded in steps 8 and 9 . Then use Table $4-1$ to find the dB level corresponding to the sum of the ratios. The resultant level should be $\geqslant 40 \mathrm{~dB}$ down from the fundamental frequency level. Record the level.

40 dB down $\qquad$

## 4-26. FREQUENCY MODULATION DISTORTION (Cont'd)

Table 4-1. dB To Power Ratio Conversion

| dB | Power Ratio $\times 10^{-4}$ | dB | Power Ratio $\times 10^{-4}$ |
| :---: | :---: | :---: | :---: |
| 20 | 100.00000 | 46 | .25119 |
| 21 | 79.43282 | 47 | .19953 |
| 22 | 63.09573 | 48 | .15849 |
| 23 | 50.11872 | 49 | .12589 |
| 24 | 39.81072 | 50 | .10000 |
| 25 | 31.62278 | 51 | .07943 |
| 26 | 2.11886 | 52 | .06310 |
| 27 | 19.95262 | 53 | .05012 |
| 28 | 15.84893 | 54 | .03981 |
| 29 | 12.58925 | 55 | .03162 |
| 30 | 10.00000 | 56 | .02512 |
| 31 | 7.94328 | 57 | .01995 |
| 32 | 6.30957 | 58 | .01585 |
| 33 | 5.01187 | 59 | .01259 |
| 34 | 3.98107 | 60 | .01000 |
| 35 | 3.16228 | 61 | .00794 |
| 36 | 2.51189 | 62 | .00631 |
| 37 | 1.99526 | 63 | .00501 |
| 38 | 1.58489 | 64 | .00398 |
| 39 | 1.25893 | 65 | .00316 |
| 40 | 1.00000 | 66 | .00251 |
| 41 | .79433 | 67 | .00200 |
| 42 | .63096 | 68 | .00158 |
| 43 | .50119 | 69 | .00126 |
| 44 | .39811 | 70 | .00100 |
| 45 | .31623 |  |  |

4-27. INCIDENTAL AM

## SPECIFICATION:

AM sidebands $>60 \mathrm{~dB}$ down from carrier with FM peak deviation of 75 kHz at a 1 kHz rate.

## DESCRIPTION:

A reference is established on the wave analyzer by detecting an AM signal of known modulation level and rate from the Synthesized Signal Generator System. The output is frequency modulated at a specified rate and level. The incidental AM level is detected during frequency modulation and compared to the carrier amplitude.

## 4-27. INCIDENTAL AM (Cont'd)



Figure 4-13. Incidental AM Test Setup

## EQUIPMENT:

Wave Analyzer . . . . . . . . . . . . . . HP 3581A
Crystal Detector . . . . . . . . . . . . . . . . . HP 8471A
15 kHz Low Pass Filter
. . . . . . . . . . . . . . (See Figure 1-3)
Resistor 10K . . . . . . . . . . . . . . .
Capacitor 1500 pF . . . . . . . . . . . . . . . . . HP 0157-0442

## PROCEDURE:

1. Set the signal generator system controls for a center frequency of $100 \mathrm{MHz}, \mathrm{a}+3 \mathrm{dBm}$ output level, the amplitude modulation mode, an internal source at 1 kHz rate, and a modulation level of $50 \%$.
2. Connect the equipment together as shown in Figure 4-13.
3. Set the wave analyzer controls for the 90 dB scale, AFC on, and resolution bandwidth 30 Hz . Tune the wave analyzer for a peak meter indication near 1 kHz . Set a reference level of 0 dB using the input sensitivity switch and the amplitude reference switch. This reference level (AM sidebands) is 12 dB down from carrier signal ( $50 \% \mathrm{AM}$ ).
4. Set the system modulation section controls for FM mode, and a modulation level of 75 kHz peak deviation.
5. The meter reading should be $>48 \mathrm{~dB}$ down ( $>60 \mathrm{~dB}$ down from carrier).
$\qquad$

## 4-28. SPURIOUS SIGNALS, NARROWBAND

## SPECIFICATION:

All narrowband spurious signals in the $\mathrm{CW}, \mathrm{AM}$, and $\phi \mathrm{M}$ modes are:
80 dB down from carrier at frequencies $<700 \mathrm{MHz}$
80 dB down from carrier within 45 MHz of the carrier at frequencies $\geqslant 700 \mathrm{MHz}$
50 dB down from carrier on the +10 dBm range.
ALL power line related spurious signals are 70 dB down from the carrier.

## DESCRIPTION:

The outputs of two Synthesized Signal Generator Systems which use the same time base reference are mixed and the difference frequency is amplified and coupled to the wave analyzer. A reference level is established, various selected frequencies are then set on the two generator systems, and the spurious signal levels are measured.


Figure 4-14. Narrowband Spurious Signal Test Setup.
EQUIPMENT:


## PROCEDURE:

1. Connect the equipment as illustrated in Figure 4-14.
2. Connect rear panel REFERENCE OUTPUT from reference system to rear panel REFERENCE INPUT of system under test. Set REFERENCE SELECTOR of system under test to EXT.
3. On reference system, set the mainframe center frequency to 500.001 MHz , the OUTPUT RANGE switch to +10 dBm , and adjust VERNIER control to a -3 dB meter reading.

## 4-28. SPURIOUS SIGNALS, NARROWBAND (Cont'd)

4. On system under test, set mainframe center frequency to 500 MHz , the RF Section OUTPUT RANGE switch to -80 dBm , and adjust VERNIER control to 0 dB indication on meter scale.
5. Set the wave analyzer scale switch to 90 dB , amplitude reference to $-60, \mathrm{dBV}$ mode, resolution bandwidth 3 Hz , display smoothing to max, and AFC on.
6. Set wave analyzer frequency control to 1 kHz and adjust the input sensitivity for a 0 dB indication on meter scale.
7. On system under test, set the OUTPUT RANGE switch to -10 dBm and adjust VERNIER to 0 dB indication on meter scale.
8. On reference system and system under test, set mainframe center frequency values to those listed in Table 4-2 and verify that levels of corresponding spurious signals are in accordance with specification. The corrected reading of spurious level relative to carrier is $70 \mathrm{~dB}-( \pm$ difference level), therefore a reading of -13 dB relative to the reference level (step 6) gives the spurious signal level. $70 \mathrm{~dB}-$ $(-13 \mathrm{~dB})=83 \mathrm{~dB}$ down.

NOTE
It may be necessary to slightly readjust the Wave Analyzer Frequency control to locate the spurious signal.

Table 4-2. Narrowband Spurious Signals Checks

| System Under Test | Reference System | Level Measured <br> (dB down) |
| ---: | ---: | :---: |
| 100.280000 MHz | 100.561000 MHz | $80 \mathrm{~dB}-$ |
| 200.280000 MHz | 200.561000 MHz | 80 dB |
| 409.720000 MHz | 409.441000 MHz | $80 \mathrm{~dB}-$ |
| 509.720000 MHz | 509.441000 MHz | 80 dB |
| 1109.720000 MHz | 1109.441000 MHz | $80 \mathrm{~dB}-$ |
| 1209.720000 MHz | 1209.441000 MHz | $80 \mathrm{~dB}-$ |

## 4-29. SPURIOUS SIGNALS, WIDEBAND

## SPECIFICATION:

All wideband non-harmonically related spurious signals in the $\mathrm{CW}, \mathrm{AM}$, and $\phi \mathrm{M}$ modes are:
80 dB down from carrier at frequencies $<700 \mathrm{MHz}$
80 dB down from carrier $>45 \mathrm{MHz}$ from carrier at frequencies $\geqslant 700 \mathrm{MHz}$
50 dB down from carrier on the +10 dBm range.

## PERFORMANCE TESTS

## 4-29. SPURIOUS SIGNALS, WIDEBAND (Cont'd)

## DESCRIPTION:

The RF OUTPUT of the Synthesized Signal Generator System is monitored by a spectrum analyzer after being passed through a 2200 MHz low pass filter. Selected signals which fall within the specified range are measured.


Figure 4-15. Wideband Spurious Signal Test Setup
EQUIPMENT:
Spectrum Analyzer . . . . . . . . . . . HP 8555A/8552B/140T
Low Pass Filter ( 2200 MHz )
Low Pass Filter ( 2200 MHz ) . . . . . . . . HP 360C

## PROCEDURE:

1. Connect equipment as illustrated in Figure 4-15.
2. With the RF Section OUTPUT RANGE switch set to +10 dBm and VERNIER control adjusted for 0 dB meter indication, set mainframe center frequency to those values listed in Table 4-3 and adjust the Spectrum Analyzer to measure corresponding spurious signal level relative to the carrier.

Table 4-3. Wideband Spurious Signals Checks

| Mainframe Frequency | Spurious Frequency | Level Measured |
| :---: | :---: | :--- |
| 1299.9 MHz | 150 MHz | 50 dB down |
|  | 1150 MHz | 50 dB down |
|  | 1450 MHz | 50 dB down |
| 1000 MHz | 950 MHz | 50 dB down |
|  | 1050 MHz | 50 dB down |
|  | 950 MHz | 50 dB down |
| 999.9 MHz | 1050 MHz | 50 dB down |
|  | 750 MHz | 50 dB down |
| 800.0 MHz | 850 MHz | 50 dB down |
| 799.9 MHz |  |  |

## PERFORMANCE TESTS

## 4-30. PHASE MODULATION PEAK DEVIATION

## SPECIFICATION:

0 to 100 degrees peak. May be overdriven to 2 radians ( $115^{\circ}$ ) in Modulation Section external dc mode.
NOTE
To check Phase Modulation peak deviation, refer to Section IV of the appropriate Modulation Section Operating and Service Manual.

## 4-31A. PHASE MODULATION DISTORTION

## SPECIFICATION:

$<5 \%$ up to 1 MHz rates, $<7 \%$ up to 5 MHz rates, and $<15 \%$ up to 10 MHz rates External modulation signal distortion must be $<0.3 \%$ to meet this specification.

## NOTES

1. Using this procedure, the proof of performance for phase modulation distortion is valid only when the HP 86635A Modulation Section is being used in the signal generator system. The change in distortion level from the 20 Hz rate as used in this procedure to the maximum 1 MHz rate is minimal. This procedure is, however, not a complete check for the Model 86634A which can use modulation rates up to 10 MHz .
2. If the signal generator system does not meet the $\phi M$ distortion specification, refer to the System's Troubleshooting information in Section VIII (Service Sheet 1) in this manual.

## DESCRIPTION:

The phase modulated output of the System Under Test is demodulated using a vector voltmeter. The vector voltmeter output is set to a linear portion of its operating range and the total harmonic distortion of the demodulated signal is measured.

## 4-31A. PHASE MODULATION DISTORTION (Cont'd)



Figure 4-16A. Phase Modulation Distortion Test Setup
EQUIPMENT:

$$
\begin{array}{llllllllllll}
\text { Vector Voltmeter } & . & . & . & . & . & . & . & . & \text { HP 8405A } \\
\text { Test Oscillator . . . . . . . . . . . . . . . . . . . HP 651B } \\
\text { Distortion Analyzer . . . . . . . . . . . . . . . . . . HP 333A } \\
50 \Omega \text { Termination . . . . . . . . . . . . . . . . . HP 11593A } \\
\text { Coaxial Tee . . . . . . . . . . . . . . . . . . . HP 1250-0781 }
\end{array}
$$

## PROCEDURE:

1. Set the Synthesized Signal Generator System controls for a center frequency of 10.000000 MHz and an output level of +3 dBm ( 0 dBm range).
2. Set the test oscillator output to 1.5 Vrms at 20 Hz . Set the signal generator system's modulation mode to off.
3. Connect the instruments as shown in Figure 4-16A.
4. Set the vector voltmeter's phase range switch to $\pm 180^{\circ}$. Set the meter offset switch for a phase meter reading of $0 \pm 10^{\circ}$.
5. Set the modulation section controls for the $\phi \mathrm{M}$ mode and a modulation level of $100^{\circ}$ as indicated by the front panel meter.
[^4]
## PERFORMANCE TESTS

## 4-31A. PHASE MODULATION DISTORTION (Cont'd)

6. Measure the total harmonic distortion of the 20 Hz demodulated signal using the distortion analyzer.

Distortion should be $<5 \%$.

## 4-31B. PHASE MODULATION DISTORTION - ALTERNATE PROCEDURE

## SPECIFICATION:

$<5 \%$ up to 1 MHz rates
$<7 \%$ up to 5 MHz rates
$<15 \%$ up to 10 MHz rates

## NOTES

1. The HP Model 86635A Modulation Section has a maximum specified phase modulation rate of 1 MHz . Therefore, only the $<5 \%$ distortion specification is applicable. Because the maximum modulation rate of the Model 86634 A is 10 MHz , all the specified distortion levels apply.
2. If the signal generator system does not meet the $\phi M$ distortion specification, refer to the System's Troubleshooting information in Section VIII (Service Sheet 1) in this manual.

## DESCRIPTION:

The phase modulated output of the System Under Test is demodulated using a phase modulation test set. The harmonic levels are measured with a spectrum analyzer and the total harmonic distoztion is calculated. A low pass filter is used between test oscillator and modulation section to insure that the modulation drive signal has less than $0.3 \%$ distortion.

## 4-31B. PHASE MODULATION DISTORTION - ALTERNATE PROCEDURE (Cont'd)



Figure 4-16B. Phase Modulation Distortion Test Setup (Alternate Procedure)
EQUIPMENT:
Synthesized Signal Generator $. ~ . ~ . ~ . ~ . ~ . ~ . ~ . ~ . ~ H P ~ 8660 C / 86602 B / 86631 B ~$
Test Oscillator . . . . . . . . . . . . . . . . . HP 651B
Mixer . . . . . . . . . . . . . . . . . . Watkins Johnson M1J
Phase Modulation Test Set . . . . . . . . . . . HP 8660C-K10
Spectrum Analyzer . . . . . . . . . . . . . HP 8553B/8552B/140T
Low Pass Filters (1 MHz $600 \Omega ; 1,5$, and
$10 \mathrm{MHz}-50 \Omega) .$.

## PROCEDURE:

1. Set the Test Oscillator to 1 MHz , connect a 1 MHz low pass filter ( 50 ohm for $86634 \mathrm{~A}, 600 \mathrm{ohm}$ for 86635 A ) to appropriate test oscillator output and adjust for 1.7 Vrms output. Connect the rest of the equipment as shown in Figure 4-16B.
2. Set the system under test for 300 MHz center frequency and +3 dBm output ( 0 dBm range). Connect the RF output jack directly to the RF input of the phase modulation test set.
3. Set the system under test controls for $\phi \mathrm{M}$ with a modulation level of $100^{\circ}$ peak deviation.
[^5]
## PERFORMANCE TESTS

## 4-31B. PHASE MODULATION DISTORTION - ALTERNATE PROCEDURE (Cont'd)

4. View the signal generator output on the spectrum analyzer display. Record the level of the second and third harmonics of the demodulated output signal with respect to the fundamental.
5. Use Table 4-1 to obtain power ratios of the harmonics. Then use Table 4-1 to find the dB level corresponding to sum of the two ratios. The resultant level should be $<5 \%$ or $\geqslant 26 \mathrm{~dB}$ down.

86634A 26 dB down $\qquad$ 86635A 26 dB down $\qquad$
6. Set the center frequency of the system under test to 299.9 MHz .
7. Set the test oscillator to $1 \mathrm{MHz}(10 \mathrm{MHz})$, connect the $1 \mathrm{MHz}(10 \mathrm{MHz})$ low pass filter to the appropriate oscillator output ( 50 or $600 \Omega$ ) and adjust for an output of 1.7 Vrms.
8. Repeat steps $3-5$. Total harmonic distortion should be $<5 \%$ or $\geqslant 26 \mathrm{~dB}$ down $(<15 \%$ or $\geqslant 16.5 \mathrm{~dB}$ down).

86634A 16.5 dB down $\qquad$ 86635A 26 dB down $\qquad$
9. Set the center frequency of the system under test to 1200 MHz . Connect the mixer and the reference system as shown in Figure 4-18b.
10. Set the reference system center frequency to 900 MHz with an RF output level of +7 dBm .
11. Increase the RF output level of the system under test (if necessary) until the Phase Modulation Test Set phase locks.
12. Set the test oscillator frequency to $1 \mathrm{MHz}(5 \mathrm{MHz})$. Connect the $1 \mathrm{MHz}(5 \mathrm{MHz})$ low pass filter ( 50 or $600 \Omega$ ) to the oscillator output. Adjust the test oscillator output level to 1.7 Vrms. Set the system under test modulation level to $100^{\circ}$ peak deviation.
13. Repeat steps $3-5$. Total harmonic distortion should be $<5 \%$ or $\geqslant 26 \mathrm{~dB}$ down $(<7 \%$ or $\geqslant 23.1 \mathrm{~dB}$ down).
$\qquad$ 86635A 26 dB down

Table 4-4. Performance Test Record (1 of 6)
Hewlett-Packard
Tested By
Models 86602B/11661
RF Section/Frequency Extension Module
Serial No. $\qquad$ Date

| Para. No. | Test | Results |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Min. | Actual | Max. |
| 4-9. | FREQUENCY RANGE $\begin{aligned} & 1.000000 \mathrm{MHz} \\ & 1299.999999 \mathrm{MHz} \end{aligned}$ | $\begin{aligned} & -1 \mathrm{~Hz} \\ & -1 \mathrm{~Hz} \end{aligned}$ |  | $\begin{aligned} & +1 \mathrm{~Hz} \\ & +1 \mathrm{~Hz} \end{aligned}$ |
| 4-11. | FREQUENCY SWITCHING TIME <br> 6 ms to be within 50 Hz of any new frequency <br> Step $9-30.000000 \mathrm{MHz} \pm 50 \mathrm{~Hz}$ <br> Step $10-29.999999 \mathrm{MHz} \pm 50 \mathrm{~Hz}$ <br> 100 ms to be within 5 Hz of any new frequency <br> Step $14-30.000000 \mathrm{MHz} \pm 5 \mathrm{~Hz}$ <br> Step 15-29.999 $999 \mathrm{MHz} \pm 5 \mathrm{~Hz}$ | $\begin{aligned} & -50 \mathrm{~Hz} \\ & -50 \mathrm{~Hz} \\ & \\ & -5 \mathrm{~Hz} \\ & -5 \mathrm{~Hz} \end{aligned}$ | $\square$ | $\begin{aligned} & +50 \mathrm{~Hz} \\ & +50 \mathrm{~Hz} \\ & +5 \mathrm{~Hz} \\ & +5 \mathrm{~Hz} \end{aligned}$ |
| 4-12. | OUTPUT LEVEL SWITCHING TIME <br> Remote programming of level change on same range accomplished in 5 ms , maximum, at 50 MHz . <br> Step 4-10 to 19 dB <br> Level change to another range accomplished in 50 ms , maximum at 50 MHz . <br> Step 5-10 to 30 dB <br> Remote programming of level change on same range accomplished in 5 ms , maximum, at 1 MHz . <br> Step 6-10 to 19 dB |  |  | 5 ms <br> 50 ms <br> 5 ms |

Table 4-4. Performance Test Record (2 of 6)

| Para. No. | Test | Results |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Min. | Actual | Max. |
| 4-13A. | OUTPUT ACCURACY <br> OUTPUT RANGE Front Panel Meter Reading | $+8.5 \mathrm{dBm}$ <br> $+5.5 \mathrm{dBm}$ <br> $+2.5 \mathrm{dBm}$ <br> - 7.5 dBm <br> - 4.5 dBm <br> $-1.5 \mathrm{dBm}$ <br> $+1.5 \mathrm{dBm}$ <br> - 8.5 dBm <br> $-18.5 \mathrm{dBm}$ <br> $-28.5 \mathrm{dBm}$ <br> $-38.5 \mathrm{dBm}$ <br> - 48.5 dBm <br> - 58.5 dBm <br> - 68.5 dBm <br> - 79.0 dBm <br> - 89.0 dBm <br> - 99.0 dBm <br> $-109.0 \mathrm{dBm}$ <br> $-119.0 \mathrm{dBm}$ <br> $-129.0 \mathrm{dBm}$ |  | $+11.5 \mathrm{dBm}$ <br> $+8.5 \mathrm{dBm}$ <br> $+5.5 \mathrm{dBm}$ <br> - 4.5 dBm <br> $-1.5 \mathrm{dBm}$ <br> $+1.5 \mathrm{dBm}$ <br> $+4.5 \mathrm{dBm}$ <br> - 5.5 dBm <br> $-15.5 \mathrm{dBm}$ <br> - 25.5 dBm <br> - 35.5 dBm <br> - 45.5 dBm <br> - 55.5 dBm <br> - 65.5 dBm <br> - 75.0 dBm <br> - 85.0 dBm <br> - 95.0 dBm <br> $-105.0 \mathrm{dBm}$ <br> $-115.0 \mathrm{dBm}$ <br> $-125.0 \mathrm{dBm}$ |
| 4-13B. | OUTPUT ACCURACY - ALTERNATE <br> PROCEDURE <br> OUTPUT RANGE Front Panel Meter Reading <br> 10 dBm <br> 10 dBm <br> 10 dBm <br> 0 dBm <br> 0 dBm <br> 0 dBm <br> 0 dBm <br> -10 dBm <br> -20 dBm <br> -30 dBm <br> -40 dBm <br> -50 dBm <br> -60 dBm <br> -70 dBm <br> - 80 dBm <br>  <br> Level change from the -70 dB <br> OUTPUT RANGE | $+8.5 \mathrm{dBm}$ <br> $+5.5 \mathrm{dBm}$ <br> $+\quad 2.5 \mathrm{dBm}$ <br> - 7.5 dBm <br> - 4.5 dBm <br> - 1.5 dBm <br> $+\quad 1.5 \mathrm{dBm}$ <br> - 8.5 dBm <br> - 18.5 dBm <br> $-28.5 \mathrm{dBm}$ <br> $-38.5 \mathrm{dBm}$ <br> - 48.5 dBm <br> - 58.5 dBm <br> - 68.5 dBm <br> - 79.0 dBm <br> 9.0 dB |  | $+11.5 \mathrm{dBm}$ <br> $+8.5 \mathrm{dBm}$ <br> $+5.5 \mathrm{dBm}$ <br> - 4.5 dBm <br> - 1.5 dBm <br> $+1.5 \mathrm{dBm}$ <br> $+4.5 \mathrm{dBm}$ <br> - 5.5 dBm <br> - 15.5 dBm <br> - 25.5 dBm <br> - 35.5 dBm <br> - 45.5 dBm <br> - 55.5 dBm <br> - 65.5 dBm <br> - 75.0 dBm <br> 11.0 dB |

Table 4-4. Performance Test Record (3 of 6)

| Para. No. | Test | Results |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Min. | Actual | Max. |
| 4-14. | OUTPUT FLATNESS Reference Level is -1.0 dBm at 1000 MHz . 1 MHz 10 MHz 100 MHz 200 MHz 400 MHz 600 MHz 800 MHz 1299 MHz | - 2.0 dBm <br> - $\quad 2.0 \mathrm{dBm}$ <br> - 2.0 dBm <br> - $\quad 2.0 \mathrm{dBm}$ <br> - $\quad 2.0 \mathrm{dBm}$ <br> - $\quad 2.0 \mathrm{dBm}$ <br> - $\quad 2.0 \mathrm{dBm}$ <br> - $\quad 2.0 \mathrm{dBm}$ |  | 0.0 dBm 0.0 dBm 0.0 dBm 0.0 dBm 0.0 dBm 0.0 dBm 0.0 dBm 0.0 dBm |
| 4-15. | HARMONIC SIGNALS <br> OUTPUT RANGE $=+10 \mathrm{dBm}$ <br> Step 5-1299 MHz Second Harmonic Third Harmonic <br> Step 6-1000 MHz Second Harmonic Third Harmonic <br> Step 6-500 MHz Second Harmonic Third Harmonic <br> Step 6-100 MHz Second Harmonic Third Harmonic <br> Step 6-10 MHz Second Harmonic Third Harmonic <br> OUTPUT RANGE $=0 \mathrm{dBm}$ Step $7-100 \mathrm{MHz}$ Second Harmonic Third Harmonic | 25 dB down 25 dB down <br> 25 dB down 25 dB down <br> 25 dB down 25 dB down <br> 25 dB down 25 dB down <br> 25 dB down <br> 25 dB down <br> 30 dB down <br> 30 dB down |  |  |
| 4-16. | PULSE MODULATION RISETIME Risetime ( $10 \%$ to $90 \%$ amplitude points) |  |  | 50 ns |
| 4-17. | PULSE MODULATION ON/OFF RATIO On/Off Ratio | 40 dB | - |  |

Table 4-4. Performance Test Record (4 of 6)

| Para. No. | Test | Results |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Min. | Actual | Max. |
| 4-18. | AMPLITUDE MODULATION DEPTH <br> AND 3 dB BANDWIDTH <br> Frequency $=500 \mathrm{MHz}$ OUTPUT RANGE $=-10 \mathrm{dBm}$ Rate $=1 \mathrm{kHz}$ <br> Step 13-30\% AM <br> Step 14 - $70 \%$ AM <br> Step 15-90\% AM <br> Frequency $=500 \mathrm{MHz}$ <br> OUTPUT RANGE $=-10 \mathrm{dBm}$ $\mathrm{AM}=30 \%$ <br> Step $19-5 \mathrm{kHz}$ rate (reference 5 div. p-p) <br> AM less than 3 dB down ( $<3.5$ div. p-p) at 100 kHz <br> Frequency-1-9 MHz OUTPUT RANGE $=-10 \mathrm{dBm}$ AM - 30\% <br> Step $21-5 \mathrm{kHz}$ rate (reference 5 div. p-p) <br> AM less than 3 dB down ( $>3.5$ div. p-p) at 10 kHz | 50 mVrms 130 mVrms 170 mVrms <br> 3.5 div. p-p <br> 3.5 div. p-p |  | 70 mVrms 150 mVrms 190 mVrms |
| 4-20. | OUTPUT IMPEDANCE <br> Center Frequency 500 MHz OUTPUT RANGE +10 dBm $\mathrm{dB}=20 \log (\mathrm{VSWR})$ $\mathrm{dB}=6.0$ for $\mathrm{VSWR}=2.0$ <br> OUTPUT RANGE dBm $\mathrm{dB}=6.0$ for VSWR $=2.0$ OUTPUT RANGE -10 dBm $\mathrm{dB}=2.3$ for VSWR $=1.3$ |  | $\longrightarrow$ | $6 \mathrm{~dB}$ <br> 6 dB $2.3 \mathrm{~dB}$ |
| 4-21. | SIGNAL-TO-PHASE NOISE RATIO Noise Level | 45 dB down | - - |  |
| 4-22. | SIGNAL-TO-AM NOISE RATIO <br> Noise Level | 65 dB down | - - |  |

Table 4-4. Performance Test Record (5 of 6)

| Para. No. | Test | Results |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Min. | Actual | Max. |
| 4-24. | AMPLITUDE MODULATION DISTORTION <br> Step 7-30\% AM <br> Total Distortion ( $<1 \%$ ) <br> Step 9-70\% AM <br> Total Distortion ( $<3 \%$ ) <br> Step 11-90\% AM <br> Total Distortion ( $<5 \%$ ) |  |  | 1\% <br> $3 \%$ <br> 5\% |
| 4-25. | INCIDENTAL PHASE MODULATION <br> Step 8 - $<0.2$ radians peak ( $<11.5^{\circ}$ peak) |  |  |  |
| 4-26. | FREQUENCY MODULATION DISTORTION Total Distortion <2\% | 37 dB down |  |  |
| 4-27. | INCIDENTAL AM Incidental AM | 60 dB down |  |  |
| 4-28. | SPURIOUS SIGNALS, NARROWBAND <br> (All spurious signals down from carrier 80 dB minimum.) | 80 dB down 80 dB down 80 dB down 80 dB down 80 dB down 80 dB down |  |  |
| 4-29. | SPURIOUS SIGNALS, WIDEBAND <br> (All spurious signals down from carrier 50 dB , minimum.) | 50 dB down 50 dB down 50 dB down 50 dB down 50 dB down 50 dB down 50 dB down 50 dB down 50 dB down |  |  |

Table 4-4. Performance Test Record (6 of 6)

| Para. <br> No. | Test | Results |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Min. | Actual | Max. |
| 4-31A. | PHASE MODULATION DISTORTION Step 6 - Distortion $(<5 \%) \leqslant 1 \mathrm{MHz}$ rate | <5\% |  |  |
| 4-31B. | PHASE MODULATION DISTORTION ALTERNATE PROCEDURE <br> Step $5-300 \mathrm{MHz}$ at <br> 1 MHz rate $86634 \mathrm{~A}<5 \%$ <br> 1 MHz rate $86635 \mathrm{~A}<5 \%$ <br> Step 6-299.9 MHz at <br> 10 MHz rate $86634 \mathrm{~A}<15 \%$ <br> 1 MHz rate $86635 \mathrm{~A}<5 \%$ <br> Step $13-1900 \mathrm{MHz}$ at <br> 5 MHz rate $86634 \mathrm{~A}<7 \%$ <br> 1 MHz rate $86635 \mathrm{~A}<5 \%$ | 26 dB down 26 dB down <br> 16.5 dB down 26 dB down <br> 23.1 dB down <br> 26 dB down |  |  |

## SECTION V ADJUSTMENTS

## 5-1. INTRODUCTION

5-2. This section contains adjustment procedures required to assure peak performance of the Model 86602B RF Section. The RF Section should be adjusted after any repair or if the unit, in conjunction with the Frequency Extension Module, fails to meet the specifications listed in Section IV of this manual. Prior to making any adjustments, allow the RF Section warmup for 30 minutes.
$5-3$. The order in which some adjustments are made to the RF Section is critical. Perform the adjustments under the conditions presented in this section. Do not attempt to make adjustments randomly to the instrument. Prior to making any adjustments to the RF Section, refer to the paragraph entitled Related Adjustments.

## 5-4. EOUIPMENT REOUIRED

$5-5$. Each adjustment procedure in this section contains a list of test equipment and accessories required to perform the adjustment. The test equipment is also identified by callouts in the test setup diagrams included with each procedure.

5-6. If substitutions must be made for the specified test equipment, refer to Table 1-2 for the minimum specifications of the test equipment to be used in the adjustment procedures. Since the Synthesized Signal Generator System is extremely accurate, it is particularly important that the test equipment used in the adjustment procedures meets the critical specifications listed in the table.
$5-7$. The HP 11672A Service Kit is an accessory item available from Hewlett-Packard for use in maintaining the RF Section. A detailed listing of the items contained in the service kit is provided in the 11672A Operating Note and in Section I of the mainframe manuals. Any item in the kit may be ordered separately.

## 5-8. SAFETY CONSIDERATIONS

5-9. Although this instrument has been designed in accordance with international safety standards, this manual and the system mainframe manual contain
information, cautions, and warnings which must be followed to ensure safe operation and to retain the complete system in safe condition. Service adjustments should be performed only by qualified service personnel.

## NOTE

Refer to the mainframe manual for safety information relating to ac line (Mains) voltage, fuses, protective earth grounding, etc.

5-10. Any adjustment, maintenance, and repair of the opened instrument under voltage should be avoided as much as possible and, when inevitable, should be carried out only by a skilled person who is aware of the hazard involved.

5-11. Capacitors inside the instrument may still be charged even if the instrument has been disconnected from its source of supply.

## WARNING

Adjustments described herein are performed with power supplied to the instrument while protective covers are removed. Energy available at many points may constitute a shock hazard.

## 5-12. FACTORY SELECTED COMPONENTS

5-13. Factory selected components are identified on the schematics and parts list by an asterisk which follows the reference designator. The normal value of the components are shown. The manual change sheets will provide updated information pertaining to the selected components. Table 5-1 lists the reference designator, the criterion used for selecting a particular value, the normal value range, and the service sheet where the component part is shown.

## 5-14. RELATED ADJUSTMENTS

5-15. The RF Output Level and 1 dB Step Attenuator Adjustments interact. The Amplitude Modulation Input Circuit Adjustment is dependent on
and should be performed after the previous mentioned adjustments. The Phase Modulation Level and Distortion Adjustment is affected by and should be performed after the Phase Modulator Driver Frequency Response Adjustment. All other adjustments are independent.

5-16. If the RF Output Level Adjustment is performed, the 1 dB Step Attenuator Adjustment should follow immediately. Repeat these procedures until the RF levels are within the stated limits without further adjustment. Then perform the Amplitude Modulation Input Circuit Adjustment. If the Phase Modulator Driver Frequency Response Adjustment is performed, the Phase Modulation Level and Distortion Adjustment should be performed.

5-17. If the RF Output Level and 1 dB Step Attenuator Adjustments are not performed, the Amplitude Modulation Input Circuit Adjustment may be considered independent. If the Phase Modulator Driver Frequency Response Adjustment is not performed, the Phase Modulation Level and Distortion Adjustment may be considered independent.

## 5-18. ADJUSTMIENT LOCATIONS

5-19. The last foldout in this manual contains a table which cross-references pictorial and schematic locations of the adjustable controls. The figure accompanying the table shows the locations of adjustable controls, assemblies, and chassis-mounted parts.

## 5-20. ADJUSTMENTS

$5-21$. Before performing the adjustment procedures (1) disconnect the mainframe (Mains) Power

Cable, (2) remove the RF Section from the mainframe, and (3) remove the RF Section covers. At this point, the RF Section is either reinserted into the mainframe or connected to the mainframe with interconnection cables supplied in the Service Kit. If the RF Section is reinserted into the mainframe for adjustments, the mainframe top and/or right side covers must be removed. Refer to the lefthand foldout page immediately preceding the last foldout in this manual for procedures explaining how to remove the RF Section from the mainframe, the RF Section cover removal, and how to interconnect the RF Section and mainframe for adjustments.

## NOTE

It may be necessary to remove the upper guide rail to gain access to some of the adjustable components.

## 5-22. POST ADJUSTMENT TESTS

5-23. After adjustments are performed verify that the system performance is within the parameters specified for the RF Section and Frequency Extension Module. Perform the applicable performance test(s) found in Section IV.

## WARNING

The multi-pin plug connector (on mainframe), which provides interconnection to the RF Section, will expose power supply voltages which may remain on the pins after the RF Section is removed and after the (Mains) power cable is disconnected from the mainframe. Be careful to avoid contact with the pins during interconnection with RF Section.

Table 5-1. Factory Selected Components

| Reference <br> Designator | Selected For | Normal Value <br> Range | Service <br> Sheet |
| :---: | :--- | :---: | :---: |
| A4R17 | Accurately sets the 10 dB difference in <br> the power output between OUTPUT <br> RANGE switch settings of +10 and 0 dBm <br> (the VERNIER control is not moved). | $237 \Omega$ | 6 |
| A16R5 | Sets the adjustment range of the Gain <br> Tracking Control A16R4. Refer to the <br> Phase Modulator Driver Adjustments <br> procedure. | 10 to $316 \Omega$ | 5 |

## ADJUSTMENTS

## 5-24. RF OUTPUT LEVEL ADJUSTMENT

## REFERENCE:

Service Sheet 6.

## DESCRIPTION:

The Meter and Detector Bias controls are adjusted alternately at specific RF Output levels until the VERNIER'S control of the RF Output is linear across the control range.


Figure 5-1. RF Output Level Adjustment Test Setup

## EQUIPMENT:

Power Meter/Sensor . . . . . . . . . . . . HP 435A/8481A
PROCEDURE:

## NOTE

Prior to performing the procedure, clean the meter face with antistatic glass cleaner.*

1. Extract the RF Section from the mainframe. Remove the mainframe top cover and the RF Section covers. Insert the RF Section into the mainframe.
2. Zero the external Power Meter.
3. Interconnect the equipment as illustrated in Figure 5-1.
4. Set the system's center frequency to 1000 MHz and the RF Section's OUTPUT RANGE switch to the 0 dBm position.
5. Adjust the VERNIER control for $\mathrm{a}+3.0 \mathrm{dBm}$ indication on the external Power Meter.
6. Adjust MTR potentiometer A4R26 for a +3.0 dB indication on the front panel meter.
7. Adjust the VERNIER control for a front panel meter indication of -6.0 dB .
8. Adjust the BIAS potentiometer A4R13 for a -6.0 dBm indication on external Power Meter.
9. Repeat steps 5 through 8 until the RF Section's front panel meter indicates power levels that are within $\pm 0.3 \mathrm{~dB}$ of the external Power Meter indications with no further adjustment.
[^6]
## ADJUSTMENTS

## 5-25. 1 dB STEP ATTENUATOR ADJUSTMENT

REFERENCE:
Service Sheet 7.
DESCRIPTION:
RF Level and RF Linearity controls are adjusted alternately at specific RF Output levels until the programmed 1 dB step control of RF Output is linear across the range ( 10 dB ).


Figure 5-2. 1 dB Step Attenuator Adjustment Test Setup
EQUIPMENT:

$$
\begin{aligned}
& \text { Marked Card Programmer } \\
& \text { Power Meter/Sensor . . . . . . . . . . . HP 3260A Opt } 001 \\
&
\end{aligned}
$$

## PROCEDURE:

1. Connect the equipment as illustrated in Figure 5-2.
2. Zero the external Power Meter.
3. Use a Marked Card Programmer to program the mainframe for a center frequency of 1000 MHz and the RF Section for an output power level of +3 dBm .
4. Adjust the RF Section's RF Level Control A10R7 for a +3.0 dBm indication on the power meter.
5. Use the Marked Card Programmer to program the RF Section for an output power level of -6 dBm .
6. Adjust the Linearity control A3R4 for a -6.0 dBm indication on the power meter.
7. Repeat steps 3 through 6 until the programmed output power levels are within $\pm 0.3 \mathrm{~dB}$ of the required power meter indication.
8. Recheck the power meter readings for the RF Output Level Adjustments. If necessary, perform the adjustments again. Then check the power meter readings for this procedure. Alternately perform one procedure and check the power meter readings on the other until the RF levels are within tolerance without further adjustment.

## 5-25. 1 dB STEP ATTENUATOR ADJUSTMENT (Cont'd)

9. Perform the Amplitude Modulation Input Circuit Adjustments.

## 5-26. AMPLITUDE MODULATION INPUT CIRCUIT ADJUSTMENT

## REFERENCE:

Service Sheet 7.

## DESCRIPTION:

A specific modulation drive level is coupled to the RF Section. The RF output signal is demodulated by a peak detector in a spectrum analyzer (when the frequency-span width is set to zero). The ac and dc components are measured with a voltmeter at the detector (vertical) output. First, the dc component is set to -283 mVdc plus the detector offset correction. Then, the ac component is measured. The AM level (\%) is $1 / 2$ (one half) the rms output.

Because of the required measurement accuracy, the accuracy of the spectrum analyzer's detector offset must be known to $\pm 2 \mathrm{mVdc}$. The offset voltage is calculated by measuring the change in the detector output for a change in the RF input and assuming a linear detector over the range of the levels used.


Figure 5-3. Amplitude Modulation Input Circuit Adjustment Test Setup


## ADJUSTMENTS

## 5-26. AMPLITUDE MODULATION INPUT CIRCUIT ADJUSTMENT (Cont‘d)

## PROCEDURE:

1. Remove the RF Section from the mainframe. Remove the mainframe top cover and the RF Section covers. Insert the RF Section into the mainframe.
2. Connect the equipment as shown in Figure 5-3.
3. Set the synthesized signal generator controls as follows: center frequency 30 MHz , OUTPUT RANGE 0 dBm . VERNIER control for a panel meter reading of +3 dB , and AM off.
4. Let the spectrum analyzer warm up for 1 hour to minimize drift of the spectrum analyzer detector output. Set the 10 dB step attenuator to 10 dB attenuation.
5. Set the spectrum analyzer center frequency to 30 MHz , frequency span per division 5 MHz , resolution bandwidth 300 kHz ; input attenuation to 20 dB , and vertical sensitivity per division 10 dB . Adjust the center frequency control to center the display. Set the frequency span to zero and tune to peak the trace.

## NOTE

Throughout this test, continually check that the signal is peaked for maximum deflection. Tune the center frequency control for maximum signal deflection.
6. Set the vertical scale to linear and adjust the reference level vernier for a digital voltmeter reading of -200 mVdc.
7. Set the 10 dB step attenuator to 0 dB and record the digital voltmeter reading.
mVdc
8. Set the 10 dB Step Attenuator to 20 dB and record the digital voltmeter reading.
9. Calculate the offset voltage using the following formula:

$$
\mathrm{V}_{\mathrm{off}}=\frac{\mathrm{mVdc}+200 \alpha}{1-\alpha}
$$

Where $\quad V_{\text {off }}$ is the offset voltage in millivolts mVdc is the DVM reading in millivolts. $\alpha$ is 3.16 (step 7) and 0.316 (step 8).

For example:

$$
\begin{gathered}
\mathrm{mVdc}=-687 \mathrm{in} \mathrm{step} 7 \\
\text { Therefore } \\
\mathrm{V}_{\text {off }}=\frac{-687+200(3.16)}{1-(3.16)}=+25.5 \mathrm{mVdc}
\end{gathered}
$$

10. Find the value of $\mathrm{V}_{\text {off }}$ for step 8. The difference between the two should be $<4 \mathrm{mVdc}$. Use the average value of $\mathrm{V}_{\text {off }}$.
$\mathrm{V}_{\text {off }}=$ mVdc

## ADJUSTMENTS

## 5-26. AMPLITUDE MODULATION INPUT CIRCUIT ADJUSTMENT (Cont'd)

11. Set the 10 dB step attenuator to 10 dB .
12. Set the system center frequency to 1000 MHz , the modulation mode to AM , the modulation source to external, and a modulation level of $50 \%$ ( 0.5 Vrms input to an Auxiliary Section) at a 1 kHz rate.
13. Set the spectrum analyzer center frequency control to 1000 MHz , and set the reference level vernier for digital voltmeter reading of $-283 \mathrm{mVdc}+\mathrm{V}_{\text {off }}$. See Step 10 .
14. Set the DVM controls to measure the peak detector's ac component. The modulation level (\%) is $1 / 2$ (one-half) the DVM reading (Vrms). Adjust the AM CAL Control A10R5 for a reading of 100 mVrms .
15. Set the RF Section's VERNIER control for a front panel meter reading of -6 dB .
16. Set the DVM to monitor the dc vertical output. Reset the DVM reading of $-283 \mathrm{mVdc}+\mathrm{V}_{\text {off }}$.
17. Set the DVM to monitor the ac vertical output. Adjust the AM Linearity control A10R2 for a DVM reading of 100 mVrms .
18. Repeat steps 13 through 17 until the DVM reading is $100 \pm 2 \mathrm{mVrms}$ at RF Section meter readings of +3 and -6 dB without further adjustment.

## 5-27. PHASE MODULATOR DRIVER FREQUENCY RESPONSE ADJUSTMENTS

## REFERENCE:

## Service Sheet 5 .

## DESCRIPTION:

The output of a sweep generator is connected to the A16 Phase Modulator Driver Assembly input while a spectrum analyzer monitors the system's phase modulated RF output. The frequency response control is adjusted for maximum flatness to $\pm 40 \mathrm{MHz}$ and for minimum peaking at 80 MHz .


Figure 5-4. Phase Modulator Driver Frequency Response Adjustment Test Setup

## ADJUSTMENTS

## 5-27. PHASE MODULATOR DRIVER FREQUENCY RESPONSE ADJUSTMENTS (Cont'd)

## EQUIPMENT:

$$
\begin{aligned}
& \text { Sweep Generator . . . . . . . . . . . . . HP 8601A } \\
& \text { Spectrum Analyzer . . . . . . . . . . . . HP 8555A/8552B/140T }
\end{aligned}
$$

## PROCEDURE:

1. Remove the RF Section from the mainframe. Remove the mainframe top cover and the RF Section covers and top guide rail.
2. Remove cable W12 from the $\phi \mathrm{M}$ Input A16J1 and wrap the connector with insulating tape. Connect 11672-60005 (from the Service Kit) to A16J1. Route the BNC end of cable into the cavity and out through the top of the mainframe. Carefully reinstall the RF Section so as not to damage the cables.
3. Set the sweep generator controls as follows: sweep range 110 MHz , frequency 80 MHz , output level -10 dBm , sweep video, sweep mode free; slow.
4. Connect the equipment as shown in Figure 5-6.
5. Set the synthesized signal generator controls for a center frequency of 1.05 GHz and an output level of 0 dBm .
6. Set the spectrum analyzer controls for center frequency of 1.05 GHz , frequency span per division 20 MHz , resolution bandwidth 300 kHz . input attenuation 30 dB , vertical sensitivity per division 10 dB , and sweep time per division 2 ms .
7. Adjust the sweep generator output level so the sidebands are approximately 34 dB below the carrier level.
8. Set the spectrum analyzer vertical sensitivity per division to 2 dB .
9. Adjust the Frequency Response Control A16C8 for maximum flatness within 40 MHz of the carrier and for the minimum peaking at 80 MHz .
10. Disconnect the sweep generator from the A16 Assembly and set the signal generator LINE switch to STBY.
11. Carefully remove the RF Section. Be careful not to damage the cables. Reconnect W12 to A16J1.

## 5-28A. PHASE MODULATION LEVEL AND DISTORTION ADJUSTMENTS

## REFERENCE:

Service Sheet 5.

## DESCRIPTION:

The phase modulated signal from the synthesized signal generator is monitored by a spectrum analyzer and is adjusted to the modulation level indicated by the modulation level meter. The phase modulated signal is then mixed down, the difference frequency is connected to an FM discriminator, and the detected output is connected to the spectrum analyzer. The adjustments are set to minimize harmonic distortion. The modulation level and distortion adjustments are repeated until both are within the required accuracy.

## ADJUSTMENTS

5-28A. PHASE MODULATION LEVEL AND DISTORTION ADJUSTMENTS (Cont‘d)


Figure 5-5A. Phase Modulation Level and Distortion Adjustment Test Setup
EQUIPMENT:

```
Spectrum Analyzer . . . . . . . . . . . . HP 8553B/8552B/140T
Synthesized Signal Generator System . . . . . HP 8660C/86603A/86631B
Test Oscillator . . . . . . . . . . . . . . HP 651B
FM Discriminator . . . . . . . . . . . . HP 5210A
Mixer, Doubler Balanced . . . . . . . . . . HP 10514A
Low Pass Filters (100 kHz at 50\Omega or 600\Omega) . . Special (See Figure 1-4)
```


## PROCEDURE:

1. Extract the RF Section from mainframe. Remove the mainframe top cover, the RF Section covers, and the top guide rail. Insert the RF Section back into the mainframe.
2. Connect the equipment as shown in Figure 5-5A. Connect the output of the System Under Test directly to the spectrum analyzer RF input. Be sure to use the correct test oscillator output and the correct low pass filter.
3. Set the test oscillator output to 100 kHz at 1.5 Vrms.
4. Set the System Under Test center frequency to 100 MHz with a 0 dBm OUTPUT level.
[^7]
## ADJUSTMENTS

## 5-28A. PHASE MODULATION LEVEL AND DISTORTION ADJUSTMENTS (Cont'd)

5. Set the spectrum analyzer controls for a center frequency of 100 MHz , resolution bandwidth of 10 kHz , frequency span per division of 0.5 MHz , sweep time per division of 10 ms , input attenuation of 30 dB , vertical scale per division to 2 dB and adjust the reference level to a readable level.
6. Set the Modulation Section controls for $\phi \mathrm{M}$ mode, external AC source, and a modulation level of exactly $82^{\circ}$ as read on the front panel meter.
7. Adjust A16R2 so the carrier and first sidebands are of equal amplitude.
8. Step the System Under Test center frequency down 1 Hz to 99.999999 MHz . The carrier and first sidebands should be within 0.5 dB . If the difference is less than or equal to 0.4 dB , proceed to step 11. If the difference is greater than 0.5 dB and if the $\phi \mathrm{M}$ deviation is $<82^{\circ}$ (first sideband is of lower amplitude than the carrier) proceed to step 9 . If the $\phi \mathrm{M}$ deviation is $>82^{\circ}$ proceed to step 10 .
9. Adjust A16R4 one-eighth turn ccw. If A16R4 is in contact with the ccw stop, increase the value of A16R5. (The normal value range is 10 to $316 \Omega$.) Set the frequency of the System Under Test to 100 MHz and repeat steps 7 and 8.
10. Adjust A16R4 one-eighth turn cw. If A16R4 is in contact with the cw stop, decrease the value of A16R5. (The normal value range is 10 to $316 \Omega$.) Set the frequency of the System Under Test to 100 MHz and repeat steps 7 and 8.
11. Set the FM discriminator controls for the 10 MHz range and the 0.1 V sensitivity, and insert an internal 1 MHz low-pass filter.
12. Set the spectrum analyzer controls for a center frequency of 200 kHz , resolution bandwidth to 3 kHz , frequency span per division to 50 kHz , input attenuation to 0 dB , log reference level to a convenient level, vertical sensitivity per division to 10 dB , and scan time per division to 10 ms .
13. Set the Reference System controls for a center frequency of 309 MHz and an output level of +7 dBm .
14. Set the System Under Test center frequency to 300 MHz with a modulation level of $100^{\circ}$ as read on the front panel meter.
15. Refer to Figure $5-5 \mathrm{~A}$ and connect the System Under Test OUTPUT to the "RF" input of the mixer. Connect the FM Discriminator output to the spectrum analyzer RF input.
16. Adjust the spectrum analyzer's reference level control so the peak of the fundamental 100 kHz signal is viewed on the CRT display at the log reference graticule line.
17. Adjust A16R3 to null the second harmonic level; adjust A16R1 to null the third harmonic level.

## NOTE

Observing harmonic distortion of a $\phi M$ signal after passing it through an $F M$ discriminator results in an increase in level of 6 dB per octave. Therefore, the second harmonic will be 6 dB higher and the third harmonic 9.5 dB higher than with a phase demodulator.

## 5-28A. PHASE MODULATION LEVEL AND DISTORTION ADJUSTMENTS (Cont'd)

18. Step the System Under Test center frequency down 1 Hz . Note the direction and amount of readjustment of A16R3 and R1 necessary to null the second and third harmonics.
19. Set A16R3 and R1 for the best compromise (minimum second and third harmonic levels) at both center frequency settings of 299.999999 and 300 MHz .
20. Repeat steps 4 through 20 until all the conditions below are met without further adjustment.
a. Carrier and first sidebands are equal within 0.5 dB when changing Center Frequency of System Under Test between 100 and 99.999999 MHz (Steps 7-8).
b. Second harmonic levels are equal within 4 dB or $>40 \mathrm{~dB}$ down from the fundamental as indicated by the spectrum analyzer at center frequencies of 300 and 299.999999 MHz (Step 19).
c. Third harmonic levels are equal within 4 dB or $>35 \mathrm{~dB}$ down from the fundamental as indicated by the spectrum analyzer frequencies of 300 and 299.999999 MHz (Step 19).
21. Replace the mainframe cover and wait 10 minutes. Check to see if the conditions outlined in step 21 are still met. If not repeat steps 4 through 21 .

## 5-28B. PHASE MODULATION LEVEL AND DISTORTION ADJUSTMENTS - ALTERNATE PROCEDURE

## REFERENCE:

Service Sheet 5.

## DESCRIPTION:

The phase modulated signal from the synthesized signal generator is monitored by a spectrum analyzer and is adjusted to the modulation level indicated by the modulation level meter. The phase modulated signal is then mixed down, the difference frequency is connected to a phase demodulator, and the detected output is connected to the spectrum analyzer. The adjustments are set to minimize harmonic distortion. The modulation level and distortion adjustments are repeated until both are within the required accuracy.

ADJUSTMENTS

## 5-28B. PHASE MODULATION LEVEL AND DISTORTION ADJUSTMENTS - ALTERNATE PROCEDURE (Cont'd)



Figure 5-5B. Phase Modulation Level and Distortion Adjustment Test Setup (Alternate Procedure)

EQUIPMENT:
Spectrum Analyzer . . . . . . . . . . . . HP 8553B/8552B/140T
Test Oscillator . . . . . . . . . . . . . HP 651B
Low Pass Filters (1 MHz at $50 \Omega$ or $600 \Omega$ )
Phase Modulation Test Set . . . . . . . . . Hpecial (See Figure 1-4)

## PROCEDURE:

1. Extract the RF Section from mainframe. Remove the mainframe top cover, the RF Section covers, and the top guide rail. Insert the RF Section back into the mainframe.
2. Connect the equipment as shown in Figure 5-5B. Connect the output of the System Under Test directly to the spectrum analyzer RF input. Be sure to use the correct test oscillator output and the correct low pass filter.
3. Set the test oscillator output to 100 kHz at 1.5 Vrms.
4. Set the System Under Test center frequency to 100 MHz with a 0 dBm OUTPUT level.
5. Set the spectrum analzer controls for a center frequency of 100 MHz , resolution bandwidth of 10 kHz , frequency span per division of 0.5 MHz , sweep time per division of 10 ms , input attenuation of 30 dB , vertical scale per division of 2 dB , and adjust the reference level to a readable level.
6. Set the Modulation Section controls for $\phi \mathrm{M}$ mode, external AC source, and a modulation level of exactly $82^{\circ}$ as read on the front panel meter.
[^8]
## ADJUSTMENTS

## 5-28B. PHASE MODULATION LEVEL AND DISTORTION ADJUSTMENTS - ALTERNATE PROCEDURE (Cont'd)

7. Adjust A16R2 so the carrier and first sidebands are of equal amplitude.
8. Step the System Under Test center frequency down 1 Hz to 99.999999 MHz . The carrier and first sidebands should be within 0.5 dB . If the difference is less than or equal to 0.5 dB , proceed to Step 11. If the difference is greater than 0.5 dB and if the $\phi \mathrm{M}$ deviation is $<82^{\circ}$ (first sideband is of lower amplitude than the carrier) proceed to Step 9 . If the $\phi \mathrm{M}$ deviation is $>82^{\circ}$ proceed to Step 10.
9. Adjust A16R4 one-eighth turn ccw. If A16R4 is in contact with the ccw stop, increase the value of A16R5. (The normal value range is 10 to 316 ohms.) Set the frequency of the System Under Test to 100 MHz and repeat Steps 7 and 8.
10. Adjust A16R4 one-eighth turn cw . If A16R4 is in contact with the cw stop, decrease the value of A16R5. (The normal value range is 10 to 316 ohms.) Set the frequency of the System Under Test to 100 MHz and repeat Steps 7 and 8.
11. Set the spectrum analyzer controls for a center frequency of 2 MHz , resolution bandwidth to 30 kHz , frequency span per division to 0.5 MHz input attenuation to $0 \mathrm{~dB}, \log$ reference level to a convenient level, vertical sensitivity per division to 10 dB , and scan time per division to 10 ms .
12. Set the System Under Test center frequency to 300 MHz with a modulation level of $100^{\circ}$ as read on the front panel meter.
13. Connect the phase modulation test set between the signal generator output and the spectrum analyzer input as shown in Figure 5-5B.
14. Adjust the spectrum analyzer's reference level so the peak of the fundamental 1 MHz signal is viewed on the CRT display at the log reference graticule line.
15. Adjust A16R3 to null the second harmonic level; adjust A16R1 to null the third harmonic level.
16. Step the System Under Test center frequency down 1 Hz . Note the direction and amount of readjustment of A16R3 and R1 necessary to null the second and third harmonics.
17. Set A16R3 and R1 for the best compromise (minimum second and third harmonic levels) at both center frequency settings of 299.999999 and 300 MHz .
18. Repeat steps 4 through 20 until all the conditions below are met without further adjustment.
a. Carrier and first sidebands are equal within 0.5 dB when changing Center Frequency of System Under Test between 100 and 99.999999 MHz (Steps 7-8).
b. Second harmonic levels are equal within 4 dB or $>40 \mathrm{~dB}$ down from the fundamental at center frequencies of 300 and 299.999999 MHz (Step 17).
c. Third harmonic levels are equal within 4 dB or $>35 \mathrm{~dB}$ down from the fundamental at center frequencies of 300 and 299.999999 MHz (Step 17).
19. Replace the mainframe cover and wait 10 minutes. Check to see if the conditions outlined in step 18 are still met. If not repeat steps 4 through 19.

# SECTION VI REPLACEABLE PARTS 

## 6-1. INTRODUCTION

6-2. This section contains information for ordering parts. Table 6-1 lists abbreviations used in the parts list and throughout the manual. Table 6-2 lists all replaceable parts in reference designation order. Table 6-3 contains the names and addresses that correspond with the manufacturers' code numbers.

## 6-3. EXCHANGE ASSEMBLIES

6-4. The A13 Attenuator Assembly may be replaced on an exchange basis, thus affording a considerable cost saving. Exchange, factory-repaired and tested assemblies are available only on a trade-in basis; therefore, the defective assemblies must be returned for credit. For this reason, assemblies required for spare parts stock must be ordered by the new assembly part number. The A13 assembly exchange part number is 86601-60109.

## 6-5. ABBREVIATIONS

6-6. Table 6-1 lists abbreviations used in the parts list, schematics and throughout the manual. In some cases, two forms of the abbreviation are used, one all in capital letters, and one partial or no capitals. This occurs because the abbreviations in the parts list are always all capitals. However, in the schematics and other parts of the manual, other abbreviation forms are used with both lower case and upper case letters.

## 6-7. REPLACEABLEPARTS LIST

6-8. Table 6-2 is the list of replaceable parts and is organized as follows:
a. Electrical assemblies and their components in alpha-numerical order by reference designation.
b. Chassis-mounted parts in alpha-numerical order by reference designation.
c. Miscellaneous parts.

The information given for each part consists of the following:
a. The Hewlett-Packard part number.
b. The total quantity (Qty) used in the instrument.
c. The description of the part.
d. A typical manufacturer of the part in a five-digit code.
e. The manufacturer's number for the part.

The total quantity for each part is given only at the first appearance of the part number in the list.

## 6-9. ORDERING INFORMATION

6-10. To order a part listed in the replaceable parts table, quote the Hewlett-Packard part number, indicate the quantity required, and address the order to the nearest Hewlett-Packard office.

6-11. To order a part that is not listed in the replaceable parts table, include the instrument model number, instrument serial number, the description and function of the part, and the number of parts required. Address the order to the nearest Hewlett-Packard office.

## 6-12. SPARE PARTS KIT

6-13. Stocking spare parts for an instrument is often done to ensure quick return to service after a malfunction occurs. Hewlett-Packard has a "Spare Parts Kit" available for this purpose. The kit consists of selected replaceable assemblies and components for this instrument. The contents of the kit and the "Recommended Spares" list are based on failure reports and repair data, and parts support for one year. A Recommended Spares list or the Spare Parts Kit (which contains the list) may be ordered through your nearest Hewlett-Packard office.

## 6-14. DIRECT MAIL ORDER SYSTEM

6-15. Within the USA, Hewlett-Packard can supply parts through a direct mail order system. Advantages of using the system are:
a. Direct ordering and shipment from the HP Parts Center in Mountain View, California.
b. No maximum or minimum on any mail order (there is a minimum order amount for parts ordered through a local HP office when the orders require billing and invoicing).
c. Prepaid transportation (there is a small handling charge for each order).
d. No invoices - to provide these advantages, a check or money order must accompany each order.

6-16. Mail order forms and specific ordering information is available through your local HP office. Addresses and phone numbers are located at the back of this manual.

Table 6-1. Reference Designations and Abbreviations (1 of 2)

| REFERENCE DESIGNATIONS |  |  |  |
| :---: | :---: | :---: | :---: |
| A . . . . . . . . . . . assembly <br> AT .. attenuator; isolator; termination | E . . . . . . . miscellaneous electrical part | P . . . electrical connector (movable portion); plug | U . . . . . integrated circuit; microcircuit |
| B . . . . . . . . . fan; motor | FL . . . . . . . . . . . filter | Q . . . . . transistor: SCR; | VR . . . . . . voltage regulator; |
| BT . . . . . . . . . battery | H . . . . . . . . . hardware | triode thyristor | breakdown diode |
| C . . . . . . . . . . capacitor | HY . . . . . . . circulator | R . . . . . . . . . . . resistor | W . . . cable: transmission |
| CP . . . . . . . . . . coupler | J . . . electrical connector | RT . . . . . . . ${ }^{\text {a }}$ thermistor | path; wire |
| CR . . . . . . diode; diode | (stationary portion); | S . . . . . . . . . . switch | X . . . . . . . . . . . socket |
| DC . . ${ }_{\text {thyristor; directional coupler }}$ | jack | T . . . . . . . . . transformer | Y . . . er erystal unit (piezo- |
| DL . . . . . . . . delay line | K . . . . . . . . . . . relay | TC . . . . . . . thermocouple | Z .... tuned cavity; tuned |
| DS . . . . . . annunciator; | L . . . . . . . coil; inductor | TP . . . . . . . test point | circuit |
| signaling device <br> (audible or visual); | MP . . . . . . . miscellaneous |  |  |
| lamp; LED | anical part |  |  |
| ABBREVIATIONS |  |  |  |
| A . . . . . . . . . . ampere | COEF . . . . . . . coefficient COM . . . . . . . . . common COMP . . . . . composition COMPL . . . . . . . complete CONN . . . . . . . connector CP . . . . . . cadmium plate CRT . . . cathode-ray tube CTL . . . . complementary transistor logic | EDP . . . . electronic data | INT . . . . . . . . . internal |
| ac.... alternating current |  | processing | kg . . . . . . . . . kilogram |
| ACCESS . . . . accessory |  | ELECT . . . . electrolytic | kHz . . . . . . . . kilohertz |
| ADJ . . . . . . adjustment |  | ENCAP . . . . encapsulated | k $\Omega$. . . . . . . . . kilohm |
| A/D . . . analog-to-digital |  | EXT . . . . . . . external | kV . . . . . . . . . . kilovolt |
| AF . . . . audio frequency |  | F . . . . . . . . . . . farad | lb . . . . . . . . . . pound |
| AFC . . . . . . . . automatic frequency control |  | FET . . . . . field-effect | LC . . . . . . . . inductancecapacitance |
| AGC . . . . automatic gain |  | F/F . . . . . . . flip-flop | LED . . light-emitting diode |
| control | transistor logic <br> CW . . . . . continuous wave | FH . . . . . . . . . flat head | LF . . . . . low frequency |
| AL . . . . . . . . aluminum | cw . . . . . . . . clockwise | FIL H . . . . fillister head | LG . . . . . . . . . . . long |
| ALC . . . . . automatic level control | cm . . . . . . . . centim | FM. . frequency modulation | LH . . . . . . . . . left hand |
|  | D/A . . . digital-to-analog | FP . . . . . . . front panel | LIM . . . . . . . . . . limit |
| AM . . . amplitude modulation | dB . . . . . . . . . . . decibel | FREQ . . . . . . frequency FXD . . . . . . . . . . . fixed | LIN . . . linear taper (used |
| AMPL . . . . . . . . amplifier APC . . . . automatic phase control | $\mathrm{dBm} \ldots .{ }^{\text {decibel referred }}$ | g . . . . . . . . . . . . $\quad$ gram | lin . . . . . . . . . . linear |
|  | dc . . . 1 mW direct current | GE . . . . . . . germanium | LK WASH . . . lock washer |
|  | dc $\ldots . . . . . . ~ d i r e c t ~ c u r r e n t ~$ deg . . degree (temperature | GHz . . . . . . . . gigahertz | LO . . . low; local oscillator |
| ASSY . . . . . . . AUX | interval or difference) | GL . . . . . . . . . . . glass | LOG . . . . logarithmic taper |
| AUX . . . . . . . . . auxiliary avg $\qquad$ average |  | GRD . . . . . . . ground (ed) H . . . . . . . . . . . . . henry | (used in parts list) <br> $\log . . . . . . .$. logrithm(ic) |
| avg . . . . . . . . . . . average AWG . . . . American wire gauge | $\bigcirc$ angle) | h . . . . . . . . . . . . hour | LPF . . . . low pass filter |
|  | C . . . . . degree Celsius | HET . . . . . . ${ }^{\text {Heterodyne }}$ | LV . . . . . . . low voltage |
|  | $\bigcirc_{K}^{F} \ldots .$. degree Fahrenheit | HD . . . . . . . . . . . . . head | ma . . . . . . . . . milliampere |
| BCD . . . . . . binary coded |  | HDW . . . . . . . hardware | MAX . . . . . maximum |
| BD . . . . . . . . . . . board |  | HF . . . . . high frequency | M ${ }^{\text {a }}$. . . . . . . megohm |
| BE CU $\underset{\substack{\text { copper }}}{\ldots . .}$ beryllium | DET . . . . . . . . . detector | HG . . . . . . . . . mercury | MEG . . . . meg ( $10^{6}$ ) (used |
| BFO . . . . beat frequency | DIA . . . diameter (used in parts list) | HP ..... Hewlett-Packard | MET FLM . . . metal film |
|  |  | HPF . . . . high pass filter | MET OX . . metallic oxide |
| BH . . . . . . . . binder head | DIFF AMPL . . differential | HR . . . . . . . hour (used in parts list) | MF . . . medium frequency; microfarad (used in |
| BP . . . . . . . . . . bandpass | div . . . . . . . . . division | HV . . . . . . . high voltage | parts list) |
| BPF . . . . bandpass filter | DPDT ${ }^{\text {double-throw }}$ double-pole, | Hz . . . . . . . . . . Hertz | MFR . . . . . manufacturer |
| BRS . . . . . . . . . . brass |  | IC . . . . integrated circuit | mg . . . . . . . milligram |
| BWO . . . . . backward-wave <br> oscillator | DR . . . . . . . . . . . . drive DSB . . . . double sideband | ID . . . . . inside diameter | MHz . . . . . . . megahertz |
|  |  | IF . . . . . intermediate | mH . . . . . . . millihenry |
|  | DSB . . . . double sideband <br> DTL . . . . diode transistor logic | frequency <br> IMPG $\qquad$ impregnated | mho . . . . . . . . . . . mho MIN . . . . . . . minimum |
|  |  | in $\qquad$ inch | min . . . . . . minute (time) |
|  | ECL . . . . emitter coupled <br> logic | INCD . . . . incandescent | . . ' . . . . . minute (plane |
|  |  | INCL . . . . . . include(s) | angle) |
|  | EMF . . electromotive force | INP . . . . . . . . input | MINAT . . . . . miniature |
|  |  | INS . . . . . . insulation | mm ....... millimeter |
| NOTE |  |  |  |
| All abbreviations in the parts list will be in upper-case. |  |  |  |

Table 6-1. Reference Designations and Abbreviations (2 of 2)

| MOD . . . . . . modulator |  |
| :---: | :---: |
| мом | momentary |
| MOS . . . . . . . . me |  |
| ms | millisecond |
| MTG . . . . . . . . mounting |  |
| MTR. | . . meter (indicating device) |
| device) |  |
| mVac . . . . . milliv |  |
| mVdc $\ldots . .$.mVpk |  |
|  |  |
| mVp-p . . . millivolt, peak- |  |
| mVrms . . . millivolt, rms |  |
| mW . . . . . . . . milliwatt |  |
| MUX ....... multiplex |  |
| MY . . . . . . . . . . . mylar |  |
| $\mu_{\text {A }}$. . . . . . microampere |  |
|  |  |
|  |  |
| $\mu_{\text {mho }}^{\mu \mathrm{H}} \ldots \ldots \ldots . \mathrm{m}^{\text {microhenry }}$ |  |
| $\mu \mathrm{s}$. |  |
| $\mu \mathrm{V}$. . . . . . . . microvolt |  |
| $\mu$ Vac . . . . . microvolt, ac |  |
| $\mu \mathrm{Vdc} . . . .{ }^{\text {c }}$ microvolt, dc |  |
| $\mu \mathrm{Vpk} . .$. microvolt, peak |  |
| $\mu \mathrm{Vp-p} \underset{\text { to-peak }}{\ldots}$ microvolt, peak- |  |
| $\mu \mathrm{Vrms}$ | microvolt, rms |
|  |  |
| nA . . . . . . . nanoampere |  |
| NC . . . . . n no connection |  |
| N/C . . . . normally closed |  |
| NE . . . . . . . . . . . neon |  |
| NEG . . . . . . . . negative |  |
| nF . . . . . . . . nanofarad |  |
| NI PL . . . . . . nickel plate |  |
| N/O . . . . . normally open |  |
| NOM . . . . . . . . nominal |  |
| NORM . . . . . . . normal |  |
| NPN . . . negative-positive- |  |
| NPO | negative-positive |
|  | zero (zero temperature coefficient) |
| NRFR | not recommended |
|  | for field replacement |
| NSR | . . . . not separately replaceable |
|  | ns . . . . . . . . nanosecond |
| nWOBD |  |
|  |  |
|  |  |


| D . . . . . outside diamete |  |
| :---: | :---: |
|  |  |
| OP AMPL . . . amplifier |  |
| OPT . . . . . . . . optio |  |
| OSC . . . . . . . . oscillator |  |
| OX . . . . . . . . . . . . oxide |  |
| oz . . . . . . . . . . . . ounce |  |
| P . . . . peak (used in parts list) |  |
|  |  |
| PAM . . . . pulse-amplitude modulation |  |
| PC . . . . . printed circuit |  |
| PCM . . pulse-code modulation; pulse-count modulation |  |
| PDM . . . . . pulse-duration modulation |  |
| PH BRZ phosphor bronze |  |
|  |  |
| PHL . . . . . . . . . Phillips |  |
| PIN . . . positive-intrinsicnegative |  |
| PIV . . . . . . peak inverse voltage |  |
| pk . . . . . . . . . . . . peak |  |
| PL . . . . . . . . . phase lock |  |
| PLO . . . . . . . phase lock |  |
|  |  |
| PM . . . . phase modulation |  |
| PNP . . . positive-negativepositive |  |
| P/O . . . . . . . . part of |  |
| POLY . . . . . polystyrene |  |
| PORC . . . . . . . porcelain |  |
| POS . . positive; position(s) <br> (used in parts list) |  |
|  |  |
| POSN . . . . . . position |  |
| POT . . . . . potentiometer |  |
| p-p . . . . . . . peak-to-peak |  |
| PP . . . peak-to-peak (used |  |
| in parts list) |  |
| PPM . . . . . pulse-position modulation |  |
|  |  |
| PREAMPL . . . preamplifier |  |
| PRF . . . pulse-repetition frequency |  |
|  |  |
| PRR . . . . pulse repetition rate |  |
|  |  |
| ps . . . . . . . . picosecond |  |
| PT . . . . . . . . . . . point |  |
| PTM . . . . . . . . pulse-time |  |
|  |  |
| M . . . . . . . pulse-width |  |
|  |  |


| PWV . . . . . . peak working voltage |  |
| :---: | :---: |
| RC . . . . . . . . resistancecapacitance |  |
| RECT | rester |
| EF | reference |
| REG | gulated |
| REPL | eplaceable |
| RF . . . . . radio frequency |  |
| RFI . . . . radi interfere |  |
| RH . . . h |  |
| RLC . . . . . . . $\begin{gathered}\text { resistance- } \\ \text { inductance- } \\ \text { capacitance }\end{gathered}$ |  |
| rms . . . . root-mean-square |  |
| RND . . . . . . . . . . round |  |
|  |  |
| R\&P . . . . . rack and panel |  |
| RWV $\underset{\text { voltage }}{\text { e. }}$ reverse working |  |
|  |  |
|  |  |
|  | econd (plane angle) |
| S-B . . . . slow-blow (fuse) |  |
|  |  |
| SCR . . . silicon controlle |  |
| SE | selen |
| SECT |  |
| SEMICO |  |
| SHF |  |
| SI | n |
| SIL |  |
| $\mathrm{SLR}_{\text {SL }} \ldots$. . . signal-to |  |
|  |  |
| SNR . . signal-to-noise ratio SPDT | . . . . . single-pole, double-throw |
| SPG | spring |
| SR . |  |
| SPST $\underset{\text { single-throw }}{\text { and }}$ |  |
| SSB . . . . . single sideband |  |
| SST . . . . . stainless stee |  |
| STL . . . . . . . . . . . steel |  |
| SQ | square |
| SQ . . . . . . . . ${ }_{\text {Standing-wave ratio }}$ |  |
| SYNC . . . . . synchronize |  |
| T . . timed (slow-blow fuse) |  |
| TA . . . . . . . . . tantalum |  |
| TC | . . . . . . temperature |


| D . . . . . . . . . time delay |  |
| :---: | :---: |
| TFT . . thin-film transistor |  |
| TGL . . . . . . . . . . . toggle |  |
| THD . . . . . . . . . thread |  |
| THRU . . . . . . . through |  |
| TI . . . . . . . . . titanium |  |
| TOL . . . . . . . . tolerance |  |
| TRIM . . . . . . trimmer |  |
| TSTR ....... transistor |  |
| TTL . . transistor-transistor logic |  |
|  |  |
| TV . . . . . . . . television |  |
| TVI television int |  |
| TWT . . traveling wave tube |  |
| $\mathrm{U} \ldots \ldots \operatorname{micro}\left(10^{-6}\right) \text { (used }$ |  |
| UF . . . microfarad (used in parts list) |  |
| HF . . ultrahigh frequency |  |
| UNREG . . . unregulated |  |
| V . . . . . . . . . . . . . . volt |  |
| VA .. . . . . . voltampere |  |
| Vac . . . . . . . . volts, ac |  |
| VAR . . . . . . . . . . variable |  |
| VCO . . . voltage-controlled oscillator |  |
| Vdc . . . . . . . . volts, dc |  |
| VDCW . . volts, dc, working <br> (used in parts list) |  |
| V(F) . . . . . . volts, filtered |  |
| $\text { VFO .. } \begin{gathered} \text { variable-frequency } \\ \text { oscillator } \end{gathered}$ |  |
| VHF . . . . . very-high frequency |  |
| Vpk . . . . . . . . volts, peak |  |
| Vp-p . . volts, peak-to-peak |  |
| Vrms . . . . . . volts, rms |  |
| VSWR . . . voltage standing wave ratio |  |
|  |  |
| VTO . . . . . . voltage-tuned oscillator |  |
| VTVM . . . . vacuum-tube voltmeter |  |
| V(X) . . . . . volts, switched |  |
| W . . . . . . . . . . . . . . watt |  |
| W/ . . . . . . . . . . . . with |  |
| WIV . . . . working inverse voltage |  |
|  |  |
| WW . . . . . . wirewound |  |
| W/O . . . . . . . . without |  |
| YIG . . yttrium-iron-garnet |  |
| $Z_{0}$. . . . . . characteristic |  |
|  |  |

Vdc . . . . . . . . . volts, dc VDCW . . volts, dc, working (used in parts list)

VFO . . variable-frequency oscillator
quency
Vpk . . . .... . volts, peak
Vp-p . . volts, peak-to-peak
Vrms . . . . . . . volts, rms
VSWR . . . voltage standing oscillator

V(X) . .... voltmeter

WIV . . . . working inverse impedance

NOTE
All abbreviations in the parts list will be in upper-case.

## MULTIPLIERS

| Abbreviation | Prefix | Multiple |
| :---: | :--- | :---: |
| T | tera | $10^{12}$ |
| G | giga | $10^{9}$ |
| M | mega | $10^{6}$ |
| k | kilo | $10^{3}$ |
| da | deka | 10 |
| d | deci | $10^{-1}$ |
| c | centi | $10^{-2}$ |
| m | milli | $10^{-3}$ |
| $\mu$ | micro | $10^{-6}$ |
| n | nano | $10^{-9}$ |
| p | pico | $10^{-12}$ |
| f | femto | $10^{-15}$ |
| a | atto | $10^{-18}$ |

Table 6-2. Replaceable Parts

| Reference <br> Designation | HP Part Number | Oty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: |
| A 1 | 86602-60002 | 1 | MOUULATOR FILTER ASSY | 28480 | 86602-60002 |
| AlCl | 0160-3874 | 1 | CAPACITOR-FXD 10 PF +-. 5PF 200WVDC CER | 28480 | 0160-3874 |
| A1J1 | 0360-1514 |  | TERMINAL-STUC SGL-PIN PRESSOMTG | 28480 | 0360-1514 |
| AlJ 2 | 0360-1514 |  | TERMINAL-STUD SGL-PIN PRESS-MTG | 28480 | n360-1514 |
| All 1 | 9140-0158 | 2 | CGIL-FXD MOLDED RF ChOKE IUH 10\% | 24226 | 10/101 |
| All 2 | 9140-0158 |  | COIL $\triangle$ FXD MOLDEO RF CHOKE IUH 10\% | 24226 | 10/101 |
| A1L 3 | 9100-2247 | 1 | COIL-FXD MOLDEO RF CHOKE . IUH 10\% | 24226 | 10/100 |
| A1P1 | 1251-3172 | 5 |  | 00779 00779 | $2=331677-9$ $2-331677-9$ |
| AlP 2 A1P3 | $1251-3172$ $1251-3172$ |  | CONNECTOR;1-CONT SKT 03 DIA CONNECTOR;1-CONT SKT 03 OIA | 00779 | $2-331677-9$ $2-331677-9$ |
| A1P4 | $1251-3172$ |  | CONNECTOR;1-CONT SKT . 03 DIA | 00779 | 2-331677-9 |
| A1P 5 | 1251-3172 |  | CONNECTOR;1-CONT SKT . 03 DIA | 00779 | 2-331677-9 |
| A2 | 86603-60001 | 1 | ALC MOTHER BCARD ASSY | 28480 | 86603-60001 |
| A2C1 | 0160-2204 | 2 | CAPACITOR-FXD 100PF +-5\% 300WVDC MICA | 28480 | 0160-2204 |
| A2C 2 | 0160-3457 | 1 | CAPACITOR-FXO 2000PF +-108 250 WVDC CER | 28480 | 0160-3457 |
| A2J1 | 1250-1255 | 1 | CCNNECTOR-RF SMB M PC | 98291 | 51-051-0000 |
| A 2 K 1 | 0490-0916 | 3 | RELAY-REED 1A .5A 50V CONT 5V-COIL | 28480 | 0490-0916 |
| A 201 | 1854-0404 | 5 | TRANSISTOR NPN SI TO-18 PD=360MW | 28480 | 1854-0404 |
| A2R 1 | 0698-0084 | 1 | RESISTOR 2.15K 1\% -125W F TC=0+100 | 16299 | C4-1/8-T0-2151-F |
| A2R 2 $A 2 R 3$ | $0757-1060$ $0757-0441$ | 1 | RESISTOR $1961 \% .5 \mathrm{~W}$ F TC $=0+\infty 100$ RESISTOR $8.25 \mathrm{~K} \quad 18.125 \mathrm{WF} \mathrm{TC}=0+100$ | 19701 24546 | MF $7 C 1 / 2-T 0=196 R-F$ $C 4=1 / 8-T 0=8251-F$ |
| A2R 3 A2R | -0757-0441 | 1 |  | 24546 19701 | $C 4=1 / 8-T 0=8251-F$ MFTC $1 / 20 T 0=422 R \circ F$ |
| A2R 4 A2R 5 | 0698-3405 $0757-0438$ | 11 |  | 19701 24546 | MF7C1/2-T0-422ROF C4-1/8-T0 -51110 F |
| A2R 6 | 0757-0438 |  | RESISTOR 5.11K 1\% .125W F TC=0* 100 | 24546 | C4-1/8-T0-5111-F |
| A2R 7 | 0757-0401 | 1 | RESISTOR $1001 \% .125 \mathrm{~W}$ F TC $=0+100$ | 24546 | C4-1/8- T0-101-F |
| A2R 8 | 0698-3403 | 1 | RESI STOR $3481 \% .5 \mathrm{~W}$ F TC $=0+-100$ | 24546 | NA 6 |
| A2R9 | 0757-0276 | 1 | RESISTOR 61.9 12.125W F TC $=0+=100$ | 24546 | C4-1/8- T0-6192-F |
| A 2VR1 | 1902-3139 | 1 | DIODE - ZNR 8.25V 5\% DO-7 PD=.4W TC= + .053\% | 04713 | SZ 10939-158 |
| A2xA3 | 1251-1626 | 3 | CONNECTOR-PC EDGE 12-CONT/ROW 2-ROWS | 71785 | 252-12-30-300 |
| A2×A4 | 1251-1626 |  | CONNECTOR-PC EDGE 12-CONT/ROW 2-ROWS | 71785 | 252-12-30-300 |
| A $2 \times 416$ | 1251-1626 |  | CONNECTOR-PC EDGE 12-CONT/ROW 2-ROWS <br> A2 MISCELLANEOUS | 71785 | 252-12-30-300 |
|  | 0360-1514 | 6 | TERMINAL-STUD SGL-PIN PRESS-MTG | 28480 | 0360-1514 |
| A3 | 86602-60001 | 1 | ALC AMPLIFIER ASSY | 28480 | 86602-60001 |
| A3C1 | 0180-0058 | 2 | CAPACITOR-FXO 50UF+75-10\% 25VDC AL | 56289 | 300506G 5255 C 2 |
| A 3 C 2 | $0180-0058$ |  | CAPACITOR-FXD 50UF +75010\% 25VOC AL | 56289 | 300506G6025CC2 |
| A 3C 3 | 0160-2199 | 2 | CAPACITOR-FXD 30PF $+\infty 5 \%$ 300WVDC MICA | 28480 | 0160-2199 |
| A 3C4 | 0160-2199 |  | CAPACITOR-FXD 30PF +-5\% 300HVDC MICA | 28480 | 0160-2199 |
| A 3C5 | 0160-0302 | 1 | CAPACITOR FFXD .018UF $+=10 \%$ 200WVDC POLYE | 56289 | 292P18392 |
| A 3 C 6 $A 3 C 7$ | 0160-3468 $0160-2204$ | 1 | CAPACITOR=FXC . $12 U F+10 \%$ 8OWVOC POLYE CAPACITOR $-F X C$ 100PF $+55 \%$ 300WVDC MICA | $\begin{aligned} & 56289 \\ & 28480 \end{aligned}$ | $\begin{aligned} & 292 P 1249 R 8 \\ & 0160-2204 \end{aligned}$ |
| A3CR1 | 1901-0047 | 3 | DIDDE-SHITCHING 20V 75MA LONS | 28480 | 1901-0047 |
| A 3CR2 | 1901-0047 |  | DIDOE-SHITCHING 20V 75MA 10NS | 28480 | 1901-0047 |
| A 3CR3 | 1901-0047 |  | DIODE-SWITCHING 20V 75MA 10NS | 28480 | 1901-0047 |
| A 3CR4 | 1901-0050 | 2 | DIDDE-SWITCHING 80V 200NA 2NS DO-7 | 28480 | 1901-0050 |
| 43K1 | 0490-0916 |  | RFLAY-REED 1A .5A 50V CONT 5V-COIL | 28480 | 0490-0916 |
| A3L 1 | 9140-0237 | 4 | COIL-FXC MOLDED RF CHOKE 200UH 5\% | 24226 | 15/203 |
| A3L2 | 9140-0237 |  | COIL-FXD MOLDED RF CHOKE 200UH 5\% | 24226 | 15/203 |
| A3L 3 | 9140-0105 | 1 | COIL-FXD MOLDED RF CHOKE 8.2UH 10\% | 24226 | 15/821 |
| A 301 A 302 A | $1853-0020$ $1854-0404$ | 3 | TRANSISTOR PNP SI PD=300MW FT=150MHZ TRANSISTOR NPN SI TO-18 PD=360MH | 28480 28480 | $1853-0020$ $1854-0404$ |
| A 303 | 185E-0020 | 1 | TRANSISTOR J-FET N-CHAN D-MODE TO-18 SI | 28480 | 1855-0020 |
| A 304 | 1853-0034 | 5 | TRANSISTOR PNP SI TO-18 PD=360MW | 28480 | 1853-0034 |
| A305 | 1853-0020 |  | TRANSISTOR PNP SI PD $=300 \mathrm{MW}$ FT $=150 \mathrm{MHZ}$ | 28480 | 1853-0020 |
| A306 | 1853-0034 |  | TRANSISTOR PNP SI TO-18 PO=360MW | 28480 | 1853-0034 |
| A 307 | 18540404 |  | TRANSISTOR NPN SI TO-18 PD=360MH | 28480 | 1854-0404 |
| A 308 | 1854-0404 |  | TRANSISTCR NPN SI TO-18 PD=360MW | 28480 | 1854-0474 |
| A309 | 1853-0034 |  | TRANSISTOR PNP SI TO-18 PD=360MW | 28480 | 1853-0034 |
| A30iv | 1854-0221 | 2 | TRANSISTOR-DUAL NPN PD $=750 \mathrm{MH}$ | 28480 | 1854-0221 |
| A 3011 | 1854-0053 | 1 | TRANSISTOR NPN 2 N 2218 SI TO-5 PD $=800 \mathrm{MH}$ | 04713 | 2N2218 |

Table 6-2. Replaceable Parts


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| Reference Designation | HP Part Number | Qty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { A4R16 } \\ & \text { A4R17* } \end{aligned}$ | $\begin{aligned} & 0698-0083 \\ & 0698-3442 \end{aligned}$ | 1 | RESISTOR 1.96 K 1\% . 125 W F TC $=0+100$ RESISTOR 237 18 . 125 W F TC=0+= 100 *FACTCRY SELECTED PAFT | 16299 16299 | $\begin{aligned} & C 4-1 / 8-T O-1961-F \\ & C 4-1 / 8=T 0-237 R=F \end{aligned}$ |
| A4R18 | 0757-0280 |  |  | 24546 16299 | C4-1/8-T0-1 001-F $\mathrm{C} 4=1 / 8-\mathrm{T} 0-422 \mathrm{~F}-\mathrm{F}$ |
| A4R19 | 0698-3447 | 2 | RESISTOR 422 18 . 125 W F TC $=0+100$ | 16299 | $C 4-1 / 8-T 0-422 R=F$ |
| A4R 20 A 4 R 21 | $0698-0082$ $0698-3447$ | 2 | RESISTOR 464 RESISTOR RES | 15299 16299 | $\begin{aligned} & C 4=1 / 8-T O-4640-F \\ & C 4=1 / 8=T O=422 R=F \end{aligned}$ |
| A4R 22 | 0698-3157 | 1 | RESISTOR 19.6K 1\% -125W F TC $=0+100$ | 16299 | C $4=1 / 8=$ T0-19620F |
| A4R 23 | 0698-3455 | 1 | RESISTOR $261 \mathrm{~K} 1 \% .125 \mathrm{~W}$ F TC $=0+=100$ | 16299 | C $4-1 / 8=T 0-2613-F$ |
| A4R 24 | 0757-0439 | 1 | RESISTOR 6.81K 1\% . 125 W F TC=0 +100 | 24546 | $\mathrm{C} 4=1 / 8=\mathrm{T} 0=6811-\mathrm{F}$ |
| $\begin{aligned} & A 4 R 25 \\ & \text { A4R } 26 \end{aligned}$ | $\begin{aligned} & 0698-0082 \\ & 2100-2489 \end{aligned}$ | 1 | RESISTOR 464 1\% . 125 W F TC= $0+100$ RESISTOR=TRMR 5K 10\% C SIDE~ADJ 1:TURN | 16299 19701 | $\begin{aligned} & \mathrm{C} 4=1 / 8=T 0=4640=\mathrm{F} \\ & \text { ET5 } 0 \times 502 \end{aligned}$ |
| A4S 1 | $3101=0973$ | 1 | SWITCH-SL DPCT-NS MINTR . 5A 125VAC/DC PC | 79727 | GF126-0018 |
| A4TP1 A4TP2 | $0360-1514$ $0360-1514$ |  | TERMINAL-STUD SGL-PIN PRESS-MTG TERMINAL-STUD SGL-PIN PRESS-MTG | 28480 29480 | $\begin{aligned} & 1360-1514 \\ & 0360=1514 \end{aligned}$ |
| A4U1 | 1826-0013 | 1 | IC OP AMP | 28480 | 1826-0013 |
|  |  |  | a4 Miscellaneous |  |  |
|  | $\begin{aligned} & 4040=0748 \\ & 1480-0073 \\ & 4040=0751 \\ & 1480-0073 \end{aligned}$ | 4 | ```EXTRACTOR=PC BO BLK POLYC .062-80=THKNS PIN:DRIVE 0.250" LG EXTRACTOR=PC BD ORN POLYC .062=BD=THKNS PIN:DRIVE 0.250" LG``` | 28480 00006 28480 00000 | $\begin{aligned} & 4040=0748 \\ & 080 \\ & 4040=0751 \\ & 08 D \end{aligned}$ |
| A5 | 5086-7049 | 1 | MIDULATCR ASSY | 28480 | 5086-7049 |
| A 5 J 1 |  |  | NSR |  |  |
| A 5J 2 |  |  | NSR |  |  |
| A 5J3 A 5 J |  |  | NSR NSR |  |  |
| A5J5 |  |  | NSR |  |  |
| A5J 6 |  |  | NSR |  |  |
| A6 | 5086-7048 | 1 | AMPLIFIER DETECTOR ASSEMBLY | 28480 | 5086-7048 |
| A6J1 |  |  | NSR |  |  |
| A6J 2 A6J 3 |  |  |  |  |  |
| A6J 4 |  |  | NSR |  |  |
| A 655 |  |  | NSR |  |  |
| A6J 6 |  |  | NSR |  |  |
| A7 | 86602-60044 | 1 | MIXER ASSY (EXCEPT OPTION 002) | 28480 | 86602-60044 |
| A7J1 | 86602-20022 | 3 | CONNECTOR, BULKHEAD | 28480 | 86602-20022 |
| A7J 3 | 86602-20022 |  | CONNECTOR, BULKHEAD CONNECTOR, BULKHEAD | 28480 28430 | $86602-20022$ $86602-20022$ |
|  |  |  | a7 Miscellaneous |  |  |
|  | 0360-0124 | 3 1 | TERMINAL-STUC SGL-PIN PRESS-MTG COVER, FILTER | 28480 28480 | $\begin{aligned} & 0360=0124 \\ & 5001-0002 \end{aligned}$ |
|  | 86602-00003 | 1 | COVER, MIXER, SMALL | 28480 | 86602-00003 |
|  | 86602-20026 | 1 | BUSHING SUPPRESSOR | 28480 28480 | $\begin{aligned} & 86602-20026 \\ & 866 \cap 2-20029 \end{aligned}$ |
|  | 86602-20029 | 1 | SUPPRESSOR | 28480 | $866 \cap 2-20029$ |
|  | $\begin{aligned} & 86603-00005 \\ & 86603-20024 \end{aligned}$ | 1 | COVER, MIXER, LARGE HOUSING, MIXER | $\begin{aligned} & 28480 \\ & 28480 \end{aligned}$ | $\begin{aligned} & 86603-00005 \\ & 86603-20024 \end{aligned}$ |
| A7A1 | 86602-20009 | 1 | balidn mixer assy | 28480 | 86602-20009 |
| A7A2 | 86602-60008 | 1 | BALANCE MIXER ASSY | 28480 | 86602-60008 |
| A7A2CR1 | 5080-0271 | 1 | DİDDE, SILICON, MATCHED QUAD | 28480 | 5080-0271 |
| A7A 3 | 5086 7066 | 1 | LOW PASS FILTER ASSY,1.45GHZ | 28480 | 5086-7066 |
| A7A4 | 86603-20023 | 1 | TRANSITION ASSY | 28480 | 86603-20023 |
| A7A 5 | 86602-20044 | 1 | TRANSITION ASSY | 28480 | 86602-20044 |

Table 6-2. Replaceable Parts

| Reference <br> Designation | HP Part Number | Oty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: |
| A7 | 86603-60023 | 1 | MIXER ASSY (CPTION OO2 ONLY) | 28480 | 86603-60323 |
| A7 C1 | 0160-4082 | 1 | CAPACITOROFXD 1000PF +-20\% 200WVDC CER | 28480 | 0160-4082 |
| $\begin{array}{ll}\text { A7 } & \mathrm{J1} \\ \text { A7 } & \mathrm{J2}\end{array}$ | $86602-20022$ $86602-20022$ | 3 | CONNECTOR, BULKHEAC CONNECTOR, BULKHEAD | 28480 28480 | $\begin{aligned} & 86602-20022 \\ & 86602-20022 \end{aligned}$ |
| A7 ${ }^{\text {J3 }}$ | 86602-20022 |  | CONNECTOR, BULKHEAD | 28480 | 86602-20022 |
| A7 L1 | 9100-1666 | 1 | COIL-FXD MCLDED RF CHOKE 3.6MH 5\% | 24226 | 22/364 |
|  | 0340-0044 | 1 | A7 MISCELLANEOUS TERMINAL-STUD DBL-TUR PRESS MTG | 83330 | 92-1500 |
|  | 0360-0124 | 1 | TERMINAL-STUD SGL-PIN PRESS-MTG | 28480 | C360-0124 |
|  | 5001-0002 | 1 | COVER, FILTER | 28480 | 5001-0002 |
|  | 86602-00003 | 1 | COVER, MIXER, SMALL | 28480 | 86602-00003 |
|  | 86602-20026 | 1 | BUSHING | 28480 | 86602-20026 |
|  | 86602-20029 | 1 | SUPPRESSOR | 28480 | 86602-20029 |
|  | $\begin{aligned} & 86603-00005 \\ & 86603-20024 \end{aligned}$ | 1 | COVER, MIXER, LARGE HOUSING, MIXER | 28480 28480 | $\begin{aligned} & 86603-00005 \\ & 86663-20024 \end{aligned}$ |
| A7A1 | 86602-20009 | 1 | BALUN MIXER ASSY | 28480 | 86502-20009 |
| A7A3 ${ }^{\text {a }}$ | 5086-7066 | 1 | LOW PASS FILTER ASSY,1.45GHZ | 28480 | 5086-7066 |
| A 744 | 86603-20023 | 1 | TRANSITION ASSY | 28480 | 86603-20023 |
| A7A 5 | 86603-60010 | 1 | LOW PASS FILTER AS SY, 50 MHZ (OPT 002 ONLY) | 28480 | 86603-60010 |
| A7A5 C1 | 0160-4303 | 2 | CAPACITOR-FXD .027UF +-10\% 50WVDC CER | 26654 28480 | $3 B \times 050 S 273 K$ |
| A7A5 C2 A7A5 ${ }^{\text {C3 }}$ | $0160-4305$ $0160-4308$ | 2 |  | 28480 26654 | $0160-4305$ 28N100S 330 K |
| A7A5 C4 | $0160-4247$ |  | CAPACI TOR $=$ FXD . $047 \mathrm{UF}+-10 \%$ 100WVDC CER | 28480 | 0160-4247 |
| A7A5 C5 | 0160-4303 |  | CAPACITCR=FXD . $027 \mathrm{UF}+-108$ 50WVDC CER | 26654 | 38×050S273K |
| A7A5 Cb | 0160-4305 | 1 | CAPACITOR=FXD 47 PF +-10\% 100WVDC CER | 28480 | 0160-4305 |
| A7A5 CR1 | 1901-0639 | 2 | DICDE-PIN 110 O | 28480 28480 | $\begin{aligned} & 1901-0639 \\ & 1901-0639 \end{aligned}$ |
| A7A5 CR2 | 1901-0639 |  | DICDEPPIN 110 V |  |  |
| A7A5 L1 | 86603-80001 | 2 | INDUCTGR, TCROID | 28480 23480 | 86603-80001 $86603-80001$ |
| A7A5 L2 | 86603-80001 |  | INOUCTOR, TOROID | 28480 | 86603-80001 |
| ATAS R1 | 0698-7222 | 2 | RESISTOR 261 2\% . 05 WH F TC=0+-100 | 24546 | C 3-1/8-TO-261R-G |
| A7A5 R2 | 0698-7222 |  | RESISTCR 26128.05 W F TC=0+100 | 24546 | C3-1/8-T0-261R-G |
| A7A5 R3 | 0698-7229 | 1 | RESISTOR 511 2\% .05W F TC=0+100 | 24546 | C3-1/8-T0-511R-G |
| AB | 86603-67003 | 1 | 4 GHZ AMPLIFIER ASSY(EXCEPT OPTION 0021 | 28480 | 86603-67003 |
| A8 | 86603-67001 | 1 | 4 GHZ AMPLIFIER ASSY(OPTION OD2 ONLY) | 28480 | 86603-67:01 |
| $\begin{aligned} & A B J 1 \\ & \text { A8J } 2 \end{aligned}$ |  |  | $\begin{aligned} & \text { NSR } \\ & \text { NSR } \end{aligned}$ |  |  |
| A9 | 86602-60040 | 1 | ATTENUATOR DRIVER ASSY (EXCEPT CPTION OOI) | 28480 | 86602-60040 |
| A9CR1 | 1901-0025 | 8 | DIODE-GEN PRP 100V 200NA DO-7 | 28480 | 1901-0025 |
| A9CR2 | 1901-0025 |  | DIODE-GEN PRP 100V 200NA DO-7 | 28480 | 1901-0025 |
| A9CR3 | 1901 -0025 |  | OIDDE®GEN PRP 100V 200NA DD-7 | 28480 | 1901-0025 |
| A9CR4 | 1901-0025 |  | DIODE-GEN PRP 100V 200NA DO-7 | 28480 28480 | $1901-0025$ $1901=0025$ |
| A9CR5 | 1901-0025 |  | DIODE-GEN PRP LOOV 200NA DO-7 | 28480 | 1901-0025 |
| A9CR6 | 1901-0025 |  | CIODE-GEN PRP 100V 200NA D0-7 | 28480 | 1901-0025 |
| A9CR7 | 1901-0025 |  | DIDDE-GEN PRP 100V 200NA DO-7 | 28480 | 1901-0025 |
| A9CR8 | 1901-0025 |  | OTODEGGEN PRP 100V 200NA DO-7 | 28480 | 1901-0025 |
| A 901 | 1853-0213 | 4 | TRANSISTOR PNP 2N4 236 SI TO-5 PD=1W | 04713 | 2N4236 |
| A902 | 1854-0361 | 4 | TRANSISTCR NPN $2 N 4239$ SI TO-5 PD=800MW | 04713 | 2N4239 |
| A903 | 1853-0020 | 17 | TRANSISTOR PNP SI PD $=300 \mathrm{MH} \quad \mathrm{FT}=150 \mathrm{MHZ}$ | 28480 | 1853-0020 |
| A904 | 1854-0071 | 4 | TRANSISTOR NPN SI PD $=360 \mathrm{MH} \quad \mathrm{FT}=2 \mathrm{COSMHZ}$ | 28480 | 1854-0071 |
| A905 | 1854-0404 | 5 | TRANSISTCR NPN SI TO-18 PD=360MH | 28480 | 1854-0404 |
| A 906 | 1853-0020 |  | TRANSISTOR PNP SI PD $=300 \mathrm{MW} \quad \mathrm{FT}=15 \mathrm{CMHZ}$ | 28480 | 1853-0020 |
| A907 | 1853-C213 |  | TRANSISTOR PNP 2 N4 236 SI TO-5 PD $=1 \mathrm{H}$ | 04713 | 2N4236 |
| 4908 | 1854-0361 |  | TRANSISTCR NPN 2 N4 239 SI TO-5 PD=800MW | 04713 | 2N4239 |
| A 909 | 1853-0020 |  | $\begin{array}{ll}\text { TRANSISTOR PNP SI } \\ \text { TRANSISTOR } & \text { PPN SI } \\ \text { ST }\end{array}$ | 28480 | $1853-0020$ 1854 |
| A9010 | 1854-0071 |  | TRANSISTOR NPN SI PD $=300 \mathrm{MW} \quad \mathrm{FT}=200 \mathrm{MHZ}$ | 28480 | 1854-0071 |
| A9011 A 9012 | 1854-0404 |  |  | 28480 28480 | 1854-0404 |
| A 9812 A 9013 | 1853-0213 |  | TRANSISTOR PNP SI PO=300MW FT $=150 \mathrm{MHZ}$ TRANSISTOR PNP 2 NH 236 SI TO-5 PD=1W | 04713 | 2N4236 |
| A9014 | $1854-0361$ |  | TRANSISTCR NPN 2 N4 239 SI TO-5 PD $=800 \mathrm{MW}$ | 04713 | 2N4239 |
| A9815 | 1853-0020 |  | TRANSISTOR PNP SI PD=300MH FT $=150 \mathrm{MHZ}$ | 28480 | 1853-0020 |

Table 6-2. Replaceable Parts

| Reference Designation | HP Part Number | Oty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: |
| A 9016 | 18540071 |  | TRANSISTCR NPN SI PD=300MW FT=200MHZ | 28480 | 1854-0071 |
| A9017 | 185400404 |  | TRANSISTOR NPN SI TO-18 PD $=360 \mathrm{MW}$ | 28480 | 1854-0404 |
| A9018 | 1853-0020 |  | TRANSISTOR PNP SI PD $=300 \mathrm{MW}$ FT $=150 \mathrm{MHZ}$ | 28480 | 1853-0020 |
| A9019 | 1853-0213 |  | TRANSISTOR PNP 2N4 236 S1 T0-5 PO=1W | 04713 | 2 N 4236 |
| A 9020 | 1854-0361 |  | TRANSISTCR NPN 2N4239 SI TO=5 PD=800Mn | 04713 | 2N4239 |
| A9021 | 1853-0020 |  | TRANS ISTOR PNP SI PD=300MW FT= 150 MHZ | 28480 | 1853-0020 |
| A9022 | 1854-0071 |  | TRANSISTOR NPN SI PD=300MW FT $=200 \mathrm{MHZ}$ | 28480 | 1854-0071 |
| A9023 | $1854-0404$ |  | TRANSISTOR NPN SI TO-18 PD= 360MW | 28480 28480 | $1854-0404$ $1853-0020$ |
| A 9024 | 1853-0020 |  | TRANSISTOR PNP SI PD $=300 \mathrm{MW}$ FT $=150 \mathrm{MHZ}$ | 28480 | 1853-0029 |
| A9R 1 | 0757-0280 | 11 | RESISTOR 1K 1\% . 125 W F TC=0 $=0100$ | 24546 | C4-1/8-T0-1001-F |
| A9R2 | 0757-0159 | 8 | RESISTOR 1K 18.5 W F TC=0 +0100 | 19701 | MF 7C1/2-T0-1RO-F |
| A9R3 | 0757-0159 |  | RESISTOR 1K 18, .5W F TC $=0+=100$ | 19701 | MF7C1/2-T0-1R0-F |
| A9R4 | 0698-3440 | 4 | RESISTOR 19618 -125w F TC $=0+0100$ | 16299 | C4-1/8-T0-196R-F |
| A9R 5 | 0683-0335 | 6 | RESISTCR 3.3 5\% . 25 W FC $T C=-400 /+500$ | 01121 | CB3365 |
| A9R6 | $0683-0335$ |  | RESISTOR 3.3 5\% .25W FC TC $=0400 /+500$ | 01121 | CB33G5 |
| A9R 7 | 0757-0401 | 8 | RESISTOR 10018.125 W F TC=0+ 100 | 24546 | C4-1/8-T0-101-F |
| A9R8 | 0757-0401 |  | RESISTOR 10018.125 W F TC $=0+\cdots 100$ | 24546 | C4-1/8-TJ-101-F |
| A9R9 | 0698-4002 | 8 | RESISTOR 5 K 18. 125 W F TC=0+ 100 | 16299 | C4-1/8-T0-5001=F |
| A9R 10 | 0698-4002 |  | RESISTOR 5K 18.125 F TC $=0+\cdots 100$ | 16299 | C4-1/8-70-5001=F |
| A9R 11 | 0757-0280 |  | RESISTOR 1K 18.125 W F TC= $0+0100$ | 24546 | C4-1/8= ${ }^{\text {c }}$ - $1001=F$ |
| A9R 12 | 0757-0159 |  | RESISTOR 1 K 18.5 W F TC=0+-100 | 19701 | MF7C $1 / 2=T 0-1 R 0-F$ |
| A9R13 | 0757-0159 |  | RESISTOR 1K 1\%.5W F TC $=0+=100$ | 19701 | MF7C1/2-T0-1R0-F |
| A9R14 | 0698-3440 |  | RESISTOR 19618.125 W F TC $=0+\rightarrow 100$ | 16299 |  |
| A9R15 | 0683-0335 |  | RESISTOR 3.3 5\% . 25 W FC TC $=\mathbf{= 4 0 0 / + 5 0 0}$ | 01121 | CB3365 |
| A9R 16 | 0683-0335 |  | RESISTOR 3.3 5\% . 25 W FC TC $=\mathbf{- 4 0 0 1 + 5 0 0}$ | 01121 | CB3365 |
| A9R17 | 0757-0401 |  | RESISTRR 10018.125 W F TC $=0+100$ | 24546 | C4-1/8-T0 $=101-\mathrm{F}$ |
| A9R18 | 0757-0401 |  | RESISTRR 100 18 \% 125 W F TC $=0+100$ | 24546 | C4-1/8=T0-101-F |
| A 9R19 | $0698-4002$ $0698-4002$ |  |  | 16299 16299 | $C 4=1 / 8-T 0=5001-F$ $C 4-1 / 8=T 0=5001=F$ |
| A9R 20 | 0698-4002 |  | RESISTOR 5K 1\% . 125 W F TC $=0+0100$ | 16299 | C4-1/8-T0-5001*F |
| A9R 21 | 0757-0280 |  | RESISTOR 1K 1\%. 125 W F TC=0+> 100 | 24546 | C4-1/8= T0 $=1001 \bigcirc F$ |
| A9R22 | 0757-0159 |  | RESISTOR 1K 1\% .5W F TC $=0+=100$ | 19701 | MF7C1/2-T0-1ROF |
| A9R23 | 0757-0159 |  | RESISTOR 1 K 18.5 W F TC $=0+=100$ | 19701 | MF7C $1 / 2-T 0 \rightarrow 1 \mathrm{P}=\mathrm{F}$ |
| A9R24 A9R 25 | -6698-3440 |  | $\begin{array}{llll}\text { RESISTOR } & 196 & 18 \\ \text { RESISTOR } & 3.3 & 5 \% & .125 \mathrm{~W} \\ \text { F }\end{array}$ | 16299 01121 | C4-1/8-T0-196R $-F$ C33 |
| 49 R 25 | 0683-0335 |  | RESISTOR 3.3 5\% .25W FC TC $=0 \times 400 /+500$ | 01121 | CB3365 |
| A9R26 | 06830335 |  | PESISTOR 3.3 5\% . 25 WW FC TC $=-400 /+500$ | 01121 | CB33G5 |
| A9R 27 | 0757-0401 |  | RESISTOR 100 1\% .125W F TC $=0+100$ | 24546 | C4-1/8- $\mathrm{TO}^{\text {c }}=101-\mathrm{F}$ |
| A9R 28 | 0757-0401 |  | RESISTOR 100 1\% . 125 W F TC $=0+100$ | 24546 | C4* 1/8-TJ $-101-F$ |
| A9R 29 | 0698-4002 |  | RESISTOR 5K 1\% - 125 W F TC $=0+-100$ | 16299 |  |
| A9R 30 | 0698-4002 |  | RESISTOR 5K 1\% . 125 W F TC=0+ 100 | 16299 | C4-1/8-TJ $50001=F$ |
| A9R 31 | 0757-0280 |  | RESISTCR 1K 1\% -125W F TC= $=0+100$ | 24.546 | C4-1/8-50-1001=F |
| 49 R 32 | 0757-0159 |  | RESISTOR 1K 1\%.5W F TC=0+=100 | 19701 | MF7C1/2-T0-1P0-F |
| A9R 33 | 0757-0159 |  | RESISTOR 1K 1\%.5W F TC=0+-100 | 19701 | MF7C1/2-T0-1R0-F |
| A9R34 | 0698-3440 |  | RESISTAR 196 1\% .125W F TC=0tol00 | 16299 | C $4-1 / 8=T 0-196 R=F$ |
| A9R 35 | 0811-2815 | 2 | RESISTCR 1.5 5\% .75W PW TC $=0+50$ | 91637 | FS1/2-T2-1R5-J |
| A9R 36 | 0811-2815 |  | RESISTOR 1.5 5\% .75W PW TC $=0+50$ | 91637 | FS1/2-T2 1R5-J |
| A9R 37 | 0757-0401 |  | RESISTCR 10018.125 W F TC $=0+100$ | 24546 | C4-1/8-T0 $=101.5$ |
| A9R38 | 0757-0401 |  | RESISTCR 10018.125 W F TC $=0+100$ | 24546 | $C 4-1 / 8-T 0-101-F$ $C 4 \sim 1 / 8=T 0-5001 \circ$ |
| A9R 39 A9R 40 | $0698-4002$ $0698-4002$ |  |  | 16299 16299 | $\mathrm{C} 4-1 / 8=T 0-5001 \sim \mathrm{~F}$ $\mathrm{C} 4-1 / 8=\mathrm{T} 0=5001=\mathrm{F}$ |
|  |  |  |  |  |  |
| AgVR1 AgVR2 | 1902-3002 | 4 | $\begin{array}{lllll}\text { DIODE-2NR } & 2.37 V & 58 & \text { DO-7 } & \mathrm{PD}=.4 \mathrm{~W} \\ \text { TC= }\end{array}$ | 04713 04713 | SL $10939-2$ SZ $10939-2$ |
| A9VR3 | 1902-3002 |  |  | 04713 | S2 10939-2 |
| A9VR4 | 1902-3002 |  | DIDDE-2NR 2.37V 5\% DO-7 PD=.4W TC=0.074\% | 04713 | SZ 10939-2 |
|  |  |  | a9 miscellaneous |  |  |
|  | $\begin{aligned} & 1480=0073 \\ & 4040=0752 \end{aligned}$ | 7 2 |  | $\begin{aligned} & 00900 \\ & 28480 \end{aligned}$ | $\begin{aligned} & \text { OBD } \\ & 4040=0752 \end{aligned}$ |
| A10 | 86602-60006 | 1 | REFERENCE ASSY | 28480 | 86602-600.66 |
| ${ }^{\text {A }} 10 \mathrm{Cl}$ | 0180-0291 | 2 |  | 56289 | 150D1 $05 \times 903542$ |
|  |  |  |  |  |  |
| A10k1 | 0490-0916 | 6 | RELAY-REED 1 A .5 A 50V CONT 5V-COIL | 28480 | 0490-0916 |
| A10K2 | 0490-0916 |  | RELAY-REED 1A .5A 50V CONT 5V-COIL | 28480 | 0490-0916 |
| A10k3 | 0490-0916 |  | RELAY-REED 1A .5A 50V CONT 5V-CDIL | 28480 | 0490-0916 |
| A $10 \times 4$ | 0490-0916 |  | RELAY-REED 1A .5A 50V CONT 5V-COIL | 28480 | 0490-0916 |
| A10K5 | 0490-0916 |  | RELAY-REED 1A .5A 50V CONT 5V-COIL | 28480 | 0490-C916 |
| Alük6 | 0490-0916 |  | RELAY-REED 1A .5A 50V CONT 5V-COIL | 28480 | 0490-0916 |
| A 1001 | 1853-0020 |  | TRANSISTOR PNP SI PD=300MH FT= 150 MHZ | 28480 | 1853-0020 |
| A 1002 | 1853-0020 |  | TRAFiSISTCR PNP SI PD $=300 \mathrm{MW} \quad \mathrm{FT}=150 \mathrm{MHZ}$ | 28480 | 1853-0020 |
| A1003 | 1853-0020 |  | TRANSISTOR PNP SI PD $=300 \mathrm{MW}$ FT $=150 \mathrm{MHZ}$ | 28480 | 1853-0020 |
| A1004 | 1853-0020 |  | TRANSISTOR PNP SI PD=300MH FT $=150 \mathrm{MHZ}$ | 28480 | 1853-0020 |
| A1005 | 1853-0020 |  | TRANSISTOR PAP SI PD $=300 \mathrm{MW} \quad \mathrm{FT}=150 \mathrm{MHZ}$ | 28480 | 1853-0020 |

Table 6-2. Replaceable Parts


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| Reference Designation | HP Part Number | Oty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | All miscellaneous |  |  |
|  | $\begin{aligned} & 4040-0754 \\ & 1480-0073 \end{aligned}$ | 1 |  | 29480 00000 | $\begin{aligned} & 4040=0754 \\ & 080 \end{aligned}$ |
|  | 86603-00007 | 1 | INSULATOR | 28480 | 86603-00007 |
|  | 0380-0803 | 4 | STANDOFF-RND.094LG.09110.12500 BRS CD | C6540 | 9200-8-8-091 |
| A 12 | 86602-60038 | 1 | LOGIC MOTHER BOARD ASSY | 28480 | 86602-60038 |
| A12C1 | 0160-2055 | 2 | CAPACITOR-FXD . O1UF +80-20\% 100 WVOC CER | 28480 | 0160-2055 |
| A12C2 | 0160-2055 |  |  | 29480 | 0160-2055 |
| A12L1 | 9140-0144 | 2 | COIL $-F X D$ MCLDED RF CHCKE 4.7UH 10\% | 24226 | 10/471 |
| A12L2 | 9140-0144 |  | COIL-FXD MOLDED RF CHOKE 4.7UH 10\% | 24226 | 10/471 |
| A12XA9 | 1251-1626 | 1 | CONNECTOR PC EDGE 12-CONT/ROW 2 RGWS | 71785 | 252-12-30-300 |
| A $12 \times \mathrm{Al} 10$ | 1251-2034 | 1 | CONNECTOR-PC EDGE 10-CONT/ROW 2-RCWS | 71785 | 252-10-30-300 |
| A12XA11 | 1251-1388 | 1 | CONNECTOR-PC EDGE 15-CONT/ROW 2-RJWS | 71785 | 252-15-30-008 |
| A 13 | $86601=60039$ | 1 | ATTENUATOR ASSY(EXCEPT OPTION OO1) | 28480 | 86601-60039 |
| $\begin{aligned} & \text { A } 13 \mathrm{~J} 1 \\ & \text { A13. } \end{aligned}$ |  |  | $\begin{aligned} & \text { NSR } \\ & \text { NSR } \end{aligned}$ |  |  |
| A14 | 86602-60042 | 1 | WIRING HARNESS,MAINIEXCEPT OPT'S 001-002 (INCLUDES P5, P7, P8, P13 \& P14) | 28480 | 86602-60041 |
| A14 | 86602-60042 |  | WIRING HARNESS,MAIN(OPTION OOI ONLY) <br> (INCLUDES P5, P7, P8, P13 \& P14) | 23480 | 86602-60042 |
| A 14 | 86602-60045 |  | WIRING HARNESS,MAIN(OPTION 002 ONLY) (INCLUDES P5, P7, P8, P13 \& P14) | 28480 | 86602-60.245 |
| A15 | 866C2-60035 | 1 | 20 MHZ AMPLIFIER ASSY | 28480 | 86602-60035 |
| A15Cl | 0160-2437 | 7 | CAPACITOR-FXD 5000PF +80-20\% 200WVDC CER NSR | 28480 | 0160-2437 |
| A15 J1 | $1250=1194$ | 3 | CONNECTOR=RF SM-SLC M SGL-HOLE-FR 50-CHM NSR | 28480 | 1250-1194 |
| A15J2 | 1250-1194 |  | CONNECTOR-RF SM-SLD M SGL=HOLE-FR $50-0 H M$ NSR | 28480 | 1250=1194 |
| A16 | 86603-60002 | 1 | PHASE MODULATOR DRIVER ASSY (OPTION 002 ONLY) | 28480 | 86603-60002 |
| ${ }^{\text {A } 16 C 1}$ | 0160-4247 |  | CAPACITOR-FXD . 047 Cl ( +-20\% 50WVDC CER | 28480 | 0160-4247 |
| A16C2 | 0160-0127 | 1 |  | 28430 28480 | $0160=0127$ $0150-4247$ |
| A16C5 | O 160-3874 | 1 | CAPACITOR $\triangle$ FXD 10PF + . 5 PF 200WVDC CER | 28480 | 0160-3874 |
| A16C6 A16C7 | $0160-3879$ $0180-0228$ | 1 | CAPACITOR-FXD -O1UF +-20\% 100WVOC CER CAPACI | 28480 56289 | $\begin{aligned} & 0160-3879 \\ & 1500226 \times 9015 B 2 \end{aligned}$ |
| A16C8 | 0121-0447 | 1 | CAPACITOR $=V$ TRMR $-C E R 1.5 / 2.5 P F 63 V$ | 0086S | 5S-TRIK0 04 |
| A16C9 | 0180-0374 |  | CAPACITOR-FXD 10UF+10\% 20VDC TA | 56289 | 150D106×902082 |
| A16C10 | 0180-0228 |  | CAPACITOR FXD 22UF $¢$ 10\% 15VDC TA | 56289 | $1500226 \times 901582$ |
| A16CR 1 | 1901-0179 | 2 | DIODESSWITCHING 15V 50NA 750PS DO-7 | 28480 | 1901-0179 |
| A16CR2 | 1901-0179 |  | OI ODE-SWITCHING 15V 50NA 750PS DO-7 | 28480 | 1901-0179 |
| A16CR3 | 1901-0033 | 1 | DIODE-GEN PRP 180V 200NA DO-7 | 23480 | 1901=0033 |
| A16E1 | 0410-0184 | 1 | OVEN: CCMPGNENT | 01275 | 5ST1-2 |
| A16J1 A16J2 | $1250-1377$ $1250-1377$ | 2 | CONNECTCR-RF SMB FEM PC CONNECTOR-RF SMB FEM PC | $2 K 497$ $2 K 497$ | $\begin{aligned} & 700214 \\ & 700214 \end{aligned}$ |
| A16L1 | 9140-0158 | 1 | COIL-FXD MOLDED RF ChCKE 1UH $10 \%$ | 24226 | $10 / 101$ |
| A1601 | 1855=0327 | 1 | TRANSISTOR $\quad$-FET $2 N 4416$ N-CHAN D-MODE | 01295 | 2 N 4416 |
| A1602 A1603 | 1854-0023 | 2 | TRANSISTOR NPN SI TO-18 PD=360MW | 28480 23480 | $1854-0623$ $1853-0050$ |
| A1603 A1604 | $1853-0 C 5 C$ $1853-0018$ | 1 | $\begin{array}{llll}\text { TRANSISTCR PNP SI } \\ \text { TRANSISTOR } & \text { PAP SI } & \text { TO-18 } & \text { PD } \\ \text { S }\end{array}$ | 23480 28480 | $1853-0050$ $1853-0018$ |
| A1604 A1605 | $1853-0018$ $1853-0018$ | 2 |  | 28480 28480 | $1853-0018$ $1853-0018$ |
| A1606 | 1854-0345 | 2 | TRANSISTUR NPN 2 N5 179 SI TO-72 PD $=200 \mathrm{MW}$ | 04713 | 2N5179 |
| A1607 | 1854-0345 |  | TRANSISTOR NPN 2 N5 179 SI TO-72 PD=200MW | 04713 | 2N5179 |
| Al608 | 1853-0034 | 1 | TRANSISTCR PNP SI TO-18 PD=360M | 28480 | 1853-0034 |
| A1609 | 1855-0081 | 1 | TRANSISTOR J-FET 2 N5245 N-CHAN D-MODE SI | 01295 | 2N5245 |
| A16010 | 1854-0247 | 1 | TRANSISTOR NPN SI TO-39 PD=1W FT=8COMHZ | 28480 | 1854-0247 |
| A 16011 | 1854-0023 |  | TRANSISTOR NPN SI TO-18 PD=360MW | 28480 | 1854-0023 |
| Al6R1 | 2100-3123 | 1 | RESISTOR-TRMR 500 10\% C SIDE-ADJ 17-TURN | 32997 | 3006P-1-501 |
| Al6R2 Al A | $2100-3095$ $2100-3154$ | 1 | RESISTOR-TRMR 200 10\% C SIDE-ADJ 17 TURN RESISTOR-TRMR 1 L 10\% C SIDE-ADJ 17 TURN | 32997 32997 | $3006 P=1-201$ $3006 P=1=102$ |
| A16R4 | 2100-2633 |  | RESISTOR-TRMR IK 10\% C SIDE=ADJ $1=$ TURN | 30983 | ET50×102 |
| A16R5 | 0698-7216 | 1 | RESISTOR 14728.05 WF TC $=0+2100$ | 24546 | C3-1/8-T0-147R-G |

Table 6-2. Replaceable Parts

| Reference Designation | HP Part Number | Oty | Description | Mfr <br> Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: |
| A16R6 | 0698-7260 | 4 |  | 24546 | C3-1/9-T0-1002-G |
| ${ }_{\text {Albr }}$ Al | 0698-7259 | 1 | RESISTOR 8.25K 28 \% 05 W F TC $=0+\infty 100$ | 24546 24546 | C $3=1 / 8-T 0 \rightarrow 82510 G$ |
| Al6R8 | 0698-7260 |  | RESISTCR 10K 28.05 W F TC $=0+=100$ | 24546 | C3-1/8= T0-1002-G |
| A16R9 | 0698-7250 | 1 | RESISTOR 3.83K 2\%.05W F TC $=0+\infty 100$ | 24546 | 「 $3=1 / 8-70-3831-6$ |
| Al6R10 | 0698-7260 |  | RESISTOR 10K 28.05 W F TC $=0+100$ | 24546 | C3-1/8- T0-1002-G |
| A16R11 | 0698.7243 | 1 | RESISTOR $1.96 \mathrm{~K} 2 \% .05 \mathrm{~W}$ F TC $=0+\infty 100$ | 24546 | $C 3=1 / 8-T 0=1961=G$ |
| Al6R12 | 0698-7260 |  | RESISTOR 10K 2\%.05W F TC $=0+=100$ | 24546 | C3. 1/8- T0-1002-G $^{\text {c }}$ |
| A16R13 | 0693-7236 | 3 | RESISTOR 1 K 28.05W F TC $=0+0100$ | 24546 | C3-1/8- T0-1001-G |
| A16R14 | 0698-7244 | 3 | RESISTOR 2.15K 2t .05W F TC $=0+0100$ | 24546 | ( $3-1 / 8-T 0-21510 \mathrm{G}$ |
| Al6R15 | 0698-7244 |  | RESISTOR 2.15K 2\% .05W F TC $=0+100$ | 24546 | C3-1/8-T0-2151-G |
| Al6R16 | 0693-7244 |  | RESISTOR 2.15K 2\% .05W F TC $=0+=100$ | 24546 | C $3-1 / 8 \rightarrow T 0-2151-G$ |
| A16R17 | 0698-7219 | 2 | RESISTOR 196 2\% . $05 \mathrm{5H}$ F TC $=0+100$ | 24546 | C3-1/8-T0-1960-G |
| Al6R18 | 0698-7219 |  | RESISTOR 196 2\% .05W F TC $=0+\cdots 100$ | 24546 | C3-1/8-T0-196R-G |
| Al6R19 Al6R20 | $0698-7248$ $0757-0418$ | 1 |  | 24546 | C3-1/8-TJ-3161-G |
| Al6R20 | 0757-0418 | 2 | RESISTOR 619 1\% . 125 W F TC= $=0+100$ | 24546 | C4-1/8- $00-619 R=F$ |
| Al6R21 | 0757-0418 |  | RESISTCR 619 1\% . 125 W F TC= $0+100$ | 24546 | C4-1/8-T0-619R-F |
| Al6R22 | 0698-0083 |  | RESISTOR 1.96 K 1\% .125W F TC $=0+=100$ | 16299 | $\mathrm{C} 4-1 / 8-\mathrm{T})=1961=\mathrm{F}$ |
| A16R23 | 0698-7212 | 4 | RESISTOR 100 2\% .05W F TC=0+-100 | 24546 | C $3.1 / 8=T 0=100 R-G$ |
| A16R24 | 0757-0416 |  | RESISTRR 511 1\% .125W F TC $=0+100$ | 24546 | C4-1/8-T0-511R=F |
| A16R25 | 0698-7212 |  | RESISTCR 10028.05 W F TC $=0+100$ | 24546 | C3-1/80 TO-100P=G |
| A16R26 | 0698-7236 |  | RESISTOR 1K 2 LS .05 W F TC $=0+\cdots 100$ | 24546 | C3-1/8-T0-1001-G |
| Al6R27 | 0698-7188 | 2 | RESISTOR 1028.05 W F TC $=0+8100$ | 24546 | C3-1/8-T00-10f-G |
| Al6R28 | 0757-0280 |  | RESISTOR 1K 1\%. 125 W F TC $=0+-100$ | 24546 | C4-1/8-T0-1001-F |
| A16R29 | 0698-7212 |  | RESISTOR 10028.05 W F TC $=0+\rightarrow 100$ | 24546 | C3-1/8-T0-100R-G |
| Al6R30 | 0698-7188 |  | RESISTOR 1028.05 W F TC $=0+\infty 100$ | 24546 | C. $3=1 / 8-T 00=10 R=G$ |
| A $16 R 31$ A16R32 | $0698-7195$ $0698-7195$ | 3 | RESISTOR 19.6 28 .05 W F $T C=0+\infty$ <br> RESISTOR 19.6 28    <br> R      | 24546 24546 | $C 3-1 / 8-T 00=19 R 6=G$ $C 3=1 / 8-T 00=19 R 6=G$ |
| A16R33 | 0698-7212 |  | RESISTGR 100 28 . 105 W F TC $=0+100$ | 24546 | C3-1/8=T0-100R $\mathrm{G}^{\text {C }}$ |
| A16R34 | 0757-0280 |  | RESISTOR 1K 1\% . 125 W F TC $=0+100$ | 24546 | C4-1/8= $50-1001-\mathrm{F}$ |
| A16R35 | 0698-3633 | 1 | RESISTOR 390582 W MO TC= $=0+200$ | 24546 | FP42-2= T00-390R=J |
| ${ }^{\text {Al6R36 }}$ | 0698-7236 |  | RESISTOR 1K 2\% .05W F TC $=0+\infty 100$ | 24546 24546 | $C 3-1 / 8=T 0=1001-G$ |
| A16R37 | 0698-7195 |  | RESISTOR 19.6 $2 \%$.05W F TC=0+-100 | 24546 |  |
| $\begin{aligned} & A 16 U 1 \\ & \text { Al } \end{aligned}$ | $\begin{aligned} & 1858-0032 \\ & 1820-0174 \end{aligned}$ | 1 | IC CA3146E XSTR ARRAY IC SN74 04 N INV | $\begin{aligned} & 02735 \\ & 01295 \end{aligned}$ | CA3146E SN7404N |
|  |  |  | al6 miscellaneous |  |  |
|  | $\begin{aligned} & 1200-0173 \\ & 1480-0073 \end{aligned}$ | 1 | INSULATOR-XSTR TO $=5$. 075-THK PIN: DRIVE 0.250" LG | $28480$ <br> 00 CO | $\begin{aligned} & 1200-0173 \\ & \text { OBD } \end{aligned}$ |
|  | 4040-0748 | 1 | EXTRACTOR↔PC BD BLK POLYC . $062=$ BD THKNS | 28480 | 4040-0749 |
|  | 4040-0750 | 1 | EXTRACTOR-PC BD RED POLYC . 062 -BD-THKNS | 28486 | 4(4)0-075:) |
| A17 | $86603-60019$ $86603-00004$ | 1 | PHASE MODULATOR ASSY(OPTION 002 ONLY) CCVEE, Phase modulator housing | 28480 28480 | $\begin{aligned} & 86603-60019 \\ & 86603-00004 \end{aligned}$ |
|  | 86603-20011 | 1 | HOUS ING, PHASE MODULATOR | 28480 |  |
| A17J1 | 1250-1194 |  | CONNECTUR-RF SM-SLD M SGL-HOLE-FR 50-0HM | 28480 | 1250-1194 |
| A 17 Pl | 1250-0563 | 2 | CONNECTOR-RF SMA M 4 HOLE FLG FR | 28480 | 1250-0563 |
| A 17 P2 | 1250-0563 |  | CCNNECTOR-RF SMA M 4 HOLE FLG FR | 28480 | 1250-0563 |
| Al7Al | 86603-60003 | 1 | phase modulator board assy | 28480 | 86603-60003 |
| Al7A1C1 | 0160-0559 | 3 | CAPACITOR-FXD 10PF +-10\% 100WVCC CER | 28480 | 0160-0559 |
| Al7AlC2 | 0160-0559 |  | CAPACITOR-FXD 10PF +ol0\% 100WVCC CER | 28480 | 0160-0559 |
| Al7AlC 3 | 0160-0559 |  | CAPACITOR-FXD 10PF tol0\% 100WVCC CER | 28480 | 0160-0559 |
| A17AlCR1 | 0122-0074 | 2 | DIODE-VVC . 7 PF 10\% CO/C25-MIN=4 BVR=40V | 96341 | MA45644 |
| A17A1CR2 | 0122-0074 |  | DIODE-VVC .7PF 10\% CO/C25-MIN=4 BVR=40V | 96341 | MA45644 |
| A18 | 0955-0045 | 1 | CIRCULATOR 4-PORT (OPTION 002 ONLY) | 28480 | 0955-0045 |
| A19 | 0960-0426 | 1 | ISOLATOR ASSEMBLY, 3.9-4.1 GHZIOPT OC2) | 28480 | 0960-0425 |
| A 20 | 86602-60043 | 1 | FILTER CONTROL ASSY(OPTION 002 ONLY) | 28480 | 86602-60043 |
| A 20Cl | 0180-0374 |  | CAPACITOR-FXO LOUF-108 20VDC TA | 56289 | $1500106 \times 902$ OB2 |
| A20C2 | 0180-0374 |  | CAPACITOR - FXD 10UF $+10 \%$ 20VDC TA | 56289 | $1500106 \times 902082$ |
| A20C3 | 0180-0291 |  | CAPACITOR-FXC 1UF+ $\sim$ 10\% 35VDC TA | 56289 | $1500105 \times 9035$ A2 |
| A 2011 | 9140-0210 | 1 | COIL-FXD MOLDED RF CHOKE 100UH 5\% | 24226 | 15/103 |
| A $20 \mathrm{R1}$ | 0757-1094 | 1 | RESISTOR 1.47K 1\% .125W F TC $=0+100$ | 24546 | C4-1/8-T0-1471-F |
| A $20 \mathrm{R2}$ | 0757-0442 |  | RESISTOR 10K 1\% .125W F TC=0+ 100 | 24546 | C $4-1 / 8-\mathrm{T} 0-1002-F$ |
| A 20 R 3 | 0757-0441 | 1 | RESISTER 8.25K 1\% .125W F TC $=0+100$ | 24546 | C4-1/8-T0-8251-F |
| $\begin{aligned} & \text { A20U1 } \\ & \text { A20U2 } \end{aligned}$ | $\begin{aligned} & 1820=0661 \\ & 1826-0013 \end{aligned}$ | 1 | IC SN74 32 N GATE IC OP AMP | $\begin{aligned} & 01295 \\ & 28480 \end{aligned}$ | $\begin{aligned} & \text { SN7432N } \\ & 1826-0013 \end{aligned}$ |

Table 6-2. Replaceable Parts


Table 6-2. Replaceable Parts

| Reference Designation | HP Part Number | Oty | Description | Mfr Code | Mfr Part Number |
| :---: | :---: | :---: | :---: | :---: | :---: |
| P13 | 1251-2262 | 1 | CONNECTOR=PC EDGE $10 \cdot$ CUNT/ROW 2-ROWS (PART OF A14) | 71785 | 251-10-30-400 |
| P 14 | 1251-2500 | 1 | CONNECTOR-PC EDGE 6-CONT/ROW 2-ROWS (PART OF A14) | 71785 | 251-060 $31-400$ |
| R1 | 2100-3113 | 1 | RESISTOR-VAR CONTROL CC 2.5K 10\% 10CW | 01121 |  |
| R2 | 0698-3430 | 1 | RESISTOR 21.5 1\% . 125 W F TC=0+-100 | 03828 | PMF55-1/B=T0 21R5-F |
| S1 S1 | $3100=3088$ $3100-3050$ | 1 | SWITCH, ROTARY (OPTION OO1 ONLY) SHITCH, RCTARY (EXCEPT OPTION OO1) | 28480 28480 | $3100-3093$ $3100-305$ |
| S1 | 3100-3050 | 1 | SHITCH, RCTARY (EXCEPT OPTION 001) | 28480 | 3100-305: |
| TB1 | 0360-1780 | 1 | TERMINAL; STRIP; 5-TERM | 71032 | 13558 |
| W1 | $86603-20038$ $86603-20012$ | 1 | CABLE ASSY, FILTER OUTPUT(EXCEPT OPT OO2) CABLE ASSY, FILTER OUTPUT(OPT OO2 ONLY) | 23480 28480 | $86603-20038$ 86603020012 |
| $W 1$ $W 2$ | 86603-20012 | 1 | CABLE ASSY, FILTER OUTPUT(OPT OO2 ONLY) CABLE ASSY,MIXER LO INPT(EXCEPT OPT OO2) | 28480 28480 | $86603-20012$ $86603-20037$ |
| W2 | 86603-20014 | 1 | CABLE ASSY,MIXER LO INPT(OPT 302 ONLY) | 28480 | 86603-20¢14 |
| W3 | 86603-60013 | 1 | CABLE ASSY,RF INPT (INCL MP12 \& MP14) | 28480 | 86603-60013 |
| W4 | 86603-20016 | 1 | CABLE ASSY, ISOLATOR OUTPUT | 28480 | 86603-20.116 |
| W5 | 86603-20015 |  | CABLE, MIXER, RF INPUT | 28480 | $86603-20015$ |
| W6 | 86603-20017 | 1 | CABLE ASSY, MIXER OUTPUT | 28480 | 86603-20017 |
| W7 | 86602-20021 | 1 | CABLE ASSY, OUTPUT (EXCEPT OPT OO11) | 28480 | $86602=20021$ |
| W7 | 86602-20016 | 1 | CABLE ASSY, OUTPUT (OPTION OO1 ONLY) | 28480 | 86602-20016 |
| W8 | 86602-60012 | 1 | CABLE ASSY,AM INPT, GRAY/YELLOW <br> (INCLUDES MP10, P/O P6) | 28480 | 86602-60012 |
| W9 | 86602-60023 | 1 | CABLE ASSY,PULSE INPT, WHITE/GREEN (INCLUDES MPIU \& MPI1, P/O PGI | 23480 | 86602-60023 |
| W10 | 86603-20013 | 1 | CABLE, CIRCULATOR CUTPUTIOPTION 002 JnLY) | 28480 | 86603-20.013 |
| W11 | 8660360014 | 1 | CABLE ASSY,LO INPT (INCLUDES MP12 EMP 14) | 28480 | $86603=60014$ $86603-60015$ |
| W12 | 86603-60015 | 1 | CABLE,PHASE MOD DR IVER INPTIOPT 002 ONLY; INCLUOES MP10 \& MP13) | 28480 | 86603-60015 |
| W13 | 86603-20036 | 1 | CABLE ASSY, CIRCULATOR INPTIOPT 002 ONLY | 28480 | 86603-20036 |
| W14 | 86603-60012 | 1 | CABLE,PHASE MOD DRIVER OUTPUT(OPT 002 ONLY INCLUDES MP13) | 28480 | 86603-60012 |
| 115 | 86602-60033 | 1 | CABLE ASSY, 2 OMHZ INPT, WHITE/BLUE <br> (INCLUDES MP10 \& MP11, P/O P6) | 28480 | 86602-60.33 |
| W16 | 8120-1126 | 1 | CABLE ASSY, $20 / 30 \mathrm{MHZ}$, WHITE/ORANGE (P/O P6; SEE MP10) | 28480 | 8120-1126 |
| W17 | 8120-1129 | 1 | CABLE ASSY,360/450MHZ, WHITE/YELLOW (P/O P6; SEE MP10) | 28480 | 8120-1129 |
| W18 | 8120-1128 | 1 | CABLE ASSY, 100 MHZ , WHITE/BRDWN (P/O P6; SEE MP10) | 28480 | 8120-1129 |
| W19 | 86602-60034 | 1 | CABLE ASSY, 2OMHZ CUTPUT, WHITE/RED (INCLUDES MP10 \& MP11, P/O P6) miscellaneous parts | 28480 | 86602-60034 |
|  | $\begin{aligned} & 0370=1089 \\ & 0370-1107 \end{aligned}$ | 1 | KNOBOBASEERND. 5 IN JGK SGI-DECAL KNOB-BASE-PTR AND BAR . 5 IN JGK (OPTION 001 ONLY) | 28480 28480 | $\begin{aligned} & 0370-1089 \\ & 6370-1107 \end{aligned}$ |
|  | $\begin{aligned} & 0370-2386 \\ & 3050-0029 \end{aligned}$ | 1 | KNOB(EXCEPT CPTION 001) <br> WASHER-FL MTLC NO.-3/8 •378-IN-ID | 28480 28480 | $\begin{aligned} & 0370-2386 \\ & 3 C 50-0029 \end{aligned}$ |
|  | 3050-0090 | 1 | WASHER-SPR WAVY NO. 5 5/8 .64-IN $=10$ (EXCEPT OPTION OO1) | 78189 | 3564-28-01 |
|  | $86601-00013$ $86601-00014$ | 1 | LATCH BRACKET, ATTENUATOR(EXCEPT OPTION OO1) | 28480 28480 | $\begin{aligned} & 86601-00013 \\ & 86601=00014 \end{aligned}$ |
|  | 86601-00034 | 1 | PANEL, FRONT (EXCEPT OPTION OO1) | 28480 | 86601-0.0034 |
|  | $86661-00036$ $86601-00052$ | 1 | MOUNT, METER CCVER, HALF | 28480 28480 | $\begin{aligned} & 86601-00036 \\ & 86601-00052 \end{aligned}$ |
|  | 86601-20017 | 1 | HOUS ING, FRONT | 28480 | 86601-20017 |
|  | 86601-20018 | 1 | PANEL, REAR | 28480 | $86601-20018$ |
|  | 86601-20019 | 1 | Stud latch | 28480 | 86601-20019 |
|  | 86601-20020 | 1 | WASHER LATCH | 28480 | 86601-20.220 |
|  | 86601-20069 | 1 | FRAME, FRONT PANEL GUIDE, PLUG-IN | 28480 | $86601-20069$ |
|  | $86601-20080$ $86601-40018$ | 2 | GUIDE, PLUG-IN SCREW, METER ADJUST | 28480 23480 | $\begin{aligned} & 86601-20980 \\ & 86601=40018 \end{aligned}$ |
|  | 86602-00005 | 1 | SUPPORT, TCP | 28480 | 86602-00005 |
|  | $86602-00006$ $86602=00007$ | 1 | SUPPORT, BCTTOM PANEL, FRCNT (CPTION 001 nNLY) | 28480 28480 | $86602-0.3006$ $86602=00007$ |
|  | 86602-20019 | 2 | PLATE, FRCNT SUPPORT | 28480 | 86632-20.19 |
|  | 866C3-20028 |  | PLATE, REAR SUPPORT | 28480 | 86603-20028 |
|  | 86602-20028 | 2 | GUIDE, CONNECTCR | 28480 | 86602-20028 |
|  | $\begin{aligned} & 86603-00001 \\ & 86603-00002 \end{aligned}$ | 1 | SUPPORT, RIGHT FRONT SUPPORT, RIGHT REAR | 28480 28480 | $\begin{aligned} & 86603-30,301 \\ & 86603=00302 \end{aligned}$ |
|  | 86603-00003 | 1 | SUPPORT, MIXER | 2848 C | 86603-00,03 |
|  | $866 C 3-C J J C 8$ $86602-20041$ | 1 | SUPPORT, LEFT WINDOW (EXCEPT CPTION 002) | 28430 28480 | $86603-0.0008$ $86602-20041$ |
|  | 86602-20042 | 1 | WINDOW (OPTICN 002 CNLY) | 28480 | 86602-20.342 |

Table 6-3. Code List of Manufactures

| Mfr Code | Manufacturer Name | Address | Zip Code |
| :---: | :---: | :---: | :---: |
|  | K.s. A. A. Common STETNERRTRUSH INC TEXAS INSTK INC SEMICONO CMPNT DIV RCA CORD TOLIO SIATE OIV <br>  MUMOROLA SEHICONDUCTOR PRDOUCTS <br>  <br>  <br>  <br>  VARAONNE INC NATIONAL SEMICONOUCTUR CORP MEELETT-PACKARO COOCOCORPORATE HE MoDutec Inc <br>  birnack co inc <br> TRW ELEK COMPONENTS CIINCH DIV <br>  <br>  AMPE NGL SALES OIV UF BUNKER-RAMO DALE ELECTRONCS INC CNT <br>  sealectro cyap | ANY SUPPLIER OF THE U.S.A. CAZENOVIA NY <br> MILWAUKEE HI <br> SOMMERVILLE NJ <br> WHIPPANY NJ <br> NEW ROCHELLE NY <br> RALEIGH NC SUNNYVALE <br> MINERAL WELLS TX <br> NORTH HAVEN CT <br> GOWANDA NY BRADFORD PA <br> INDI ANAPOLIS IN <br> SANTA CLARA CA <br> PALO ALTO CA <br> NORWALK CT <br> RIVERSIDE CA <br> NORTH ADAMS MA FREEPORT LI NY <br> ELK GROVE VILLAGE IL ELGIN IL <br> WARMINSTER PA <br> HAZVILLE CT <br> COLUMBUS NE <br> WOODSIDE NY <br> MAMARONECK NY |  |

## SECTION VII <br> MANUAL CHANGES

## 7-1. INTRODUCTION

7-2. This section contains information for adapting this manual to instruments for which the content does not apply directly.

## 7-3. MANUAL CHANGES

7-4. To adapt this manual to your instrument, refer to Table 7-1 and make all of the manual changes listed opposite your instrument serial
number. Perform these changes in the sequence listed.

7-5. If your instrument serial number is not listed on the title page of this manual or in Table 7-1 below, it may be documented in a yellow MANUAL CHANGES supplement. For additional important information about serial number coverage refer to INSTRUMENTS COVERED BY MANUAL in Section I.

Table 7-1. Manual Changes by Serial Number

| Serial Prefix or Number | Make Manual Changes |
| :---: | :---: |
| 1433 A | A |

## 7-6. MANUAL CHANGE INSTRUCTIONS

## CHANGE A

Table 6-3:
Change A9R5, R6, R15, R16, R25, and R26 to 0811-2815, RESISTOR 1.5 OHM $5 \% 0.5 W$ PW TUBULAR, 91637, RS1/2-T2-IR5-J.

## Service Sheet 10:

Change the value of A9R5, R6, R15, R16, R25, and R26 to 1.5 OHM.

## SECTION VIII SERVICE

## 8-1. INTRODUCTION

8-2. This section contains troubleshooting and repair information for the RF Section plug-in. Safety of technical personnel is considered. Circuit operation and troubleshooting on system, plug-in and assembly levels is provided.
$8-3$. The service sheets normally include principles of operation and troubleshooting information, a component location diagram, and a schematic, all of which apply to a specific portion of circuitry within the instrument.

8-4. Information related to operation of the RF Section plug-in as part of the 8660 -series Synthesized Signal Generator System is provided in Service Sheet 1 .

8-5. Service Sheets 2 and 3 include an overview of RF Section operation, troubleshooting on an assembly or stage level, and a troubleshooting block diagram. The block diagrams also serve as an index for the remaining service sheets.

8-6. The Schematic Diagram Notes, Figure 8-3, aid in interpreting the schematics.

8-7. The last foldout in the manual includes a table which cross-references all pictorial and schematic locations of each assembly, chassis mounted component, and adjustable component. The figure is a pictorial representation of the RF Section and shows location of the aforementioned parts.

## 8-8. SAFETY CONSIDERATIONS

8-9. Although this instrument has been designed in accordance with international safety standards, this manual contains information, cautions, and warnings which must be followed to ensure safe operation and to retain the instrument in safe condition (see Sections II, III, and V). Service and adjustments should be performed only by qualified service personnel.

8-10. Any adjustment, maintenance, and repair of the opened instrument under voltage should be avoided as much as possible and, when inevitable, should be carried out only by a skilled person who is aware of the hazard involved.

8-11. Capacitors inside the instrument may still be charged even if the instrument has been disconnected from its source of supply.

## WARNING

The service information is often used with power supplied and protective covers removed from the instrument. Energy available at many points may cor:stitute a shock hazard.

## 8-12. PRINCIPLES OF OPERATION

8-13. The Principles of System Operation explains how the RF Section operates within the Synthesized Signal Generator System, i.e., how other sections affect the RF Section and in turn how they are affected by the RF Section. Control functions in both local and remote modes are also explained.

8-14. Service Sheet 1 includes a block diagram and an explanation of system operation with respect to the RF Section.

8-15. Overall operation of the RF Section is discussed in Service Sheet 2 and 3. The remaining service sheets are concerned only with sections and/or circuit assemblies within the RF Section plug-in.

## 8-16. TROUBLESHOOTING

## NOTE

When a malfunction occurs, refer to Section VIII of the HP Model 8660series mainframe Operating and Service Manual to begin troubleshooting (System Troubleshooting Guide). Then, if that information indicates possible problems in the RF Section, refer to the Systems Troubleshooting information in Service Sheet 1. This information may be used to isolate the defect to the RF Section, another plug-in, or the mainframe. If the problem is in this plug-in, turn to Service Sheet 2 for further troubleshooting information.

## 8-17. System Troubleshooting

8-18. The System Troubleshooting information in Section VIII of the HP 8660-series mainframe manual should be used when first attempting to isolate a circuit defect. If the defect cannot be isolated to an individual instrument in the system, the technician is normally directed to the System Troubleshooting in the RF Section manual (Service Sheet 1). The problem may then be isolated to the RF Section, Modulation Section, Frequency Extension Module, or the mainframe.

## 8-19. RF Section Troubleshooting

8-20. When the defect has been isolated to the RF Section, refer to Service Sheet 2. This information is used to isolate the problem to a section or assembly.

## 8-21. Troubleshooting Aids

8-22. Circuit Board Aids. Test points are physically located on the circuit boards as metal posts or circuit pads and usually have either a reference designator (such as TP1) or a label which relates to the function (AM, Pulse, ID, etc.). Transistor emitters, diode cathodes, the positive lead of electrolytic capacitors, and pin 1 of integrated circuits are indicated by a variety of symbols such as E , a diode symbol, + , and a tear-drop shape respectively. Also, a square circuit pad (as opposed to the round pad) may be used in place of any of the previously mentioned symbols.

8-23. Service Sheet Aids. RF levels, ac voltages, and dc voltages are often shown on schematic diagrams. Integrated circuit connection diagrams plus diagrams of relays and printed circuit connectors help to locate specific inputs and outputs. Notes are used to explain certain circuits or mechanical configurations not easily shown on the schematic.

8-24. The locations of individual components mounted on printed circuit boards are found on individual service sheets on the pictorial representation of the circuit boards. Chassis mounted parts, major assemblies, and adjustable components locations are found on the last foldout in this manual.

8-25. Table 8-3, Schematic Diagram Notes, provides information relative to symbols and values shown on the schematic diagrams.

8-26. Service Kit and Extender Boards. The HP 11672A Service Kit contains interconnect cables, RF cables, various coaxial adaptors, and an adjustment tool, all of which are useful in servicing the RF Section plug-in. Refer to the HP 11672A Operating Note for a listing and pictorial representation of the contents. A list of the service kit contents is also found in the Test Equipment and accessories list in Section I of the mainframe manual.

8-27. Circuit board extenders are provided with the mainframe. These extender boards enable the technician to extend plug-in boards clear of the assembly to provide easy access to components and test points. Refer to the list found under Accessories Supplied in Section I of the mainframe manual.

## 8-28. RECOMMENDED TEST EQUIPMENT

8-29. Table 1-2 lists the test equipment and accessories recommended for use in servicing the instrument. If any of the recommended test equipment is unavailable, instruments with equivalent specifications may be used.

## 8-30. REPAIR

## 8-31. General Disassembly Procedures

8-32. Procedures for removing the RF Section plugin from the mainframe and the covers from the plug-in are found on the left-hand foldout page immediately preceding the last foldout in the manual.

8-33. The machine screws used throughout the plug-in have a Pozidriv head. Pozidriv is very similar in appearance to the Phillips head, but using a Phillips screwdriver may damage the Pozidriv screw head.

## 8-34. Non-Repairable Assemblies

$8-35$. Repairs should not be attempted on the following assemblies if any is found to be defective during troubleshooting:

## A5 Modulator Assembly

A6 1-1300 MHz Amplifier Assembly
A8 4 GHz Amplifier Assembly
A13 Attenuator Assembly
A15 20 MHz Amplifier Assembly
A18 Circulator Assembly
A19 3.9-4.1 GHz Isolator Assembly
AT1 Isolator
AT2 3 dB Attenuator
FL1 4 GHz Band Pass Filter

## 8-36. Module Exchange Program

8-37. Only the A13 Attenuator is available as a restored assembly. It may be ordered as a replacement under the Module Exchange Program. Refer to Section VI for ordering information.

## 8-38. Repair Procedures

8-39. LO Signal Circuits Repair Procedure. Refer to Figure 8-1. This procedure is used in conjunction with Service Sheet 2 for isolating circuit defects which are evident as a phase modulation problem or an incorrect LO signal level (option 002 instruments only). Perform the procedure if one of the following components is suspected of being defective: W1, W2, W10, W13, W14, A7, A8, A17, A18, A19, or AT2.

8-40. Front Panel Housing Disassembly and Repair Procedure. Circuits and parts located in the front

Panel Housing are the meter, output range switch, and vernier control. Perform the procedure in Table 8-1 to gain access to these circuits for purposes of repair.

8-41. Rear Panel Disassembly Procedure. To gain access to assemblies and parts mounted on or behind the rear panel, refer to Figure 8-2. The A12 Logic Mother Board, A15 20 MHz Amplifier, and the P6 Interconnect Plug are accessible only after removing the panel.

## 8-42. Post Repair Adjustments

8-43. After a defective circuit is repaired, refer to Section V and perform the adjustment procedure(s) for circuits which may be affected by the change. Consider the instructions under paragraphs entitled Related Adjustments and Post Adjustment Tests.

## LO SIGNAL CIRCUITS REPAIR



## NOTE

In conjunction with this procedure, use the troubleshooting information on Service Sheet 2 to isolate a circuit malfunction to one of the following assemblies, circuits, or cables: A7, A8, A18, A19, AT2, W1, W2, W10, or W13 (RF problem); A17 or W14 (phase modulation problem). The procedure applies for option 002 instruments only.
a. Set the System Line switch to Standby.
b. Remove screws 2, 7 , and 14 to release the A17 Phase Modulator (3) and A18 Circulator 5 Assemblies.
c. With a $5 / 16^{\prime \prime}$ open end wrench, loosen the SMA connectors (6) 8 , and (3). Carefully pull the assemblies 3 and away from the aluminum decking until A17 3 slips past AT1 1 .

Figure 8-1. LO Signal Circuits Repair (1 of 3)
d. Phase Modulation Problems. Separate A17 and A18 at connectors 4 and (11) Set the system LINE switch to ON. Measure the output of W14 at connector 12 .
e. Set the system LINE switch to Standby, replace the defective part of assembly. Reassemble the items in the reverse order given for disassembly.

## Be sure W14 13 runs under connector 11 and is not crushed under A17 1

f. RF Problems. To measure the LO signal at the output of A18 (10) , remove the SMA connectors (6) and 8) and set the System LINE switch to ON.
g. If the output from A18 is correct, proceed to step h. Otherwise, determine which of A18, W13, A19, or W1 is defective by measuring the outputs of W13, A19, and W1. Refer to Service Sheet 2.
h. Disconnect the System's line (Mains) power. Release the A20 Assembly by removing the screws (one each where circuit board and aluminum decking meet). Lift the assembly straight up. Connect a ground lead from the chassis to the angle bracket which is connected to the ground point on the circuit board.
i. Remove cable W2 at the A8 Assembly output. (The A8 output jack is closer to the top of the RF Section).
j. Reconnect the System's line (Mains) power. Measure the output level from A8 (refer to Service Sheet 2). If the output level is correct, determine if cable W2 or the A7 Mixer Assembly is defective. If the level is incorrect, proceed to step k .
k. Remove the three screws which secure the A8 Assembly. Remove the cable connector 98 at the output of A18. Carefully pull A8 away from the decking so the end of AT2 (connected to the input of A8) is exposed.

1. With the wrench, loosen and remove AT2 from A8. Carefully remove W10 and AT2 from between the decking.
m. Reconnect the cable to the output of A18 10 . Check the outputs from AT2 and W10 to determine if AT2, W10, or A8 is defective (refer to Service Sheet 2).
n. Discard the defective part or assembly. Reassemble the items removed in the reverse order (leave A20 till last).

## CAUTION

When tightening the coaxial connectors, be sure the other end of the cable can be connected without bending the cable. Be sure all connectors are tightened but only enough to ensure a good connection. Excessive bending of semi-rigid coax or excessive tightening of the connectors may damage the cables and/or connectors beyond repair.

## FRONT PANEL HOUSING DISASSEMBLY AND REPAIR

a. Place the RF Section in the normal upright position.
b. With a Pozidriv screwdriver, remove the two screws which hold the top of the front panel to the housing.
c. Turn the plug-in over with the bottom up. Remove the screw which is seen through the curved cutout slot in the latch when it is in the closed or latched position.
d. With a knurled nut wrench, loosen the knurled nut on the OUTPUT jack. Remove the nut by hand.
e. Pull the front panel away from the housing.
f. Determine what part or assembly is defective and replace it.
g. Reinstall the front panel by following the preceding steps in the reverse order. Be careful not to crush any wires between the front panel and the chassis.

## REAR PANEL DISASSEMBLY


a. On the rear panel, remove screws 1 and 2 which hold the A13 Assembly in place. Screw (1) is located under the Option 002 sticker.
b. Remove the screws 5 and (6) which hold the top rear deck to the rear panel.
c. Remove the screws and 4 which hold the rear panel to the left rear deck. Carefully pull the rear panel back and away to expose the assemblies and parts.

## SCHEMATIC DIAGRAM NOTES

Resistance in ohms, capacitance in microfarads, inductance in microhenries other otherwise noted.

Asterisk denotes a factory-selected value. Value shown is typical. Part may be omitted.

Indicates backdating. Refer to Table 7-2.

Tool-aided adjustment.
Manual control.

Encloses front-panel designation.
[---] Encloses rear-panel designation.
Circuit assembly borderline.

$\xrightarrow{\text { CW }}$| Other assembly borderline. Also used to indicate mechanical inter- |
| :--- |
| connection (ganging). | | Heavy line with arrows indicates path and direction of main signal. |
| :--- |
| Heavy dashed line with arrows indicates path and direction of main <br> feedback. |
| Wiper moves toward CW with clockwise rotation of control (as viewed <br> from shaft or knob). |

Numbered Test point. Measurement aid provided.
 No measurement aid provided.

Encloses wire color code. Code used is the same as the resistor color code. First number identifies the base color, second number identifies the wider strip, third number identifies the narrower stripe. E.g., 947 denotes white base, yellow wide stripe, violet narrow stripe.

A direct conducting connection to the earth, or a conducting connection to a structure that has a similar function (e.g., the frame of an air, sea, or land vehicle).

Coaxial or shielded cable.

Stripline (i.e., RF transmission line above ground).

## SCHEMATIC DIAGRAM NOTES



Arrows on relays indicate direction of arm movement when energized.

Filters. Specific type indicated by crosses on curved lines.


Example of Highpass Filter.

## SWITCH DESIGNATIONS

EXAMPLE: A3S1AR(2-1/2)

A3S1 = SWITCH S1 WITHIN ASSEMBLY A3
$A=$ 1ST WAFER FROM FRONT ( $A=1 S T, E T C$ )
$R=$ REAR OF WAFER ( $F=F R O N T$ )
$(2-1 / 2)=$ TERMINAL LOCATION (2-1/2) (VIEWED FROM FRONT)



## SERVICE SHEET 1

## NOTE

When a malfunction occurs, refer to Section VIII of the HP Model 8660series mainframe Operating and Service Manual to begin troubleshooting (System Troubleshooting Guide). Then, if that information indicates possible problems in the RF Section, refer to the Systems Troubleshooting information in this manual (Service Sheet 1). This information may be used to isolate the defect to the RF Section, another plug-in, or the mainframe. If the problem is in this plug-in, refer to Service Sheet 2 for further troubleshooting information.

## RF SECTION OPERATION IN THE SYNTHESIZED SIGNAL GENERATOR SYSTEM

In order to understand the operation of the RF Section or to effectively troubleshoot it, the entire Synthesized Signal Generator System must be understood. The emphasis here is on the RF Section and its relationship with the other units which make up the system.

## PRINCIPLES OF OPERATION

The HP Model 86602B RF Section Plug-in (as part of the HP 8660 -series Synthesized Signal Generator System, has an RF Output of +10 to -146 dBm across $50 \Omega$ from 1 to 1299.999999 MHz . The RF signals coupled from mainframe to the Frequency Extension Module are converted to two phaselocked outputs which are coupled to the RF Section. The signals are mixed, amplified, and coupled to the OUTPUT jack through the RF Attenuator.

The RF detector produces a dc output proportional to the RF output signal. The dc output is compared to a reference voltage. Any difference in dc levels produces an error current which drives the PIN diode modulator. The current flow through the PIN diodes controls the RF output level. The negative feedback loop described, is an ALC loop which holds the RF output level constant.

## Output Frequency Selection

The desired output frequency is selected by the Digital Control Unit (DCU) in the mainframe. Control logic levels to the mainframe RF circuits set the frequencies of the signals to the Frequency

Extension Module. Other logic levels are coupled to the extension module from the mainframe to set the frequency of the generated RF outputs which are coupled to RF Section. The signals are mixed and the converted signal is coupled to the OUTPUT jack.

## Modulation Selection

Depending on the Auxiliary or Modulation Section, amplitude, frequency, phase, or pulse modulation may be selected.
a. The amplitude modulation drive signal is coupled to the RF Section from the Modulation Section. The drive signal is superimposed on the reference level which controls the ALC loop. Thus, the ALC loop causes the RF output level to change at the modulation signal rate.
b. Frequency modulation is accomplished by setting the modulation mode control to FM. The modulation drive signal frequency modulates a 20 MHz VCO signal which is generated in the Modulation Section. This signal is coupled to the RF Section, amplified, and coupled on to the Frequency Extension Module. The extension module circuits transfer the frequency modulation information from the 20 MHz signal to the 3.95 to 2.75 GHz oscillator signal. This signal is then coupled to the RF Section circuits.
c. Phase modulation occurs when the selected modulation mode is set to $\emptyset \mathrm{M}$. The modulation drive signal from the modulation section is applied to the LO signal so its phase deviation varies with the drive signal amplitude.
d. The Pulse ID logic input opens the ALC loop so there is no RF output without a pulse modulation drive signal. A -10 volt peak pulse will momentarily bias the RF output on.

## RF Output Level Selection

The RF output level is selected by the front panel OUTPUT RANGE switch and the VERNIER control. The VERNIER control (in conjunction with the front panel meter) is used to set the output within a usable range of 10 dB . The OUTPUT RANGE switch controls the output level range by inserting attenuation in 10 dB steps to 150 dB .

## SERVICE SHEET 1 (Cont'd)

## Remote Operation

In remote mode the frequency, modulation, and RF output levels are programmed into the DCU. Through parallel BCD PI (plug-in) control lines, an input is sent to the various storage registers. A one-of-six address selects the register which will accept the information. Frequency information is routed into one of 3 registers: center frequency, step (except 8660A), and sweep (except 8660A). Modulation information is routed to either the Modulation Mode/Source register or the Modulation Level register. RF output level (attenuation) information is routed to the attenuation storage register in the RF Section by addressing the ATTN CLK.

The attenuation information is stored in the register until new data is received. Until that time the stored information is connected through various logic and decoding circuits and applied to the relays and switches which set the RF output level to the desired value. The RF Section front panel controls are inoperative in the remote mode.

## SYSTEM TROUBLESHOOTING

When a malfunction occurs, refer to Section VIII of the HP Model 8660 -series mainframe Operating and Service Manual to begin troubleshooting (System Troubleshooting Guide). Then, if that information indicates possible problems in the RF Section, return to this service sheet and perform the following tests which may help isolate the problem to an instrument (mainframe or a plug-in).

## Preparing the RF Section for Troubleshooting

Follow the Removal and Disassembly Procedures on the foldout page which just preceeds the last foldout in the manual. Follow the directions for removing the RF Section from mainframe, removing its covers, and making the interconnections from mainframe to RF Section for troubleshooting purposes.

## Output Level Incorrect

The following steps check the signal levels input to the RF Section from the Frequency Extension Module. Also, the attenuation data input to the RF Section must be checked if the instrument is being operated in the remote mode.
a. Disconnect the RF cable connected to P2 (on rear panel above the multi-pin connector P6). Measure the level of the 3.95 to 2.75 GHz signal from the cable with a spectrum analyzer ( $>+10 \mathrm{dBm}$ ). Reconnect the cable to P2.
b. Disconnect the RF cable connected to P1 (on rear panel below the multi-pin connector). Measure the level of the 3.95 to 4.05 GHz signal from the cable with a spectrum analyzer ( $>-4 \mathrm{dBm}$ ). Reconnect the cable to P1.
c. If either signal level from the extension module is incorrect, the problem is either in the extension module or the interconnections to the RF Section. Check the continuity of the cables and, if necessary, refer to the extension module manual for further troubleshooting information.
d. If both signal levels are correct and the system is being operated in the remote mode, switch to local (front panel) control. If the problem is still evident, refer to Service Sheet 2 for further troubleshooting information.
e. If the problem disappears, check continuity of the input data lines (PI-1, PI-2, PI-4, and PI-8) and the ATTN CLK input to the mainframe. If continuity exists, proceed to Section VIII of the mainframe manual and troubleshoot the DCU. Otherwise, refer to Service Sheet 3.

## Frequency Problems

The mainframe center frequency readout is correct but the frequency at the RF Section's front panel jack is incorrect. The mainframe, and the frequency Extension Module contain the only controlled frequency sections. If the RF frequencies to the extension module are incorrect or if the levels are too low, the circuit defect is in the mainframe or the interconnections to the extension module (including the A15 20 MHz Amplifier Assembly). If these levels and frequencies are all correct, the extension module is malfunctioning or the data input from the mainframe DCU is incorrect.

## NOTE

If the coaxial test cable 11672-60008 (for checking outputs from the multi-pin connector J6) is not available, proceed to step $b$.

SERVICE SHEET 1 (Cont'd)

RF Signal Levels

| Pin <br> Numbers <br> J6 (Main- <br> frame) or <br> Inter- <br> connect <br> Cable | Frequency* (MHz) | Signal <br> Level <br> (dBm) |
| :---: | :--- | :--- |
| 62 | $20 \mathrm{MHz} \pm 1 \mathrm{~Hz}$ |  |
| 63 | 20 to $30 \mathrm{MHz} \pm 1 \mathrm{~Hz}$ | $>-7 \mathrm{dBm}$ |
| 64 | 360 to $450 \mathrm{MHz} \pm 1 \mathrm{~Hz}$ | $>+10 \mathrm{dBm}$ |
| 65 | $100 \mathrm{MHz} \pm 1 \mathrm{~Hz}$ | $>+10 \mathrm{dBm}$ |

*To achieve the $\pm 1 \mathrm{~Hz}$ tolerance, the System mainframe and the frequency counter must share a common timebase.
a. Check the low frequency RF inputs to the RF Section. Set the mainframe Line switch to standby (STBY), disconnect the interconnect cable from the multi-pin connector P6 on the RF Section rear panel. Return the mainframe line switch to the ON position. Check the frequencies and levels according to the tables with a spectrum analyzer and a frequency counter. If the levels and frequencies are all correct, the same signals must be checked to ensure continuity into the Frequency Extension Module. Refer to the Troubleshooting Information in the extension module manual. Otherwise, proceed to step b.
b. Check the RF signal levels and frequencies at their assembly outputs in the mainframe. Refer to the Section VIII of the mainframe manual. Check the 20 MHz FM/CW signal at A4J7, 100 MHz at A4J8, and 360 to 450 MHz at A4J12. The 20 to 30 MHz signal is found on the A 2 Mother Board Assembly which is located directly beneath the A4 Assembly. The tables of frequencies and levels still apply for these measurements. If any of the outputs are incorrect, refer to the appropriate troubleshooting information relating to the circuits which generate that particular frequency in Section VIII of the mainframe manual.
c. If all inputs (step b) are correct and if any of the J6 outputs (step a) were incorrect, check continuity of the interconnections to the RF Section. In the case of problems with the 20 MHz CW/FM signal, refer to the Modulation Section manual. If all inputs (step b) are correct and the J6 outputs to the RF Section were not checked, proceed to the extension module for further troubleshooting information.

Center Frequency Versus
Frequency of 360 to 450 MHz Signal

| Center Frequency <br> Readout | Actual Frequency <br> (350 to $\mathbf{4 5 0} \mathrm{MHz}$ Signal) |
| :--- | :---: |
| 0.00 GHz | 450 MHz |
| 0.01 | 440 |
| 0.02 | 430 |
| 0.03 | 420 |
| 0.04 | 410 |
| 0.05 | 400 |
| 0.06 | 390 |
| 0.07 | 380 |
| 0.08 | 370 |
| 0.09 | 360 |
| 0.10 | 450 |

## NOTE

If the problem is not in the RF Section or interconnections, the information in the Frequency Extension Module will determine if the problem is in the digit 8,9 , and 10 logic control inputs from the mainframe or the frequency controlled circuits in the extension module.

## Modulation Problems

Amplitude, Frequency, and Phase Modulation. Defects in modulation circuits can usually be classed as either accuracy or distortion problems. In each case it must be determined if the problem is in the Modulation Section, RF Section, or (in FM mode only), the Frequency Extension Module.
a. System modulation accuracy is checked by performing the appropriate performance test in Section IV of the modulation section manual. If the results indicate a problem exists, check the modulation section output with a full scale level setting. The table indicates where to make the measurement, the type of measurement, and the normal signal measured. A coaxial cable from the 11672A Service Kit (11672-60008) connects to the appropriate signal on J6 (the mainframe-to-RF Section interconnect jack).

If the measured signal shows the output modulation signal is incorrect, perform the appropriate adjustment in Section $V$ of the modulation section manual. If the signal cannot be properly adjusted, refer to Section VIII of the modulation section

## SERVICE SHEET 1 (Cont'd)

Assembly (refer to the last foldout for its location). If either the signal or dc voltage is not present, check continuity back to the Auxiliary Section. If necessary, refer to the HP

Model 86631B Operating Note and troubleshoot the Auxiliary Section. Otherwise, refer to Service Sheet 1 for more troubleshooting information.

Center Frequency Versus Frequency of 20 to 30 MHz Signal

| Center <br> Frequency <br> Readout <br> $(\mathrm{MHz})$ | Exact <br> Frequency <br> (20 to 30 MHz <br> Signal)(MHz) | Center <br> Frequency <br> Readout <br> $(\mathbf{M H z})$ | Exact <br> Frequency <br> $(20$ to 30 MHz <br> Signal) (MHz) | Center <br> Frequency <br> Readout <br> $(\mathrm{MHz})$ | Exact <br> Frequency <br> $(\mathbf{2 0}$ to 30 MHz <br> Signal) (MHz) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 0.000000 | 30.000000 | 0.000400 | 29.999600 | 0.080000 | 29.920000 |
| 0.000001 | 29.999999 | 0.000500 | 29.999500 | 0.090000 | 29.910000 |
| 0.000002 | 29.999998 | 0.000600 | 29.999400 | 0.100000 | 29.900000 |
| 0.000003 | 29.999997 | 0.000700 | 29.999300 | 0.200000 | 29.800000 |
| 0.000004 | 29.999996 | 0.000800 | 29.999200 | 0.300000 | 29.700000 |
| 0.000005 | 29.999995 | 0.000900 | 29.999100 | 0.400000 | 29.600000 |
| 0.000006 | 29.999994 | 0.001000 | 29.999000 | 0.500000 | 29.500000 |
| 0.000007 | 29.999993 | 0.002000 | 29.998000 | 0.600000 | 29.400000 |
| 0.000008 | 29.999992 | 0.003000 | 29.997000 | 0.700000 | 29.300000 |
| 0.000009 | 29.999991 | 0.004000 | 29.996000 | 0.800000 | 29.200000 |
| 0.000010 | 29.999990 | 0.005000 | 29.995000 | 0.900000 | 29.100000 |
| 0.000020 | 29.999980 | 0.006000 | 29.994000 | 1.000000 | 29.000000 |
| 0.000030 | 29.999970 | 0.007000 | 29.993000 | 2.000000 | 28.000000 |
| 0.000040 | 29.999960 | 0.008000 | 19.992000 | 3.000000 | 27.000000 |
| 0.000050 | 29.999950 | 0.009000 | 29.991000 | 4.000000 | 26.000000 |
| 0.000060 | 29.999940 | 0.010000 | 29.990000 | 5.000000 | 25.000000 |
| 0.000070 | 29.999930 | 0.020000 | 29.980000 | 6.000000 | 24.000000 |
| 0.000080 | 29.999920 | 0.030000 | 29.970000 | 7.000000 | 23.000000 |
| 0.000090 | 29.999910 | 0.040000 | 29.960000 | 8.000000 | 22.000000 |
| 0.000100 | 29.999900 | 0.050000 | 29.950000 | 9.000000 | 21.000000 |
| 0.000200 | 29.999800 | 0.060000 | 29.940000 | 9.999999 | 20.000001 |
| 0.000300 | 29.999700 | 0.070000 | 29.930000 |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |

## SERVICE SHEET 1 (Cont'd)

manual for further troubleshooting information. Once the adjustment is satisfactorily made, recheck the system modulation accuracy.

If the system accuracy is still incorrect, perform the appropriate adjustment procedure in Section V of the RF Section manual. If this adjustment cannot satisfactorily be made, refer to the troubleshooting information of Service Sheet 2.
b. Modulation distortion problems are verified by performing the appropriate distortion test determined by the modulation type (refer to Section IV of this manual). If the test indicates an excessive distortion level is present in the RF output signal, the source of the distortion must be determined.

Measurements of the signals from the Modulation Section may be made at the J6 connector after the RF Section has been removed. For each modulation type, the output distortion is typically $<1 \%$. If the distortion is excessive, refer to the troubleshooting information in Section VIII of the modulation section manual. Otherwise, perform the appropriate adjustment procedures in Section V of the RF Section manual.

Recheck the performance test in Section IV of this manual. If necessary, refer to the troubleshooting information in Service Sheet 2.

Unusual Phase Modulation Level Problems. If phase modulation level accuracy varies excessively with system center frequency, check the gain tracking inputs (Digit 8) for the correct logic level for the selected center frequency. If the logic levels are incorrect, refer to the mainframe manual for further troubleshooting information. If the inputs are correct, refer to Service Sheet 2.

Pulse Modulation Problems. Pulse Modulation of the Signal Generator System is accomplished by using the HP Model 86631B Auxiliary Section and an external pulse generator.
a. Set the Auxiliary Section external modulation control to Pulse. To the input jack couple an external pulse of -10 Vpk with the "pulse off" voltage set to 0 Vdc .
b. Measure the voltage on the test point labeled PULSE (located on a circuit board at the right side rear of the plug-in). This voltage should be about +5 Vdc . Also, check the pulse input from the white-green cable where it enters the A2 Assembly. If either the signal or dc voltage is not present, check continuity back to the Auxiliary Section. If necessary, refer to the HP Model 86631B Operating Note and troubleshoot the Auxiliary Section. Otherwise, refer to Service Sheet 2 for more troubleshooting information.

Modulation Accuracy Test Levels

| Modulation Type | Measurement Location | Signal Parameter Measured | Measured Signal (for Full Scale) Modulation Level |
| :---: | :---: | :---: | :---: |
| Amplitude ${ }^{1}$ | A12 Assembly at test point labeled AM. (Right side rear of plug-in or J6 pin 55. | AC Voltage | 2.8 Vp-p (1.0 Vrms) at 1 kHz rate |
| Frequency ${ }^{2}$ | $\text { Pin } 62 \text { of J6 }$ | Frequency <br> Deviation (peak) | $20 \mathrm{MHz} \pm 10 \mathrm{kHz}$ <br> ( $\mathrm{FM} \times 1$ range) at 1 kHz rate |
| Phase ${ }^{1}$ | A16 Assembly input (white/ green cable) or J6 pin 59 | AC Voltage | 4.2 Vp-p (1.5 Vrms) at 1 kHz rate |
| ${ }^{1}$ If the input is very low or non-existant, verify that continuity of the input exists back to the modulation section. If continuity exists, refer to Service Sheet 2. <br> ${ }^{2}$ If no frequency modulation of the RF Signal is present or if the RF signal is incorrect only in the FM mode, refer to Section VIII of the modulation section manual for further troubleshooting information. |  |  |  |
|  |  |  |  |

## RF SECTION TEST POINTS

RIGHT SIDE VIEW


## LEFT SIDE VIEW



Figure 8-4. System Test Point Locations


Figure 8-6. System Troubleshooting Block Diagram

## SERVICE SHEET 2 (Cont'd)

passed from port 2 to port 3 (J3) where it is again reflected from the phase modulator with additional phase shift approximately equal to that which occurred at port 2. The signal is passed from port 3 to port 4 (J4) and through the 3 dB attenuator to the 4 GHz Amplifier Assembly.

In other than option 002 instruments (no phase modulation circuits), the LO signal is coupled directly from FL1 to the A8 4.0 GHz Amplifier Assembly.

## Mixer Section

The mixer output is derived from mixing the LO and RF inputs. The phase modulated or cw LO signal is amplified and coupled to the Mixer Assembly. The RF signal passes through the Isolator ( 20 dB reverse isolation) to the Modulator Assembly where it encounters variable series attenuation. The series attenuation is controlled by the bias signal from the ALC feedback loop. The modulator's RF output signal is coupled directly to the Mixer where it is mixed with the LO signal. The difference frequency output is coupled to the Amplifier/ Detector Assembly.

## Amplifier/Detector Section

The RF input to the Amplifier/Detector Assembly is amplified 41 dB . This high level signal is coupled to the 10 dB Step Attenuator.

The Amplifier/Detector Assembly also contains the RF Detector circuit. It produces a dc voltage which is proportional to the peak RF output voltage. This signal, which is amplified to drive the front panel meter and the AM Gain compensation circuits in the Reference Assembly, is also coupled to the ALC Amplifier Assembly

## ALC Section

Reference Assembly. In the Local Mode, the RF output level is set by the front panel controls. The unmodulated RF level to the 10 dB Attenuator is set by the ALC loop's de bias voltage which, in turn, is controlled by the VERNIER setting.

In the AM mode the modulation drive signal is superimposed on the reference voltage. The average amplitude of the RF output is dependent on the average dc level (which is equal to the dc reference voltage) while the instantaneous RF output voltage and its rate of change (modulation characteristics) are dependent on the superimposed modulation drive signal.

In the remote mode, the entire system responds to programmed inputs; the front panel controls of all instruments are inhibited. In the RF Section, the reference output is coupled to the ALC Assembly through the 1 dB Step Attenuator. Therefore, the vernier function is controlled by the 1 dB Step Attenuator.

ALC Amplifier. The ALC Amplifier compares the Detector Amplifier Assembly output to the Reference Assembly output. Any change

## SERVICE SHEET 2 (Cont'd)

in the detected RF level or the reference level is immediately reflected at the ALC assembly output. This output is coupled to the A5 Modulator Assembly as the Modulator Bias signal. Because the RF input to the 10 dB Step Attenuator is directly proportional to the Modulator RF output level (which is controlled by the Modulation Bias Signal), the ALC feedback loop is completed.

Pulse Modulation Circuits. During Pulse Modulation, the ALC loop is opened at the ALC Amplifier output. With no signal input, a positive bias voltage to the A5 Modulation Assembly causes the RF signal output to be at least 40 dB down ( 60 dB down at center frequencies $\geqslant 1300 \mathrm{MHz}$ ) from the "on-condition". A -10 Vdc pulse biases the RF "on".

## Attenuation Section

The Attenuator Section operates identically in local and remote modes. The inputs from the Logic Section (10D, 20D, 40D, and 80D) select the level of attenuation of the RF signal passing through the 10 dB Step Attenuator.

## TROUBLESHOOTING

It is assumed that a problem has been isolated to the RF Section as a result of using the System Troubleshooting Guide found in Section VIII of the HP Model 8660 -series mainframe Operating and Service Manual and the information entitled System Troubleshooting on Service Sheet 1. Troubleshoot the RF Section using the test equipment, information, and procedures which follow.
Test Equipment
Spectrum Analyzer
HP 8555A/8552B/140T
Oscilloscope.
HP 180C/1801A/1821A
Digital Voltmeter.
HP 34740A/34702A
Test 1. It is good practice to first check the power supply inputs to the RF Section and at the same time, it may help to check AM, Pulse ID or any other inputs which relate to the problem. The inputs may be checked at the A12 Assembly test points on the right-side rear of this plug-in.
A12 Assembly Test Points

| -10 V | $-10.0 \pm 0.1 \mathrm{Vdc}$ |
| :--- | :---: |
| +20 V | $+20.0 \pm 0.1 \mathrm{Vdc}$ |
| $-20 \mathrm{~V}_{\mu}$ | $-21.0 \pm 0.2 \mathrm{Vdc}$ |
| $+20 \mathrm{~V}_{\mu}$ | $+20.0 \pm 0.2 \mathrm{Vdc}$ |

Test 2. If the problem is related to incorrect output level, proceed to Test 3. If it is a unique type problem such as amplitude modulation, noise, etc., refer to the following items for additional troubleshooting hints.
a. Frequency Problems. Normally not caused by RF Section. Refer to Section VIII of the mainframe manual or Service Sheet 1 of this manual.

## SERVICE SHEET 2 (Cont'd)

in the detected RF level or the reference level is immediately reflected at the ALC assembly output. This output is coupled to the A5 Modulator Assembly as the Modulator Bias signal. Because the RF input to the 10 dB Step Attenuator is directly proportional to the Modulator RF output level (which is controlled by the Modulation Bias Signal), the ALC feedback loop is completed.
Pulse Modulation Circuits. During Pulse Modulation, the ALC loop is opened at the ALC Amplifier output. With no signal input, a positive bias voltage to the A5 Modulation Assembly causes the RF signal output to be at least 40 dB down ( 60 dB down at center frequencies $\geqslant 1300 \mathrm{MHz}$ ) from the "on-condition". A -10 Vdc pulse biases the RF "on".

## Attenuation Section

The Attenuator Section operates identically in local and remote modes. The inputs from the Logic Section (10D, 20D, 40D, and 80 D ) select the level of attenuation of the RF signal passing through the 10 dB Step Attenuator.

## troubleshooting

It is assumed that a problem has been isolated to the RF Section as a result of using the System Troubleshooting Guide found in Section VIII of the HP Model 8660 -series mainframe Operating and Service Manual and the information entitled System Troubleshooting on Service Sheet 1. Troubleshoot the RF Section using the test equipment, information, and procedures which follow.
Test Equipment
Spectrum Analyzer
HP 8555A/8552B/140T
Oscilloscope.
HP 180C/1801A/1821
Digital Voltmeter
HP 34740A/34702A
Test 1. It is good practice to first check the power supply inputs to the RF Section and at the same time, it may help to check AM, Pulse ID or any other inputs which relate to the problem. The inputs may be checked at the A12 Assembly test points on the right-side rear of this plug-in.

| A12 Assembly Test Points |  |
| :--- | :---: |
| -10 V | $-10.0 \pm 0.1 \mathrm{Vdc}$ |
| +20 V | $+20.0 \pm 0.1 \mathrm{Vdc}$ |
| $-20 \mathrm{~V}_{\mu}$ | $-21.0 \pm 0.2 \mathrm{Vdc}$ |
| $+20 \mathrm{~V}_{\mu}$ | $+20.0 \pm 0.2 \mathrm{Vdc}$ |

Test 2. If the problem is related to incorrect output level, proceed to Test 3. If it is a unique type problem such as amplitude modulation, noise, etc., refer to the following items for additional troubleshooting hints.
a. Frequency Problems. Normally not caused by RF Section. Refer to Section VIII of the mainframe manual or Service Sheet 1 of this manual.

## SERVICE SHEET 2 (Cont'd)

b. Spurious Signals. May be isolated by checking for signal at various locations in the RF Section. Setting the A4S1 switch to Test may help to isolate the problem to the RF circuitry or ALC loop.
c. Noise. Generally, noise originates in Frequency Extension Module or the A15 20 MHz Amplifier Assembly.
d. Amplitude Modulation. Verify that the AM signal reaches the A10 Reference Assembly.

If amplitude modulation level changes with an RF level change check the RF Section front panel meter reading versus measured RF OUTPUT level. If the panel meter reading is correct, refer to Service Sheet 7 (check AM Gain input and related circuits). Otherwise, check the meter driver amplifier and related components shown on Service Sheet 6.

Distortion problems may be caused by defective components associated with the ALC Bandwidth Input. Check the logic inputs from Service Sheet 3. Then refer to Service Sheet 3, 6, or 7 .

If the amplitude modulation level differs from the level shown, perform the related adjustment procedures in Section V to see if the error is corrected. Be sure the fault isn't in the Modulation Section. An input of 1.0 Vrms to the A10 Reference Assembly should equal 100\% AM level.
e. Phase Modulation. The output of the A16 Phase Modulator Driver Assembly is a distorted sinusoidal waveform of approximately $7.5 \mathrm{~V}_{\mathrm{p}-\mathrm{p}}$ for a full scale Modulation Section meter indication. If the output is incorrect, check the output of the cable, W12, to determine if W12 or A16 is defective. The output should be 1.5 Vrms. If the output of the A16 assembly is correct, either W14 or A17 is defective. Refer to the paragraph entitled LO Signal Circuits Repair procedure in Section VIII of this manual for disassembly and repair procedures.
Phase modulation distortion problems in the RF section will generally be caused by the A16 Phase Modulator Driver Assembly or the A17 Phase Modulator Assembly. Refer to Service Sheet 5.

## NOTE

Excessive incidental AM during phase modulation may be caused by incorrect operation of the 50 MHz Low Pass Filter. Check the control input and the RF output level of the filter. Refer to Service Sheet 4.
f. Pulse Modulation. Problems may be isolated by checking Pulse In and Pulse ID inputs. Also, check continuity from A5 Modulator Assembly inputs from Auxiliary Section.
g. Incorrect Front Panel Meter Reading. Refer to Test 3.

Test 3. If the RF output level is incorrect by more than 1 or 2 dB , proceed to Test 4 . Otherwise check the 10 H input to the A10

## SERVICE SHEET 2 (Cont'd)

Assembly related components. Refer to Service Sheet 3 if the input is incorrect. If necessary refer to Section V and perform the RF

Output Level and 1 dB Step Attenuator Adjustment procedures. If the Adjustments cannot be done or do not correct the tracking across the VERNIER range, check the Meter Driver and meter ircuitry, and the AM Gain circuits. Refer to Service Sheets 6 and 7 espectively. Also check the circuits in the A4 Assembly which are influenced by the 10 H input.

Test 4. Proceed to Test 5 if the RF output level is higher than normal. The RF outputs listed in each step of this test (4) are lower than normal. The voltages enclosed in parenthesis are Modulator Bias Signal ranges. They indicate that the ALC loop is (1) holding the RF output low, (2) is trying to increase the RF output or (3) that a output low, (2) is trying to increase the RF output or (3) that a block diagram for the normal range of Modulator Bias Signal levels.
a. The RF output is low but the ALC loop is trying to increase the level ( $\geqslant-3 \mathrm{Vdc}$ ). Check the RF outputs of FL1, A7, and A6 to isolate the problem to Service Sheets 4 (for other than option 002 instruments), Service Sheets 4 or 5 (option 002 instruments only), or Service Sheet 6 respectively

If the output of FL1 is correct and the output of A7 is incorrect, the problem may be on either Service Sheets 4 or 5 in option 002 instruments. In this case, refer to the LO Signal Circuits Repair procedure and the Troubleshooting Block Diagram to isolate the problem to an assembly or cable.

On other than option 002 instruments, if the output of A7 is defective, refer to Service Sheet 4.

Each of these assemblies and circuits, if defective, must be replaced as a unit with the exception of A7. If A7 is defective, refer to Service Sheet 4 for further troubleshooting information.
b. The RF output is low and the ALC loop is holding the Modulator Bias Signal level low ( $\geqslant+10 \mathrm{Vdc}$ ). First, check the A10 Reference Assembly output with the VERNIER control set to the cw and ccw position with A4S1 in the Normal position. If the output is abnormal, refer to the troubleshooting information on Service Sheet 7. A normal output indicates the defect is either on the A3 ALC Assembly, or the A4 Detector Amplifier Assembly.

Set the A4S1 switch to the Test position. If the Modulator Bias Signal exhibits the same response as shown in the following table, the problem is probably in the A4 Detector Amplifier Assembly. (Check the Detector Signal input at A4 pin 11.)

## SERVICE SHEET 2 (Contd)

Modulator Bias Signal

| A4S1 <br> Switch | Vernier Control Settings |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  | CW |  | ccW |  |
|  | $\mathbf{9 0 4}$ | $\mathbf{9 0 7}$ | $\mathbf{9 0 4}$ | $\mathbf{9 0 7}$ |
| Normal | +0.2 Vdc | +0.4 Vdc | +1 to <br> +11 Vdc | +0.8 Vdc |
| Test | -4 | Vdc | -3.0 Vdc | +0.3 Vdc |

c. The Modulator Bias Signal is at a quiescent level but is lower (more positive) than normal. Check the A10 Reference Assembly output level. If the output is lower (more positive than normal), check the $1 \mathrm{~A}, 2 \mathrm{~A}, 4 \mathrm{~A}$, and 8 A inputs to the A 10 Assembly (remote mode only). If they are correct or the instrument is in local mode, refer to Service Sheet 7. If the remote inputs are incorrect or the problem is associated with the 10 dB Step Attenutor, refer to troubleshooting information on Service Sheet 3. Otherwise, check the detector output and reference at A4 pin 10 and 11. Refer to Service Sheet 6.

Test 5. The RF outputs listed in each step of this test are higher than normal. The voltages enclosed in parentheses are Modulator Bias Signal ranges. They indicate that the ALC loop (1) is holding the RF output high, (2) is trying to decrease the output level or (3) that a quiescent level, although incorrect, has been reached. Refer to the block diagram for normal values of Modulator Bias Signal.
a. High RF output level; the ALC has increased the level ( $\geqslant-3 \mathrm{Vdc}$ ). Check the A10 Reference Assembly output. If the response to VERNIER control settings is abnormal, refer to Service Sheet 7 and troubleshoot the A10 Assambly. If the response is normal, set the A 4 S 1 switch to test. If the Modulator Bias Signal responds to the VERNIER control settings as indicated by the table of Test 4 b , check that the detector output responds properly to the increased RF signal level (check A4 pin 10 and 11) and refer to Service Sheet 6. Otherwise, turn to Service Sheet 7 and continue troubleshooting.
b. High RF output level; the ALC is trying to decrease the level $(\geqslant+10 \mathrm{Vdc})$. The A 5 Modulator Assembly or associated circuitry is probably defecfive (refer to Service Sheet 4).
c. The Modulator Bias Signal is at a quiescent level but higher (more negative) than normal. Check the A10 Reference Assembly output. If the A10 output is more negative than normal, check the $1 \mathrm{~A}, 2 \mathrm{~A}, 4 \mathrm{~A}$, and 8 A inputs to the A 10 assembly (remote mode only). If the A10 outputs are correct or the instrument is in local mode, refer to Service sheet 7. If the remote inputs are incorrect or the problem is associated with the 10 dB Step Attenuator, refer to the troubleshooting information on Service Sheet 3. Otherwise, check that the detector output responds properly to the increased RF signal level (check A4 pins 10 and 11). Refer to Service Sheet 6.


Figure 8-7. RF Section Simplified Block Diagram



## SERVICE SHEET 3

## NOTE

When a malfunction occurs, refer to Section VIII of the HP Model 8660-series mainframe Operating and Service Manual to begin troubleshooting (System Troubleshooting Guide). Then, if that information indicates possible problems in the RF Section, refer to the System Troubleshooting information in Service Sheet 1. This information may be used to isolate the defect to the RF Section, another plug-in, or the mainframe. If the problem is in this plug-in, return to Service Sheet 2 for further troubleshooting information.

## LOGIC CIRCUITRY <br> PRINCIPLES OF OPERATION

## General

In this instrument, logic inputs to the analog circuits control functions such as 1 dB and 10 dB steps of attenuation of the RF output signal. These inputs also influence the phase modulation signal.

In the remote mode, all control signals are external to the RF Section. In the local mode, the OUTPUT RANGE switch selects the range by using a binary coded hexadecimal output with an extro overrange line. Also, the VERNIER control is analog in nature.

## Filter Control Assembly

The ninth and tenth digit BCD inputs from the mainframe ( 100 MHz and 1 GHz ) are used to control the A7A5 50 MHz Low Pass Filter.

The decoder circuit determines when the frequency output from the A7 Assembly is greater than 100 MHz . The A7A5 50 MHz High Pass Filter is switched on which effectively traps any low frequency phase modulation drive signals which would otherwise be amplified and passed on to the RF output.

## Logic Assembly

Local operation of the 10 dB Step Attenuator is selected by a logic high on the LCL/RMT input. Thus, control of the 10 dB Step Attenuator by the inputs from the front panel OUTPUT RANGE switch is enabled while the remote inputs are inhibited

In Remote mode, a logic low in the LCL/RMT inputs inhibits front panel control and enables data information flow from the mainframe to the Logic Assembly. The ATTN CLK controls the actual data input on the PI-1, PI-2, PI-4, and PI-8 lines. The OUTPUTS to the 10 dB Step Attenuator (10L, 20L, 40L, 80L), the over-range (10H), and the 1 dB Step Attenuator outputs ( $1 \mathrm{~A}, 2 \mathrm{~A}, 4 \mathrm{~A}, 8 \mathrm{~A}$ ) are all controlled by external programming in the Remote Mode. A safety

## SERVICE SHEET 3 (Cont'd)

feature, the RESET input, sets the 10 dB Step Attenuator to the maximum attenuation when the Remote mode is first initiated.

## Attenuator Driver Assembly

The inputs from the Logic Assembly (10L, 20L, 40L, and 80L) switch the equivalent attenuator drive outputs (10D, 20D , 40D, and 80D). These outputs provide the higher voltages and current needed to drive the relays in the A13 Attenuator Assembly.

## TROUBLESHOOTING

Malfunctions in the RF Section which appear to be a logic problem may be an analog circuit problem. Refer to Service Sheet 2 to begin troubleshooting and return here if necessary.

## Test Equipment

Oscilloscope . . . . . . . . . . . HP $180 \mathrm{C} / 1801 \mathrm{~A} / 1821 \mathrm{~A}$
Digital Voltmeter . . . . . . . . . . . HP $34740 \mathrm{~A} / 34702 \mathrm{~A}$
Logic Probe . . . . . . . . . . . . HP 10525 T

## General

If the malfunction is isolated to the logic circuits, the related inputs must be checked before an attempt is made to troubleshoot the individual circuit assemblies. The control levels are fixed and may change when a new center frequency or mode of operation (local or remote) has been selected. The clocked or momentary inputs, PI (plug-in), ATTN CLK, and RESET occur only at the instant the center frequency or mode change is made.

## Local Mode

In local mode, the inputs mentioned in the preceding paragraph are not used. The $1 \mathrm{~A}, 2 \mathrm{~A}, 4 \mathrm{~A}$, and 8 A outputs are also not used. (VERNIER control replaces the 1 dB step attenuator.) Check the 1 F , $2 \mathrm{~F}, 4 \mathrm{~F}, 8 \mathrm{~F}$, and 1 H inputs against the levels shown for the S 1 switch in the diagram.

## Remote Mode

Check the Logic Assembly PI, ATTN CLK, and RESET inputs. Switch to the local mode and then back to the remote mode of operation. Verify that the attenuation level has reset to 150 dB by checking the $10 \mathrm{~L}, 20 \mathrm{~L}, 40 \mathrm{~L}, 80 \mathrm{~L}$, and 10 H outputs $[10 \mathrm{H}$ and 10 L should be low ( $<+0.8 \mathrm{Vdc}$ ) while 20L, 40L, and 80L outputs should be high ( $>+2.0 \mathrm{Vdc}$ )]. The momentary low input ( 0 Vdc as compared to the normal +5 Vdc ) may be observed on an oscilloscope at the instant of switching. A logic probe may also be used to verify the presence of the reset pulse. To verify that the PI (data) and ATTN CLK inputs are correct, program the information shown in the table at the

## Main Troubleshooting Block Diagram SERVICE SHEET 2

## SERVICE SHEET 3 (Cont'd)

bottom of this page. Check each output for the correct level. If any level is incorrect, the presence of the data and/or the ATTN CLK inputs may be checked at the instant of programming with an oscilloscope or logic probe.

## NOTE

If the problem is isolated between the inputs and outputs of an assembly, refer to the appropriate Service Sheet as indicated on the diagram.

Check the A9 Attenuator Driver Assembly outputs against the inputs.

| Programmed Attenuation | RF Output Level | Outputs |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{gathered} 1 \mathrm{~A} \\ 1 \mathrm{~dB} \end{gathered}$ | $\begin{gathered} 2 \mathrm{~A} \\ 2 \mathrm{~dB} \end{gathered}$ | $\begin{gathered} 4 \mathrm{~A} \\ 4 \mathrm{~dB} \end{gathered}$ | $\begin{gathered} 8 \mathrm{~A} \\ 8 \mathrm{~dB} \end{gathered}$ | $\begin{gathered} 10 \mathrm{~L} \\ 10 \mathrm{~dB} \end{gathered}$ | $\begin{gathered} 20 \mathrm{~L} \\ 20 \mathrm{~dB} \end{gathered}$ | $\begin{gathered} 40 \mathrm{~L} \\ 40 \mathrm{~dB} \end{gathered}$ | $\begin{gathered} 80 \mathrm{~L} \\ 80 \mathrm{~dB} \end{gathered}$ | $\begin{gathered} 10 \mathrm{H} \\ 10 \mathrm{~dB} \end{gathered}$ |
| 7 dB | $+6 \mathrm{dBm}$ | H | H | H | L | L | L | L | L | L |
| 87 dB | -74 dBm | H | H | H | L | H | H | H | L | H |
| 98 dB | -85 dBm | L | L | L | H | L | L | L | H | H |

$\mathrm{H}=$ Attenuation $=>+2.0 \mathrm{Vdc}$
$\mathrm{L}=$ No Attenuation $=<+0.8 \mathrm{Vdc}$


## SERVICE SHEET 4

## NOTE

When a malfunction occurs, refer to Section VIII of the HP Model 8660-series mainframe Operating and Service Manual to begin troubleshooting (System Troubleshooting Guide). Then, if that information indicates possible problems in the RF Section, refer to the Systems Troubleshooting information (Service Sheet 1). This information may be used to isolate the defect to the RF Section, another plug-in, or the mainframe. If the problem is in this plug-in, refer to Service Sheet 2 for further troubleshooting information.

## MIXER SECTION

## PRINCIPLES OF OPERATION

## General

The LO signal is filtered and amplified to drive the mixer. The RF signal is leveled and may be amplitude modulated at the A5 Modulator Assembly. After passing through the Modulator, the RF Signal and LO Signal are mixed; the difference frequency is passed on for further amplification.

## 4 GHz Bandpass Filter/Amplifier

Unwanted sidebands are eliminated from the LO signal by passing the signal through a bandpass filter. In option 002 instruments, the LO signal is coupled to the phase modulation circuits before being input to the 4 GHz Amplifier. The signal is amplified to a high level to drive the mixer.

## Isolator

The 3.95 to 2.75 GHz RF Signal is passed through the Isolator to the Modulator Assembly. Reverse signal attenuation is about 20 dB .

## Modulator Assembly

The effect of the PIN diode Modulator on the RF Signal is that of a variable attenuator. The level of attenuation and therefore the modulator RF output is dependent on the Modulator Bias Signal dc level.

The PIN Diode Modulator has dynamic attenuation range of $>50 \mathrm{~dB}$. A more positive modulator bias signal turns off the series diodes while the shunt diodes are forward biased. The shunt diodes and the series resistor form a voltage divider which attenuates the RF Signal. As the bias voltage goes more negative, the impedance of the shunt diodes increases while the series diodes impedance decreases. Therefore, the RF signal attenuation decreases. The shunt diodes effectively control the attenuation from 12 to $>50 \mathrm{~dB}$ down while the series diodes are effective only to about 12 dB down.

## SERVICE SHEET 4 (Cont'd)

The RF output level at the front panel jack is directly proportional to the Modulator Assembly RF output. The Modulator Bias Signal controls the A5 Modulator Assembly output and is dependent on an error voltage derived from comparing the $\& F$ detector output to the reference dc level.

## Mixer Assembly

The RF Signal is passed through a low pass filter and attenuator before leaving the Modulator Assembly. Then the RF signal is mixed with the LO signal in the Mixer Assembly, the mixer output passes through a low pass filter, and the difference frequency is a $1-1300 \mathrm{MHz}$ phase-locked signal with frequency resolution of 1 Hz .

At center frequencies $\geqslant 100 \mathrm{MHz}$, the High Pass Filter Control input from the A20 Filter Control Assembly to the A7A5 Assembly causes the mixer output to pass through the 50 MHz High Pass Filter. This reduces incidental AM distortion generated by the phase modulated signal in the balanced mixer.

## TROUBLESHOOTING

It is assumed that the troubleshooting information on Service Sheet 1 was used to isolate a circuit defect to the assemblies or cables shown on the accompanying diagram. Troubleshoot the Mixer Section by using the test equipment and procedures given below.

## NOTE

In Option 002 instruments, a defect cannot easily be isolated to circuits
shown on this schematic diagram. Refer to Service Sheet 2 and the repair procedure entitled LO Signal Circuits Repair.

Test Equipment

| Spectrum Analyzer | . | HP 8555A/8552B/140T |  |
| :--- | :--- | :--- | :--- |
| Power Meter. . | . | HP 435A/8481A |  |
| Digital Voltmeter . | . | HP 34740A/34702A |  |
| Service Kit |  |  | HP 11672A |

Service Kit HP 11672A

Test 1. Check the power supply inputs to the A8 Assembly $(+20 \mathrm{~V}$ and $-10 \mathrm{~V})$. If correct, proceed to Test 2. Otherwise check for continuity of interconnections to mainframe or an A8 Assembly defect.

## CAUTION

Slight but repeated bending of semi-rigid coaxial cables will damage them very quickly. Bend the cables as little as possible. If necessary, loosen the assembly to release the cable.

Test 2. If the RF power output is greater than normal (refer to the schematic), the A5 Modulator Assembly is probably defective. If the power output is less than normal, checking the difference assembly outputs will quickly isolate the defective assembly or cable.

## NOTE

Defects in the A15 20 MHz Amplifier Assembly and RF interconnections from mainframe to Frequency Extension Module (through the RF Section) normally will be isolated by using the Systems Troubleshooting (Service Sheet 1).


Figure 8-10. A 7 Mixer Assembly's subAssembly and Component Locations



Figure 8-11. Mixer Section Schematic Diagram

## SERVICE SHEET 5

## NOTE

When a malfunction occurs, refer to Section VIII of the HP Model 8660-series mainframe Operating and Service Manual to begin troubleshooting (System Troubleshooting Guide). Then, if that information indicates possible problems in the RF Section, refer to the Systems Troubleshooting information in Service Sheet 1. This information may be used to isolate the defect to the RF Section, another plug-in, or the mainframe. If the problem is in this plug-in, refer to Service Sheet 2 for further troubleshooting information.

## PRINCIPLES OF OPERATION

## General

The phase modulation drive signal from the modulation section is coupled to the A16 Phase Modulation Driver Assembly. The signal is predistorted and the overall gain is varied (with respect to LO predistorted and the overall gate frequency characteristics of the frequency) to compensate for the frequency characteristics of the
A17 Phase Modulator Assembly. The signal is amplified before being A17 Phase Modulator Assembly. Th
connected to the phase modulator.
With minimal loss, the LO signal passes through the A19 3.9-4.1 Isolator Assembly to the A18 Circulator Assembly. The signal passes from port 1 to port 2 and on to the phase modulator.
In the phase modulator, the varactor diode, A17A1CR1 reactively terminates the stripline transmission line which reflects the LO signal. Changing the bias voltage applied to the varactor diode changes the termination reactance. This causes the reflected signal to shift in phase with respect to the incident input signal.
The reflected LO signal travels back down the transmission line and through port 2 to port 3, where it again enters the phase modulator. The same sequence of events occurs. Thus, the phase shift of the LO signal reflected back to port 3 is approximately doubled.

The phase modulated LO signal continues from port 3 to port 4, through the AT2 3 dB Attenuator and on to the A8 4 GHz Amplifier Assembly. Due to the high input reflection coefficient of the 4 GHz Assembly. Due to the high input reflection coefficient of the 4 GHz
Amplifier, a large portion of the signal is reflected back to port 4, through to port 1, and on to the Frequency Extension Module. The AT2 3 dB Attenuator and A19 3.9-4.1 GHz Isolator Assemblies reduce the level of the reflected signal to prevent it from interfering with the extension module VCO circuits.

## A16 Phase Modulator Driver Assembly

The cable capacitance of W12 and A16L1 form a low pass filter which improves the frequency response of the input modulation drive signal up to 10 MHz .

Diode Shaping Network. The shaping network introduces third order distortion to higher level input signals (when the A16CR2

## SERVICE SHEET 5 (Cont'd)

diode begins to conduct). The level of distortion is adjusted to compensate for the third order distortion inherent in the phase modulator transfer characteristics. The demodulated third order phase modulation sidebands are minimized by adjusting A16R1, the Third Harmonic Adjust control.

Gain Tracking. Gain tracking of the modulation drive signal is introduced to compensate for the phase modulator's inability to produce a constant phase deviation at different LO frequencies. At higher LO frequencies, the phase modulator sensitivity is lower and a higher level modulation drive signal is required to produce the same phase deviation. At system center frequencies where digit $8(10 \mathrm{MHz}$ steps) is zero (LO frequency is 3.95 MHz ), logic lows ( $<+0.8 \mathrm{Vdc}$ ) are coupled to the U2 inverters. The outputs are high ( $>+2.0 \mathrm{Vdc}$ ) which bias the U1 transistors on, and current flows from the modulation drive signal path through A16R7, R9, R11 and R13 to ground. This causes maximum attenuation of the drive signal. Conversely, at center frequencies where digit 8 is other than zero, logic highs are input to one or more of the inverters and the low outputs bias the transistors off. This cuts off current flow through the shunt resistors and reduces the attenuation. Minimum attenuation occurs when digit 8 is nine (digits $8-1$ and 8-8 are high) and current flow through A16R7 and R13 is cut off.

The Gain control, A16R2, sets the absolute modulation signal level with minimum attenuation (at 4.05 GHz ). The Gain Tracking control adjusts the rate of change of attenuation with respect to the LO frequency by setting the modulation signal level with minimum attenuation (at 3.95 GHz ).
J-FET Shaping Circuit. The J-FET A16Q1 is biased so it introduces second order distortion to the modulation drive signal. This distortion compensates for the second order distortion in the transfer characteristics of the phase modulator. The transfer characteristics of the phase modulator are varied by changing the dc output from the A16 Assembly. The Second Harmonic Adjust Control A16R3 sets the second order distortion level of A16Q1 (by controlling the drain current flow) and the dc output from A16 (which is proportional to current flow) and the dc output from A16 (which is proportional to
the A16Q1 drain voltage). The distortion level is minimized the A16Q1 drain voltage). The distortion level is minimized
by demodulating the system's RF output and nulling the second order phase modulation sidebands.
Modulation Driver Amplifier. The J-FET output is coupled to the discrete component operational amplifier made up of A16Q4 through Q10 and their associated components. The input is coupled directly to the inverting input A16Q4. Any noise generated in the reference supply circuit, A16Q11, is coupled equally to both inverting and non-inverting inputs and is therefore cancelled. The amplifier's high frequency rolloff is set by A16C8. The gain of approximately 10 is determined primarily by A16R $36,1000 \Omega$, and A16R25, $100 \Omega$.

Reference Supply. A16Q5, the non-inverting input to the Modula-

## SERVICE SHEET 5 (Cont'd)

tion Driver Amplifier, is a PNP transistor and thus is biased opposite to NPN A16Q11. Any change in voltage across the base emitter junction of A16Q11 due to temperature is compensated for, by an equal and opposite change across the base-emitter junction of A16Q5. Therefore, the voltage at the emitter of A16Q5 is temperature stabilized. In similar fashion, the voltage on the emitter of A16Q4 is also temperature stabilized. The voltage at the base of A16Q7 is temperature stabilized except for the influence of A16CR3. The temperature related change in current flow through this diode appears as a change in voltage on A16Q7 and is amplified by the Modulation Driver Amplifier. This voltage change compensates for temperature related change in sensitivity of the varactor diodes in the A17 Assembly.

## A17 Phase Modulator Assembly

In the phase modulator, the LO signal passes through the blocking capacitors and down the stripline transmission lines to the varactor diode terminations, A17A1CR1 and CR2. The amount of phase shift between the incident and reflected signals is determined by the varactor capacitance.
The varactor capacitance is voltage variable. The dc bias input sets the quiescent phase shift. The instantaneous phase shift is dependent on the sum of the dc bias and the ac modulation drive signal input to the phase modulator.

## TROUBLESHOOTING

It is assumed that the troubleshooting information on Service Sheet 2 and the LO Signal Circuits Repair procedure were used to isolate the defect to one of the Assemblies. Troubleshoot the A16 or A17 Assemblies by using the following procedure.

## Test Equipment

Digital Voltmeter . . . . . . . . . . HP $34740 \mathrm{~A} / 34702 \mathrm{~A}$
Oscilloscope . . . . . . . . . . . . HP $180 \mathrm{C} / 1801 \mathrm{~A} / 1821 \mathrm{~A}$

Oscilloscope . HP 180C/1801A/1821
Spectrum Analyzer HP 180C/1801A/1821A

A16 and A17 Assembly circuit malfunctions usually result in incorrect or no modulation drive, incorrect gain tracking, or unwanted distortion. Distortion may be due to misadjusted or defective components.

Set the system's modulation section switches for $\emptyset \mathrm{M}$ mode, internal

> A1 Modulator Filter Assembly A2 ALC Mother Board Assembly A5 Modulator Assembly A7 Mixer Assembly A GHz Amplifier Assembly A12 Logic Mother Board Assembly A15 20 MHz Amplifier Assembly A20 Filter Control Assembly AT1 Isolator FL1 4 GHz Band Pass Filter SERVICE SHEET 4

## SERVICE SHEET 5 (Cont'd)

diode begins to conduct). The level of distortion is adjusted to compensate for the third order distortion inherent in the phase modulator transfer characteristics. The demodulated third order phase modulation sidebands are minimized by adjusting A16R1, the Third Harmonic Adjust control.

Gain Tracking. Gain tracking of the modulation drive signal is introduced to compensate for the phase modulator's inability to produce a constant phase deviation at different LO frequencies. At higher LO frequencies, the phase modulator sensitivity is lower and a higher level modulation drive signal is required to produce the same phase deviation. At system center frequencies where digit $8(10 \mathrm{MHz}$ steps) is zero (LO frequency is 3.95 MHz ), logic lows ( $<+0.8 \mathrm{Vdc}$ ) are coupled to the U2 inverters. The outputs are high $(>+2.0 \mathrm{Vdc})$ which bias the U1 transistors on, and current flows from the modulation drive signal path through A16R7, R9, R11 and R13 to ground. This causes maximum attenuation of the drive signal. Conversely, at center frequencies where digit 8 is other than zero, logic highs are input to one or more of the inverters and the low outputs bias the transistors off. This cuts off current flow through the shunt resistors and reduces the attenuation. Minimum attenuation occurs when digit 8 is nine (digits $8-1$ and $8-8$ are high) and current flow through A16R7 and R13 is cut off.

The Gain control, A16R2, sets the absolute modulation signal level with minimum attenuation (at 4.05 GHz ). The Gain Tracking control adjusts the rate of change of attenuation with respect to the LO frequency by setting the modulation signal level with minimum attenuation (at 3.95 GHz ).

J-FET Shaping Circuit. The J-FET A16Q1 is biased so it introduces second order distortion to the modulation drive signal. This distortion compensates for the second order distortion in the transfer characteristics of the phase modulator. The transfer characteristics of the phase modulator are varied by changing the dc output from the A16 Assembly. The Second Harmonic Adjust Control A16R3 sets the second order distortion level of A16Q1 (by controlling the drain current flow) and the dc output from A16 (which is proportional to the A16Q1 drain voltage). The distortion level is minimized by demodulating the system's RF output and nulling the second order phase modulation sidebands.

Modulation Driver Amplifier. The J-FET output is coupled to the discrete component operational amplifier made up of A16Q4 through Q10 and their associated components. The input is coupled directly to the inverting input A16Q4. Any noise generated in the reference supply circuit, A16Q11, is coupled equally to both inverting and non-inverting inputs and is therefore cancelled. The amplifier's high frequency rolloff is set by A16C8. The gain of approximately 10 is determined primarily by A16R $36,1000 \Omega$, and A16R25, $100 \Omega$.

Reference Supply. A16Q5, the non-inverting input to the Modula-

## SERVICE SHEET 5 (Cont'd)

tion Driver Amplifier, is a PNP transistor and thus is biased opposite to NPN A16Q11. Any change in voltage across the base emitter junction of A16Q11 due to temperature is compensated for, by an equal and opposite change across the base-emitter junction of A16Q5. Therefore, the voltage at the emitter of A16Q5 is temperature stabilized. In similar fashion, the voltage on the emitter of A16Q4 is also temperature stabilized. The voltage at the base of A16Q7 is temperature stabilized except for the influence of A16CR3. The temperature related change in current flow through this diode appears as a change in voltage on A16Q7 and is amplified by the Modulation Driver Amplifier. This voltage change compensates for temperature related change in sensitivity of the varactor diodes in the A17 Assembly.

## A17 Phase Modulator Assembly

In the phase modulator, the LO signal passes through the blocking capacitors and down the stripline transmission lines to the varactor diode terminations, A17A1CR1 and CR2. The amount of phase shift between the incident and reflected signals is determined by the varactor capacitance.

The varactor capacitance is voltage variable. The dc bias input sets the quiescent phase shift. The instantaneous phase shift is dependent on the sum of the dc bias and the ac modulation drive signal input to the phase modulator.

## TROUBLESHOOTING

It is assumed that the troubleshooting information on Service Sheet 2 and the LO Signal Circuits Repair procedure were used to isolate the defect to one of the Assemblies. Troubleshoot the A16 or A17 Assemblies by using the following procedure.

## Test Equipment

Digital Voltmeter . . . . . . . . . . HP $34740 \mathrm{~A} / 34702 \mathrm{~A}$
Oscilloscope . . . . . . . . . . . . HP $180 \mathrm{C} / 1801 \mathrm{~A} / 1821 \mathrm{~A}$
Spectrum Analyzer . . . . . . . . .

A16 and A17 Assembly circuit malfunctions usually result in incorrect or no modulation drive, incorrect gain tracking, or unwanted distortion. Distortion may be due to misadjusted or defective components.

Set the system's modulation section switches for $\emptyset \mathrm{M}$ mode, internal
A1 Modulator Filter Assembly
A2 ALC Mother Board Assembly
A5 Modulator Assembly
A7 Mixer Assembly
A8 4 GHz Amplifier Assembly
A12 Logic Mother Board Assembly
A15 20 MHz Amplifier Assembly
A20 Filter Control Assembly
AT1 Isolator
FL1 4 GHz Band Pass Filter
SERVICE SHEET 4

## SERVICE SHEET 5 (Cont'd)

1 kHz source, and adjust the modulation level control for a full scale meter reading $\left(100^{\circ}\right.$ or $200^{\circ}$ ). Refer to the schematics for the typical voltages.

## A16 Assembly

Test 1. Check the power supply inputs to the A16 Assembly.

Test 2. Check the peak-to-peak ac voltages at the various points as indicated on the schematic. If all seem to be correct, refer to Section $V$ and readjust the phase modulation circuits.

Test 3. If the output of the discrete component operational amplifier is defective, check the dc output and compare it to the dc inputs. If the change in dc output voltage from normal does not
follow the change in input dc voltage, the problem is probably in Q4 through Q10 or their associated components. For example, the output voltage is more positive than normal.

Test 4. Check the dc voltages on A16Q1 through Q3 and Q11.

Test 5. If the gain tracking is incorrect, check and compare the inputs and outputs of A16U1 and U2.

## A17 Assembly

Test 1. Remove the assembly cover. Check for the presence of the dc bias and ac voltage on the varactor diodes, A17CR1 and CR2.

Test 2. Verify that A 17 C 1 and C 3 are not defective.


Figure 8-12. A16 Phase Modulator Driver Assembly Component and Test Point Locations


Figure 8-13. A17 Phase Modulator Assembly Component Locations

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## NOTE

When a malfunction occurs, refer to Section VIII of the Model 8660-series mainframe Operating and Service Manual to begin troubleshooting (Systems Troubleshooting Guide). Then, if that information indicates possible problems in the RF Section, refer to the Systems troubleshooting information in Service Sheet 1 in this manual. This information may be used to isolate the defect to the $R F$ Section, another plug-in, or the mainframe. If the problem is in this plug-in, refer to Service Sheet 2 for further troubleshooting information.

## PRINCIPLES OF OPERATION

## Amplifier/Detector Assembly

The A6 1-1300 MHz Amplifier Assembly contains an RF Preamplifier and Amplifier which are separated by an elliptic low pass filter The combined RF gain is approximately 41 dB .

The RF Detector provides a dc output which is proportional to the peak RF output from the A6 Assembly. The dc level charges the 68 pF capacitor which is coupled to the A3 Detector Amplifier Assembly.

## Detector Amplifier Assembly

A small bias current through the RF and Reference Diodes is set by the A4R13 Detector Bias Adjustment for maximum detector sensitivity. Beyond the initial bias current, any further change in current flow is due to temperature variations. Because the two diodes are located in the same thermal environment, an increase in current flow through the RF Detector Diode is matched by an equal increase in current flow through the Reference Diode. The Reference Diode current is coupled to the non-inverting input of the Detector Amplifier (a discrete operational amplifier comprised of A4Q3, A4Q2, A4Q1 and associated components) while the RF Detector Diode output is coupled to the inverting output. Therefore, any change in current flow due to a change in temperature is cancelled in the operational ampli fier which leaves the output level dependent only on the peak RF output from the A6 Assembly.

At center frequenices of $<10 \mathrm{MHz}$, the Code 1 input causes A4Q4 to be biased on which connects A4C3 parallel with the 68 pF capacito found in the Amplifier/Detector Assembly.

## SERVICE SHEET 6 (Cont'd)

As the center frequency is decreased, the detector output needs to be retained for a longer period of time so the leveling circuits respond to the average RF level rather than the instantaneous level.

In output ranges of $\leqslant 0 \mathrm{dBm}$, the Detector Amplifier is coupled directly to the A3 ALC Amplifier Assembly. The output is compared to a dc reference level and an error signal results which is coupled to the A5 Modulator Assembly to complete the ALC loop. When OUTPUT RANGE switch is set to +10 dBm , the 10 H logic input goes high ( $\approx+5 \mathrm{Vdc}$ ) and turns A4Q5 off. Relay A4K1 opens and the dc voltage is attenuated 10 dB by A4R19, A4R20, A4R21, and resistors on the A3 assembly. The RF output signal increases 10 dB which brings the dc output to the A3 ALC Amplifier input back to the quiescent level present before switching to the +10 dBm range.

Amplifier A4U1 functions as an active low pass filter because of A4R23 and A4C5 which are connected in the feedback loop. The amplifier drives the meter and provides a compensating dc level which varies the AM drive input to keep the amplifier modulation level constant with change in RF output level (VERNIER Control setting).

## TROUBLESHOOTING

It is assumed that the troubleshooting information on Service Sheet 2 was used to isolate a circuit defect to the assemblies shown on the accompanying diagram. Troubleshoot the Amplifier/Detector and Detector Amplifier Assemblies by using the test equipment and procedures given below.

Test Equipment
Spectrum Analyzer . . HP 8555A/8552B/140T
Digital Voltmeter . . . HP 34740A/34702A
Test 1. If the circuit problem is associated with the meter and AM Gain output rather than the RF Output level, proceed to Test 2. Check the Detector Output, Detector Amplifier Output A4TP1, and output to ALC Amplifier to see if they are tracking the RF output level. Set A4S1 to the test position. If the RF Amplifier output remains low, the A6 assembly or an associated cable is probably defective. If the RF output increases, measure the detector and A4TP1 and A4TP2 voltages. If the detector output doesn't respond properly, the A6 assembly or an associated input component on the A4 assembly, is probably defective. If the detector output increases but the A4TP1 voltage doesn't go more negative, the Detector Amplifier or an associated component is probably defective.

If the RF output level is incorrect only in the +10 dBm range or is correct only in the +10 dBm range, and the 10 H input is correct for all ranges, the 10 dB attenuator, the relay (A4K1), or an associated component is probably defective

Test 2. Monitor the RF output with a Spectrum Analyzer. If the modulation level changes with respect to the RF carrier amplitude (change the VERNIER control to three or four different settings), A4U1 or associated components are probably defective. Otherwise, the meter control is misadjusted or the meter connections or an associated component is probably defective.

A16 Phase Modulator Driver Assembly
A17 Phase Modulator Assembly
A17 Phase Modulator Assembly
A18 Circulator Assembly
A19 3.9-4.1 GHz Isolator Assembly
AT2 3 dB Attenuator
SERVICE SHEET 5 (Option 002)


Figure 8-15. A4 Detector Amplifier Assembly Component and Test Point Locations


## SERVICE SHEET 7

## NOTE

When a malfunction occurs, refer to Section VIII of the Model 8660-series mainframe manual to begin troubleshooting (Systems Troubleshooting Guide). If the inforSection, refer to the Systems Troubleshooting inforSection, refer to the Systems Troubleshooting infor may be used to isolate the defect to the RF Section another plug-in or the mainframe If the problem is in this plug-in refer to Service Sheet 2 for further troublethis plug-in, refer to Service Sheet 2 for further troubleshooting information.

## PRINCIPLES OF OPERATION

## General

The detected signal output from the A4 Detector Amplifier Assembly is coupled into the A3 ALC Amplifier Assembly where it is compared to the reference input. Any difference in dc input levels causes an error output signal (i.e., a change from the loop quiescent state) at the difference amplifier output A3TP1. The error signal is coupled through the Gain-Shaping Amplifier to the A5 Modulator Assembly which controls the RF output level. The change in RF output level is reflected in a dc level change at the input to the dc amplifier. The change serves to balance the original error output signal at A3TP1.

## A10 Reference Assembly

The Reference Assembly output is coupled to the ALC circuit where it is compared to the Detector Amplifier output. An error signal is generated which causes the RF signal to follow the reference dc level or, in AM mode, a low frequency ac signal which is superimposed on the reference dc output.
A reference dc level is established by A10VR1. This dc level is coupled to the inverting input of A10U1 where (in the +10 dBm range only) a small RF Detector diode linearity compensation current is added from the 10 H input through resistor A10R14. The output of A10U1 passes through a remotely VERNIER Control. This provides fine adjustment of the reference output, i.e., the RF Output level over a 10 dB range.

The Amplitude Modulation drive signal is input at the non-inverting input of The Amplitude Modulation drive signal is input at the non-inverting input of
A10U1. The AM Gain input is a dc compensation signal which effects the A10U1. The AM Gain input is a dc compensation signal which effects the
level of the AM drive input. As the VERNIER control is rotated cw, the dc level of the AM drive input. As the VERNIER control is rotated cw, the dc
level goes more negative which increases the RF Output level. At the same level goes more negative which increases the RF Output level. At the same
time a negative change of the AM Gain compensation increases the time a negative change of the AM Gain compensation increases the
modulation drive signal attenuation of the AM drive signal input to A10U1. The resulting increase in modulation drive signal at the output of A10U1 tends to keep the percentage modulation level constant with change in RF output level.

In the remote mode, the front panel VERNIER control of the RF output level is inhibited and the 1 dB step attenuator assumes "vernier" control over

## SERVICE SHEET 7 (Cont'd)

a 10 dB range. A logic low ( $<+0.8 \mathrm{Vdc}$ ) on the LCL/RMT input lines biases A10Q10 off, which opens the contacts of A10K6 and isolates the VERNIER control. At the same time, A10Q1 is biased on which closes the contacts of A10K5 and enables the 1 dB step attenuator. With no attenuation (RF vernier maximum) the $1 \mathrm{~A}, 2 \mathrm{~A}, 4 \mathrm{~A}$, and 8 A inputs are all logic lows. Programmed attenuation levels will cause a logic high to appear on the appropriate input. For example, if 1 dB of attenuation is programmed (equivalent to a +2 dB front panel meter reading), a voltage of +5 Vdc will be found on A12XA10 pin J. This voltage biases A10Q9 off. Relay A10K1 opens which causes the reference to be attenuated through A10R21 and A10R22 (which is coupled to ground through A10Q8). When A10Q9 is turned off, bias current is supplied through A10R20 from the negative supply to turn A10Q8 on. Transistor A10Q8 is baised through the base-to-collector junction instead of the normal base-to-emitter junction.

Each step of attenuation is operated in the same manner. The values of the resistors in the voltage divider stick are weighted for greater attenuation of voltage output to the ALC circuits as the programmed attenuation levels are increased.

## ALC Amplifier Assembly

The Detector Amplifier output, which is proportional to the RF output level, is compared to the Reference output in the ALC Amplifier Assembly.
The detector signal is coupled to the non-inverting input of the discrete operational amplifier (A3Q10, A3Q9, and associated components) while the reference input is coupled to the inverting input. Under normal operating conditions a change in reference input causes an error output signal at A3TP1. This signal passes through the Gain-Shaping Amplifier where it is coupled to the A5 Modulator Assembly. This change in Modulation Bias Signal causes the RF output to change. The change is reflected in the Detector Amplifier input to the ALC loop. This change serves to balance the error signal at A3TP1 and a new quiescent voltage is established. In a similar fashion, the change in RF output loading or a change in signal level input from the Frequency Extension Module is compensated for in the ALC loop For example, a decrease in output level due to increased loading causes positive change in the Detector Amplifier output to the ALC Amplifier. T
resultant change in Modulator Bias Signal is negative which decreases the A5 Modulator Assembly Attenuation of the RF Signal and subsequently increases the RF output level.

At $<10 \mathrm{MHz}$, a logic high ( $>+2.0 \mathrm{Vdc}$ ) at the Code 1 input biases A3Q5 off, A3Q2 is biased off, and A3Q3 is turned on. A3C6 is now coupled to ground which effectively reduces the bandwidth of the ALC loop. This occurs so the ALC loop does not respond to individual cyclic variations in the RF Signa but rather to the relatively long term peak output of the RF Detector.

## Gain-Shaping Amplifie

The Gain-Shaping Amplifier is a discrete operational amplifier made up of A3Q7, A3Q8, A3Q6, A3Q11, A3Q4, and their associated components. Th gain-shaping component is A3CR1. When A3CR1 is reverse biased the gain

## SERVICE SHEET 7 (Cont'd)

of the amplifier is unity (times one). As the instantaneous base voltage of A3Q6 is increased (by either positive dc level or positive excursions of an AM drive signal) A3CR1 is forward biased and the amplifier gain is dependent on the ratio of A3R3 and the effective resistance of A3CR1. This variable gain is used to compensate for the non-linearity of the Modulator Assembly's input voltage to RF attenuation transfer function.

## Pulse Modulation

In the Pulse Modulation mode (HP Model 86631B Auxiliary Section is used in place of a Modulation Section), a PULSE ID logic high ( $\approx+5 \mathrm{Vdc}$ ) turn A3Q1 off which opens A3K1 and thus opens the ALC loop. At the sam time, the PULSE ID input biases A2Q1 on, closes A2K1, and connects the Pulse In through A2R9, A2C2, and A2VR1 to the A5 Modulator Assembly Withouth a pulse input, the positive bias through A2R8 biases the Modulato for maximum attenuation and reduces the power output to a minimum ( $>40 \mathrm{~dB}$ down). A -10 Vdc input pulse is required to cause the Moduator to exhibit minimum attenuation to the RF Signal

## TROUBLESHOOTING

It is assumed that the Troubleshooting information on Service Sheet 1 was used to isolate a circuit defect to the assemblies shown on the accompanyin diagram. Troubleshoot the Reference and ALC Amplifier Assemblies and pulse modulation circuits by using the test equipment and procedures given

Test Equipment
Digital Voltmeter
HP 34740A/34702A
Test 1. Check the power supply inputs to the A3 and A10 assemblies at A2XA3 pin $5(+20 \mathrm{~V})$, pin $3(+5 \mathrm{~V})$, and pin $8(-10 \mathrm{~V})$ and A12XA10 pin D $(+20 \mathrm{~V})$, pin $\mathrm{C}(+5 \mathrm{~V})$, and pin $5(-10 \mathrm{~V})$. If the voltages are correct proceed to Test 2. If incorrect, check the continuity of the inputs from the A12 Assembly.

Test 2. Check the Reference Output at P14 Pin E. If the output level is incorrect for the extreme settings of the vernier control or 1 dB Step Attenuator settings, (see schematic for levels) proceed to Test 3. If the output is correct, set A4S1 and check the levels at A3TP1 with th VERNIER (or 1 dB Step Attenuator) set to one extreme and then the other If the output levels are normal, the Gain-Shaping Amplifier or the Modulator Bias Signal resistors are probably defective. Also check the Pulse ID input and the relays. Otherwise, the Difference Amplifier is probably defective.

## SERVICE SHEET 7 (Cont’d)

Test 3. Check the reference diode A10VR1, and Reference Amplifier A10U1 and their associated components. If the unit responds only to the local control or responds to remote control and not to the VERNIER, check the LCL/RMT input and the relay. If the reference output is incorrect in remote mode only, check the 1 dB Step Attenuator,
relays, transistor switches, and other associated components. Small changes in RF Output level may be traceable to defective components coupled to the 10 H input. If it was found that the amplitude modulation level varies with RF Output level, check the components associated with the AM Gain input. If the AM drive signal is reaching the RF Section, verify that it is reaching the A10 Assembly circuitry. Determine which component or part is defective, repair or replace it.


Figure 8-17. A3 ALC Amplifier Assembly Component and Test Point Locations


Figure 8-18. A10 Reference Assembly Component Locations


Figure 8-19. A2 ALC Mother Board Assembly Component Locations



## SERVICE SHEET 8

## NOTE

When a malfunction occurs, refer to Section VIII of the Model 8660-series mainframe manual to begin troubleshooting (System Troubleshooting Guide). If the information then indicates possible problems in the $R F$ Section, refer to the Systems Troubleshooting information in Service Sheet 1 of this manual. This information may be used to isolate the defect to the RF Section, another plugin or the mainframe. If the problem is in this plug-in refer to Service Sheet 2 for further troubleshooting information before returning here.

## PRINCIPLES OF OPERATION

Logic high inputs ( $>+2.0 \mathrm{Vdc}$ ) from the A11 Logic Board Assembly will cause the driver transistors to supply current to switch the appropriate attenuator section in the A13 Attenuator Assembly. A logic low ( $<+0.8 \mathrm{Vdc}$ ) switches out the attenuation. For example, if 10 dB of attenuation is desired, the 10L input goes high, A9Q23 is biased on; A9Q19 is also biased on and supplies driving current to switch A13K1. The relay arms all drop down into the lower position. The RF Signal flow is now through attenuator section AT1 ( 10 dB ). The two lower relay arms provide a latching function for the relay. This means that until a drive current of the correct polarity is input to the A9 Attenuator Drive Assembly, the relay is latched in its present state. Also, no current flows after the switching has been completed. A9R4 and A9VR1 provide the proper bias level for the input transistors so they will respond correctly to the inputs.

A9CR1 provides protection for the driver transistor from the inductive switching transient which occurs when the drive current through the relay is turned off. A9Q21 limits the current flow through A9Q19.

The other attenuator sections function the same way as the 10 dB section. However, the 80 dB section actually uses two 40 dB sections in parallel.

## TROUBLESHOOTING

It is assumed that the troubleshooting information on Service Sheet 2 was used to isolate a circuit defect to the assemblies shown on the accompanying diagram. Troubleshoot the Attenuator and Attenuator Driver Assemblies using the test equipment and procedures given below.

## Test Equipment

Digital Voltmeter . . . . . HP 34740A/34702A
The malfunction may be isolated to either the A13 or A9 Assemblies by measuring the $10 \mathrm{D}, 20 \mathrm{D}$, 40 D , and 80 D control lines and determining if they are correct. If the problem is in the A13 Assembly DO NOT attempt to repair it. It is not a field repairable unit.

DC voltage checks should be sufficient to quickly isolate a defective component in the A9 Assembly. Remember, current flows through the drive transistors only until latching of the relays in A 13 is completed.


Figure 8-21. A9 Attenuator Driver Assembly Component Locations


## NOTE

When a malfunction occurs, refer to Section VIII of the Model 8660-series mainframe manual to begin troubleshooting (Systems Troubleshooting Guide). If the information then indicates possible problems in the RF Section, refer to the Systems Troubleshooting information in Service Sheet 1 of this manual. This information is used to isolate the defect to the RF Section, another plug-in, or the
mainframe. If the problem is in this plug-in, refer to Service Sheet 2 for preliminary troubleshooting information.

## PRINCIPLES OF OPERATION

## Local (Front panel) Control

The front panel OUTPUT RANGE switch provides a binary coded hexadecimal input ( $1 \mathrm{~F}, 2 \mathrm{~F}, 4 \mathrm{~F}, 8 \mathrm{~F}$ ) and an over range input ( 1 H ) to the A11 Assembly in the local mode. The LCL/RMT input is logic high ( $>+1.3 \mathrm{Vdc}$ ) which causes the switch inputs to be gated directly to the outputs to the attenuator driver circuits and the 10 H output. The following table shows the logic states of the inputs from the OUTPUT RANGE switch S1. The input signals are all active highs (attenuation) as are the outputs.

Local Inputs to A11 Logic Assembly

| OUTPUT <br> RANGE <br> Switch <br> Setting | Binary Coded Hexadecimal Input* |  |  |  | Over-Range Input* |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 8F | 4F | 2F | 1F | 1H |
| +10 | L | L | L | L | L |
| 0 | L | L | L | L | H |
| -10 | L | L | L | H | H |
| -20 | L | L | H | L | H |
| -30 | L | L | H | H | H |
| -40 | L | H | L | L | H |
| $-50$ | L | H | L | H | H |
| -60 | L | H | H | L | H |
| -70 | L | H | H | H | H |
| -80 | H | L | L | L | H |
| -90 | H | L | L | H | H |
| -100 | H | L | H | L | H |
| -110 | H | L | H | H | H |
| -120 | H | H | L | L | H |
| -130 | H | H | L | H | H |
| -140 | H | H | H | L | H |

## SERVICE SHEET 9 (Cont'd

## Remote Operation

In the remote mode, 3 digits of BCD attenuation information are locked into the A11 Assembly Shift Registers from the System mainframe. On the ATTN CLK input, a series of 10 pulses are received at pin K. These pulses are coupled to the trigger (T) input to the shift registers. The data input, which is synchronized with the pulses, contain no usable information for the first seven pulses On the eighth pulse, units information is clocked into the left-handed column of registers with logic highs indicating data ones and lows indicating zeroes. On the ninth pulse, the units information is shifted to the center column of registers while ten information is entered into the left hand registers. On the tenth pulse, the units word is shifted into and stored in the right hand column, the tens information in the center registers, and the hundreds information in the left registers.

The BCD information stored in the units registers is coupled to the 1 dB Step Attenuator on the A10 Reference Assembly. (In loca mode these outputs are not used. The VERNIER control is used for fine control of output level.)

The other two digits of BCD information are coupled to the BCD-to-Binary Decoder. The binary tens line actually bypasses the decoder because it expresses odd or even value in either the BCD or binary coded hexadecimal in BCD . The second digt ( 20 , 40 and 8 ) and BCD-to-Binary Decoder in a 20,40 , and 80 binary format. Wh ne the the $10,20,40$ and 80 cod signa are invert and coupled to a four input nand ate. The nand gate (over-ange) output is low only with zero input attenuation (i.e all the BCD-to-Binary Decoder output line are low). The over-range level is coupled to A11 U5C and hero to the 10 H output It is also coupled to the Full Adder long with the $10,20,40$ and 80 lines. The inputs to the adde are connected so a value of 10 is subtracted from the input with the Over-Range inactive (high); when the over-range line is low the output follows the input directly. The following tables express the assembly inputs and outputs, the BCD-to-Binary converter inputs and outputs, and the Full Adder inputs and outputs. In each cas a level of $>+2.0 \mathrm{Vdc}$ is a logic high and $<+0.8 \mathrm{Vdc}$ is logic low.

SERVICE SHEET 9 (Cont'd)

| Programmed Attenuation Input |  |  |  |  |  | OUTPUT <br> RANGE <br> Decimal <br> (dBm) | Logic Assembly Output |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Decimal } \\ (\mathrm{dB}) \end{gathered}$ | 2-Digit BCD |  |  |  |  |  |  |  |  |  | Overrange |
|  | 100 | 80 | 40 | 20 | 10 |  | 80L | 40L | 20 L | 10 L | 10H |
| 0 | L | L | L | L | L | +10 | L | L | L | L | H |
| 10 | L | L | L | L | H | 0 | L | L | L | L | L |
| 20 | L | L | L | H | L | -10 | L | L | L | H | L |
| 30 | L | L | L | H | H | -20 | L | L | H | L | L |
| 40 | L | L | H | L | L | -30 | L | L | H | H | L |
| 50 | L | L | H | L | H | -40 | L | H | L | L | L |
| 60 | L | L | H | H | L | -50 | L | H | L | H | L |
| 70 | L | L | H | H | H | -60 | L | H | H | L | L |
| 80 | L | H | L | L | L | -70 | L | H | H | H | L |
| 90 | L | H | L | L | H | -80 | H | L | L | L | L |
| 100 | H | L | L | L | L | -90 | H | L | L | H | L |
| 110 | H | L | L | L | H | -100 | H | L | H | L | L |
| 120 | H | L | L | H | L | -110 | H | L | H | H | L |
| 130 | H | L | L | H | H | -120 | H | H | L | L | L |
| 140 | H | L | H | L | L | -130 | H | H | L | H | L |
| 150 | H | L | H | L | H | -140 | H | H | H | L | L |

BCD-To-Binary Converter

| Input |  |  |  |  | Output |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1 0 0}$ | $\mathbf{8 0}$ | $\mathbf{4 0}$ | $\mathbf{2 0}$ | $\mathbf{8 0}$ | $\mathbf{4 0}$ | $\mathbf{2 0}$ |  |
| L | L | L | L | L | L | L |  |
| L | L | L | H | L | L | H |  |
| L | L | H | L | L | H | L |  |
| L | L | H | H | L | H | H |  |
| L | H | L | L | H | L | L |  |
| H | L | L | L | H | L | H |  |
| H | L | L | H | H | H | L |  |
| H | L | H | L | H | H | H |  |

SERVICE SHEET 9 (Cont'd)
Full Adder

| Inputs |  |  |  |  | Outputs |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{A}_{4}$ | $\mathrm{A}_{3}$ | $\mathrm{A}_{2}$ | $\mathrm{A}_{1}$ | $\mathrm{C}_{0}, \mathrm{~B}_{2}, \mathrm{~B}_{3}, \mathrm{~B}_{4}$ | ${ }^{\Sigma} 4$ | $\Sigma_{3}$ | $\Sigma_{2}$ | $\Sigma_{1}$ |
| 80 | 40 | 20 | 10 | Over-range | 80 | 40 | 20 | 10 |
| L | L | L | L | L | L | L | L | L |
| L | L | L | H | H | L | L | L | L |
| L | L | H | L | H | L | L | L | H |
| L | L | H | H | H | L | L | H | L |
| L | H | L | L | H | L | L | H | H |
| L | H | L | H | H | L | H | L | L |
| L | H | H | L | H | L | H | L | H |
| L | H | H | H | H | L | H | H | L |
| H | L | L | L | H | L | H | H | H |
| H | L | L | H | H | H | L | L | L |
| H | L | H | L | H | H | L | L | H |
| H | L | H | H | H | H | L | H | L |
| H | H | L | L | H | H | L | H | H |
| H | H | L | H | H | H | H | L | L |
| H | H | H | L | H | H | H | L | H |
| H | H | H | H | H | H | H | H | L |

## Local Remote Multiplex

The LCL/RMT input is a logic low in the remote mode. This enables the gates which are connected to the remote attenuation inputs (Full Adder and Over-range) so the remote signals drive the 10 dB Step Attenuator. At the same time logic inputs from the OUTPUT RANGE switch are inhibited.

## TROUBLESHOOTING

It is assumed that the troubleshooting information on Service Sheet 1 was used to isolate a circuit defect to the assembly shown on the accompanying diagram. Troubleshoot the Logic Assembly by using the test equipment and procedures given below.

## Test Equipment

Digital Voltmeter . . . HP 34740A/34702A
If the problem is evident only in the local mode of operation, check the OUTPUT RANGE switch, continuity of the connections to the A11 assembly, and the Local/Remote Multiplexer. Refer to
the table showing the OUTPUT RANGE switch output. If the defect is evident only in the remote mode of operation, check the shift registers, the BCD-to-Binary Decoder, the Full Adder, and the Local/Remote Multiplexer for proper operation. Use the tables showing inputs versus outputs as a tool to isolate the defective component.

If the defect is evident in both the Local and Remote modes, the Local/Remote Multiplexer or an associated component is probably defective.

## NOTE

If the inputs and outputs of the A11 Logic Assembly are correct, check the 10 dB step attenuator (Service Sheet 6) in all ranges, the 10 dB attenuator in the A4 Detector Amplifier Assembly, and the $1 d B$ Step Attenuator in the A10 Reference Assembly (also the 10 H inputs and associated components). Also, check the $1 d B$ and $10 d B$ Step Attenuator outputs with attenuation inputs of $1,2,4$, and $8 d B$ and 10, 20, 40, and 80 dB .


Figure 8-23. A11 Logic Assembly Component Locations


## UAAD 7 OP VIEW

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| S1 |
| :--- |
| All ASSY |
| Cl |
| LI |
| $\mathrm{U1}-10$ |



## DISASSEMBLY AND INTERCONNECTION PROCEDURES

## CAUTION

Before removing the RF Section plug-in from the mainframe, remove the main (Mains) voltage by disconnecting the power cable from the power outlet.

## RF Section Plug-in Removal

a. Release the latch below the front panel OUTPUT jack.
b. Pull the latch out while rotating it to the left until it is perpendicular to the front panel. This separates the mating plug and jack (plug-in to mainframe).
c. Grasp the latch and pull the plug-in straight out from mainframe.

## Plug-in Cover Removal

a. Remove the 16 Pozidriv screws from both covers.
b. Loosen the 4 screws which hold the teflon/aluminum plug-in guide in place.
c. Remove the covers and set them aside.
d. If necessary, remove the plug-in guides by removing the screws.

Interconnection of RF Section to Mainframe for Troubleshooting Purposes
After the RF Section is removed from the mainframe and its covers have been removed, the RF Section must be reconnected to the mainframe with interconnecting extender cables before troubleshooting can begin.

## CAUTION

With the mainframe top cover removed, power is supplied to the system during troubleshooting. Energy available at many points may constitute a shock hazard.
a. Remove the mainframe top cover. First remove the 4 Pozidriv screws; then slide the cover back and off the mainframe siderails.

## NOTE

The interconnect cables and adapters are parts found in the HP 11672A Service Kit. They may all be ordered in the kit or as individual pieces. Refer to the 11672A Operating Note for a pictorial cross reference.

## DISASSEMBLY AND INTERCONNECTION PROCEDURES (Cont'd)

b. Make connection from J6 (mainframe) to P6 (RF Section rear panel) with the 11672-60001 multi-pin interconnect cable.

## CAUTION

To avoid contact with the line voltage, remove the line (main) power cable from the power outlet before removing or connecting cables to the Frequency Extension Module.
c. Connect the 1250-1236 adapter to the 11672-60005 gray coaxial cable. Insert the adapter into P2 (on the RF Section rear panel above the multipin connector).
d. Remove the gray-blue cable from the jack on the rear side of the Frequency Extension Module. Connect the gray coaxial cable to the extension module jack.
e. Take the 11672-60004 red coaxial cable and connect it to P1 (RF Section rear panel below the multi-pin connector).
f. Disconnect the gray cable from the other extension module output jack. Connect the red coaxial cable to the jack.
g. Reconnect the mainframe line (Main) power cable to the power outlet and set the mainframe line switch to ON.

Table 8-2. Assemblies, Chassis Mounted Parts, and Adjustable Component Locations (1 of 2)

| Reference Designator | Service Sheet | Figures |  |
| :--- | :--- | :--- | :--- |
| A1 Assembly | 2,4 | - | Remarks |
| A2 Assembly | $2,4,7$ | $8-19,25$ | Circuit board, mounted on aluminum deck <br> opposite the A5 Assembly. |
| mound A16 plug into connectors |  |  |  |
| A3 Assembly |  |  |  |
| A3R4, ADJ, LIN | 2,7 | $8-17,25$ |  |
| A4 Assembly | 7 | $8-17,25$ | $8-25$, Top View |
| A4R13 AD, DET BIAS | 2,6 | $8-15,25$ |  |
| A4R26 ADJ, MTR BIAS | 6 | $8-15,25$ | $8-15$, Top View |
| A4S1 SWITCH, TEST/NORMAL | 6,6 | $8-15,25$ | $8-15$, Top View |
| A5 Assembly | 2,4 | $8-15,25$ | $8-15$, Top View |
| A6 Assembly | 2,6 | $8-25$ |  |
| A7 Assembly | 2,4 | $8-25$ |  |
| A8 Assembly | 2,4 | $8-10,25$ | Top View |
| A9 Assembly | 3,8 | $8-25$ |  |
| A10 Assembly | 2,7 | $8-21,25$ | $8-25$, Left Side View |
| A10R2, ADJ, AM LIN | 7 | $8-18,25$ | $8-25$, Left Side View |
| A10R5 ADJ, AM CAL | 7 | $8-18,25$ | $8-25$, Top View |
| A10R7 ADJ, RF LEVEL | 7 | $8-18,25$ | $8-25$, Top View |
| A11 Assembly | 3,9 | $8-18,25$ | $8-25$, Top View |
| A12 Assembly | 2,4 | $8-23,25$ | $8-25$, Left Side View |
|  |  | $8-25$ | (A9, A10, and A11 plug into connectors |
| mounted on A12) |  |  |  |

Table 8-2. Assemblies, Chassis Mounted Parts, and Adjustable Component Locations (2 of 2)

| Reference Designator | Service Sheet | Figures | Remarks |
| :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { P1, } 2 \\ & \text { P3, 4 } \\ & \text { P5 } \\ & \text { P6 } \\ & \hline \end{aligned}$ | $\begin{aligned} & 2,4 \\ & 6 \\ & 4 \\ & 2,3,4,5,7,8,9 \end{aligned}$ | $3-2$ $3-2,8-25$ | $3-2, \mathrm{P} 2$ is (1) and P 1 is (3) <br> Not Shown, +20 V inputs to A6. <br> Not Shown, +20 V input to A8 <br> $3-2, \mathrm{P} 6$ is (2) |
| $\begin{aligned} & \text { P7 } \\ & \text { P13 } \\ & \text { P14 } \end{aligned}$ | $\begin{aligned} & 4 \\ & 2,4,6,7,8,9 \\ & 2,6,8 \end{aligned}$ | $\begin{array}{r} 8-25 \\ 8-25 \\ \hline \end{array}$ | Not Shown, -10 V input to A8 |
| $\begin{aligned} & \mathrm{R} 1 \\ & \mathrm{R} 2 \end{aligned}$ | $\begin{aligned} & 2,7 \\ & 7 \end{aligned}$ | $\begin{aligned} & \hline 8-25 \\ & 8-25 \end{aligned}$ | 8-25, Front Panel Internal View 8-25, Front Panel Internal View |
| S1 | 3,9 | 8-25 | 8-25, Front Panel Internal View |
| TB1 | 6 | 8-25 | Top View |
| W1* <br> W2* <br> W3 <br> W4* <br> W5* | $\begin{aligned} & \hline 2,5 \\ & 2,4 \\ & 2,4 \\ & 2,4 \\ & 2,4 \\ & \hline \end{aligned}$ | $\begin{aligned} & 8-25 \\ & 8-25 \\ & 8-25 \\ & 8-25 \\ & 8-25 \end{aligned}$ | Right Side View, FL1 Output <br> Top View, A8 Output <br> AT1 Input, grey/blue <br> AT1 Output <br> Top View, A5 Output |
| W6* <br> W7* <br> W8 <br> W9 <br> W10* | $\begin{aligned} & 2,4,6 \\ & 2,6,8 \\ & 2,7 \\ & 2,7 \\ & 2,5 \end{aligned}$ | $\begin{aligned} & 8-25 \\ & 8-25 \\ & 8-25 \\ & 8-4,25 \\ & 8-25 \end{aligned}$ | Top View, A6 Input <br> A13 Input <br> AM Input to A12, grey/yellow Pulse Input to A2, white/green A18 Output |
| W11 <br> W12 <br> W13* <br> W14 <br> W15 | $\begin{aligned} & 2,4 \\ & 2,5 \\ & 2,4,5 \\ & 2,5 \\ & 2,4 \end{aligned}$ | $\begin{aligned} & 8-25 \\ & 8-4,25 \\ & 8-25 \\ & 8-25 \\ & 8-25 \end{aligned}$ | FL1 Input, grey <br> $\phi$ M Input to A16, white/violet <br> A18 Input <br> Right Side View, A16 Output, grey <br> A15 Input from P6, white/blue |
| W16 <br> W17 <br> W18 <br> W19 | $\begin{aligned} & 2,4 \\ & 2,4 \\ & 2,4 \\ & 2,4 \end{aligned}$ | $\begin{aligned} & 8-25 \\ & 8-25 \\ & 8-25 \end{aligned}$ | Not Shown, P6 Interconnect Cable, white/orange <br> Rear Panel Internal View, P6 Interconnect Cable, white/yellow <br> Rear Panel Internal View, P6 Interconnect <br> Cable, white/brown <br> A15 Output to P6, white/red |
| *Indicates semi-rigid coaxial cable. |  |  |  |



## LEFT SIDE VIEW



Figure 8-25. Assemblies, Chassis Parts, and Adjustable Component Locations


[^0]:    ${ }^{1}$ Aging rate for the time base of standard mainframes is
    $3 \times 10^{-8} / \mathrm{day}$; for option 001 mainframes, $3 \times 10^{-9} /$ day.

[^1]:    2 Applies only at 400 Hz and 1 kHz rates with the RF Section front panel meter indicating from 0 to +3 dBm . At a meter indication of -6 dB the distortion approximately doubles, The modulating signal distortion must be $<0.3 \%$ for the system performance to meet these specifications.

[^2]:    * Use: $\mathbf{P}=$ Performance Tests, $\mathbf{A}=$ Adjustments, $\mathbf{T}=$ Troubleshooting

[^3]:    3.5 div. p-p

[^4]:    * In Figure $4-16 \mathrm{~A}$, the test oscillator output is 50 ohms when the modulation section is a Model 86634 A and 600 ohms when used with a Model 86635A

[^5]:    * In Figure 4-16B, the test oscillator output impedance and Low Pass Filter impedance is 50 ohms when the modulation section is a Model 86634A and 600 ohms with a Model 86635A.

[^6]:    *STATNUL by Weston Instrument Inc., Newark, New Jersey

[^7]:    *In Figure $5-5 \mathrm{~A}$, the test oscillator output and low pass filter impedances are $50 \Omega$ when the modulation section being used is a Model 86634 A and $600 \Omega$ when used with an 86635 A .

[^8]:    *In Figure $5-5 B$, the test oscillator output and low pass filter impedances are 50 ohms when the modulation section being used is a Model 86634 A and 600 ohm when used with an 86635 A .

